

Life Cycle Assessment 2013 OF THE HEBB BUILDING

ZEYU ROCKY ZHANG

University of British Columbia

CIVL 498C

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PROVISIO

This study has been completed by undergraduate students as part of their coursework at the University of British Columbia (UBC) and is also a contribution to a larger effort – the UBC LCA Project – which aims to support the development of the field of life cycle assessment (LCA).

The information and findings contained in this report have not been through a full critical review and should be considered preliminary.

If further information is required, please contact the course instructor Rob Sianchuk at rob.sianchuk@gmail.com



2013

Life Cycle Assessment

OF THE HEBB BUILDING
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Executive Summary

This LCA of the HEBB building is part of a series of studies being carried out simultaneously on respective buildings at UBC in an attempt to conduct environmental performance comparisons for future reference. The HEBB building is modeled using On-Screen Takeoff and Impact Estimator. Impact categories are listed for the building and its corresponding elements. Interpretations and recommendations are given for the use of LCA.

Life Cycle Assessment of UBC HEBB Building

1.0 General Information on the Assessment

Purpose of the assessment

The life cycle analysis of the UBC HEBB building is a study intended to present the building design's environmental impacts.

By establishing materials inventory and the corresponding environmental impacts, potential future performance upgrade assessments can be made easier. Environmental performance comparisons with other UBC buildings also becomes a possibility which means sustainable development guidelines for future construction projects can be created at UBC.

This study is mainly intended for those who are involved in building development and policy making at UBC such as the Sustainability Office. Others such as engineers, architects, and external parties are also potential audiences.

Identification of building

The HEBB building, constructed in 1964, is located at 2045 East Mall, University of British Columbia. It was named after the first Head of the Physics Department, Dr. Thomas Carlyle Hebb.

The architect on the project was Thompson, Berwick & Pratt, and the cost of the construction was \$1,398,503. The lecture theatre and the 5-floor tower was mainly used by the Departments of Physics and Engineering Physics. It is a reinforced concrete structure with brick facings and painted concrete.

Other Assessment Information

Client for Assessment	Completed as coursework in Civil Engineering technical elective course at the University of British Columbia.
Name and qualification of the assessor	Zeyu Rocky Zhang, Civil Engineering Undergraduate
Impact Assessment method	OnScreen TakeOff 3.9.06 Impact Estimator 4.2.0208 TRACI 2.1
Point of Assessment	49 years.
Period of Validity	5 years.

Date of Assessment	Completed in December 2013.
Verifier	Student work, study not verified.

2.0 General Information on the Object of Assessment

Functional Equivalent

Functional unit is a performance characteristic of the product system. It is used as a reference unit to normalize the results of the study.

Aspect of Object of Assessment	Description
Building Type	Institutional
Technical and functional requirements	BC
Pattern of use	Monday to Friday (0800-1730), Sat/Sun/Holidays closed General Purpose Room x3 Capacity = 54 students each Tiered Large Group x1 Capacity = 375
Required service life	100 years

Reference Study Period

The service life of HEBB is 100 years according to UBC.

This study exclude modules B, C and D because it is a cradle-to-gate assessment. For comparison purposes, the use stage, end of life stage, and items beyond the system boundary are not considered.

Object of Assessment Scope

The foundation assembly of HEBB is composed of concrete slab-on-grade and concrete footings. The wall assemblies for both the tower and theatre consist of concrete cast-in-place interior and exterior walls. A modified version of CIQS Level 3 Elements is used due to the purpose of the study. The use stage and the end of life stage are not considered.

CIVL 498C Level 3 Elements	Description	Quantity (Amount)	Units

A11	Foundations	Total area of the footing	369.4968	m ²
A21	Lowest Floor Construction	Total area of the slab-on-grade	1898.386	m ²
A22	Upper Floor Construction	Stairs area	3878.531	m ²
A23	Roof Construction	Roof Concrete Slab area	1410.632	m ²
A31	Walls Below Grade	Cast-In-Place Exterior surface area	1049.674	m ²
A32	Walls Above Grade	Cast-In-Place Exterior and Interior surface area	3722.657	m ²
B11	Partitions	Interior Partition Walls surface area	1296.132	m ²

3.0 Statement of Boundaries and Scenarios Used in the Assessment

System Boundary

Life cycle modules included in the study are the product stage and the construction process stage. Module B, C, and D are excluded due to the nature of the analysis. The product stage includes raw material supply as source, transportation, then manufacturing to finish. The construction process stage starts with transportation, then installation to finish.

Product Stage

During the manufacturing phase, energy consumption should be significant since the transforming of raw materials and transporting of the raw materials both require energy. The transporting of energy itself also requires energy. Resource use is needed for resource extraction, which is important for the manufacturing stage. Process involving packing, collection and relocation of waste are all part of the energy use within the product stage.

Construction Stage

Energy use in transportation is dominant during the construction stage, especially for a concrete structure. For storage handling, temperature control has to be provided. Energy and resource are also needed for the handling of waste and the installation of the product.

4.0 Environmental Data

Data Sources

The Athena LCI Database is created and managed by the Athena Institute. From the beginning, the Athena Institute has been conducting life cycle research. Their goal was to develop an ever-growing set of comprehensive, comparable life cycle inventory database for building materials and products. The database not only contain information on building materials and products, it also includes energy use, transportation, construction and demolition processes such as on-site construction, maintenance, and demolition and disposal. The data is regionally sensitive, taking into consideration relevant technology differences in different region.

The US LCI Database is created by the National Renewable Energy Laboratory of the US Energy Department. Its goal is to help life cycle assessment practitioners answer questions about environmental impacts. The database provides individual gate-to-gate, cradle-to-gate and cradle-to-grave accounting of the energy and material flows into and out of the environment that are associated with producing material, component, or assembly in the US.

Data Adjustments and Substitutions

The partition walls were not correctly listed. They have been fixed for this report.

Data Quality

Data uncertainty may be due to the collection/allocation methods used in creating data, the uncertainty in the substance lifetime, travel potential, or just inaccurate data. Model uncertainty may be due to the non-linear nature of the data, or the uncertain characterization factors. Temporal variability may be due to the effect of climate, the variability over time on impact interpretation, data validity as time changes, or the actual emissions over the years. Spatial variability may be due to the regional differences in environmental sensitivity, the distribution of emissions, or the regional differences between factories. Variability between sources may be due to the differences in human exposure patterns, technology differences, or the difference between factories.

The quality of the LCI database used in this study is quite high, as they are directly from the Athena Sustainable Materials Institute.

5.0 List of Indicators Used for Assessment and Expression of Results

The two main software tools used in this LCA study are the Athena Sustainable Materials Institute's Impact Estimator and OnCenter's OnScreen TakeOff. The study conducts materials quantity takeoff by performing linear area measurements of the building's structure and envelope. Then, with IE based on TRACI, a complete environmental impact profile can be made containing impact categories:

Global warming potential

Cause Effect Chain: Air emission -> infrared radiation -> climate change affecting temperature, precipitation, and sea level

Category indicator = kg CO₂e

Endpoint: Water resource effects, human health, agricultural effects, coastal damage

Acidification potential

Cause Effect Chain: Emission atmospheric concentration -> Deposition -> Leaching

Category indicator = kg SO₂eq

Endpoint: Ecosystem changes, plant and animal mortality

Eutrophication potential

Cause Effect Chain: Water emission -> Algae and Aquatic weed growth -> Oxygen shortage

Category indicator = kg Neq

Endpoint: Death of fish, toxicity to humans

Ozone depletion potential

Cause Effect Chain: Air emission -> Reduction of Ozone Layer -> Increased UVB reaching Earth

Category indicator = kg CFC-11eq

Endpoint: Agricultural Effects, Human health, Material Damage

Photochemical smog potential

Cause Effect Chain: Air emission -> tropospheric ozone concentrations -> human inhalation -> plant growth reduction

Category indicator = kg O₃eq

Endpoint: human mortality, plant mortality

Human health respiratory effects potential

Cause Effect Chain: Air emission -> PM deposition in alveoli -> Body reacts to PM

Category indicator = kg PM_{2.5}eq

Endpoint: Human Health, Human Mortality

Weighted raw resource use

Cause Effect Chain: Resource harvesting

Category indicator = kg

Endpoint: Resource depletion

6.0 Model Development

OnScreen TakeOff was used on imported digital plans to conduct materials quantity takeoff. The measurements generated OnScreen TakeOff are formatted in such a way that the Impact Estimator building LCA software can complete the takeoff process. Using the formatted takeoff data, the CIQS level 3 elements are modeled. The impact estimator is designed mainly to aid the building community in making more environmentally conscious material and design choices. The tool achieves this by applying a set of algorithms to the inputted takeoff data in order to complete the takeoff process and generate a bill of materials. The Athena Life Cycle Inventory Database is then used to generate a cradle-to-grave LCI profile based on the bill of materials showing the impacts. Since this study is a cradle-to-gate assessment, the expected service life of the HEBB building is set to 1 year, which means the maintenance, operating energy and end-of-life stages of the building's life cycle are not considered.

Bill of Material of the building:

A11	Quantity	Unit
Concrete 30 MPa (flyash av)	176.8860	m3
Rebar, Rod, Light Sections	2.8405	Tonnes

A21	Quantity	Unit
Concrete 30 MPa (flyash av)	199.3307	m3
Welded Wire Mesh / Ladder Wire	1.7156	Tonnes

A22	Quantity	Unit
Concrete 30 MPa (flyash av)	1493.6093	m3
Rebar, Rod, Light Sections	213.2708	Tonnes

A23	Quantity	Unit
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#15 Organic Felt	4649.8579	m2
6 mil Polyethylene	1496.1885	m2
Ballast (aggregate stone)	56033.3556	kg
Concrete 30 MPa (flyash av)	216.2448	m3
Extruded Polystyrene	8892.4878	m2 (25mm)
Galvanized Sheet	1.6806	Tonnes
Nails	0.4025	Tonnes
Polyethylene Filter Fabric	0.0534	Tonnes
Rebar, Rod, Light Sections	13.7436	Tonnes
Roofing Asphalt	15173.2496	kg
Type III Glass Felt	3563.8643	m2

A31	Quantity	Unit
1/2" Regular Gypsum Board	730.3472	m2
6 mil Polyethylene	704.3203	m2
Cold Rolled Sheet	0.1341	Tonnes
Concrete 30 MPa (flyash av)	255.3989	m3
Extruded Polystyrene	691.0262	m2 (25mm)
Joint Compound	0.7289	Tonnes
Mortar	19.3272	m3
Nails	0.0694	Tonnes
Ontario (Standard) Brick	697.1496	m2
Paper Tape	0.0084	Tonnes

Rebar, Rod, Light Sections	8.9183	Tonnes
Small Dimension Softwood Lumber, kiln-dried	0.8554	m3
Solvent Based Alkyd Paint	69.0776	L
Water Based Latex Paint	7.7059	L

A32	Quantity	Unit
1/2" Regular Gypsum Board	4033.2786	m2
6 mil Polyethylene	3889.5472	m2
Aluminum	6.5099	Tonnes
Cold Rolled Sheet	0.7407	Tonnes
Concrete 30 MPa (flyash av)	962.0415	m3
Double Glazed No Coating Air	526.6749	m2
EPDM membrane (black, 60 mil)	445.2739	kg
Expanded Polystyrene	6.5100	m2 (25mm)
Extruded Polystyrene	3816.1318	m2 (25mm)
Galvanized Sheet	0.1238	Tonnes
Joint Compound	4.0253	Tonnes
Mortar	106.7329	m3
Nails	0.6408	Tonnes
Ontario (Standard) Brick	3849.9478	m2
Paper Tape	0.0462	Tonnes
Rebar, Rod, Light Sections	33.2603	Tonnes
Solvent Based Alkyd Paint	382.0644	L

B11	Quantity	Unit
Aluminum	1.1136	Tonnes
Concrete 30 MPa (flyash av)	302.0405	m3
Double Glazed No Coating Air	99.3015	m2
EPDM membrane (black, 60 mil)	76.1678	kg
Nails	0.2379	Tonnes
Rebar, Rod, Light Sections	10.6861	Tonnes
Small Dimension Softwood Lumber, kiln-dried	6.9206	m3
Water Based Latex Paint	62.3477	L

Partition walls were not corrected listed in the input document. They have been fixed.

Reference flow is the measure of the outputs from processes in a given product system required to fulfill the function expressed by the functional unit.

7.0 Communication of Assessment Results

Life Cycle Results

Life Cycle Stage	Process Module	Fossil Fuel Consumption	Global Warming	Acidification	Health Criteria – Respiratory	Eutrophication	Ozone Layer Depletion	Smog
		(MJ)	(kg CO2eq)	(moles of H+eq)	(kg PM10eq)	(kg Neq)	(kg CFC-11eq)	(kg O3eq)
PRODUCT	Manufacturing	15,050,671.41	1,423,095.85	10,042.32	3,172.97	699.65	7.43E-03	164,020.14
	Transport	612,406.79	36,969.99	229.22	6.44	16.04	1.51E-06	8,115.36
	Total	15,663,078.20	1,460,065.84	10,271.54	3,179.41	715.69	7.44E-03	172,135.50
CONSTRUCTION PROCESS	Construction-installation	838,681.90	85,247.68	656.36	157.04	34.30	3.25E-04	16,066.90
	Transport	1,716,642.76	131,189.82	610.66	18.88	44.04	5.23E-06	21,593.64
	Total	2,555,324.65	216,437.50	1,267.02	175.92	78.34	3.31E-04	37,660.54

It is evident that during the manufacturing phase of the HEBB building, energy and resource consumption is very significant. This makes sense, since concrete requires a substantial amount of energy and raw material (gravel, sand, cement, aggregate) to be processed and manufactured. As for the construction phase, transportation takes lead in energy consumption.

The production of cement is responsible for the discharge of carbon dioxide emissions. For one ton of cement manufactured, approximately one ton of carbon dioxide is emitted. Thus concrete is the main contributor to global warming potential. The by-product from concrete production is also

one of the main cause for acidification, HH Respiratory effects, eutrophication, ozone depletion, and smog.

	Material	Quantity	Units	Fossil Fuel (MJ)	Global Warming (kg CO ₂ e)	Acidification (moles of)	Human Health (kg PM ₁₀ eq)	Eutrophication (kg Neq)	Ozone Layer (kg CFC-11eq)	Smog (kg O ₃ eq)
HEBB TOTAL		5776.917	m2 (total)	3383.109	306.2296	2.170571	0.585455902	0.149109175	1.34517E-06	42.45797
Per m2				0.585625	0.053009	0.000376	0.000101344	2.58112E-05	2.32853E-10	0.00735

	Material	Quantity	Units	Fossil Fuel (MJ)	Global Warming (kg CO ₂ e)	Acidification (moles of)	Human Health (kg PM ₁₀ eq)	Eutrophication (kg Neq)	Ozone Layer (kg CFC-11eq)	Smog (kg O ₃ eq)
A11 Foundations		369.4968	m2	1051.486	148.0163	0.956029	0.354092077	0.049079327	8.16332E-07	20.61283
Per m2				2.845725	0.400589	0.002587	0.000958309	0.000132827	2.20931E-09	0.055786

	Material	Quantity	Units	Fossil Fuel (MJ)	Global Warming (kg CO ₂ e)	Acidification (moles of)	Human Health (kg PM ₁₀ eq)	Eutrophication (kg Neq)	Ozone Layer (kg CFC-11eq)	Smog (kg O ₃ eq)
A21 Lowest Floor Construction		1898.386	m2	260.3903	35.05953	0.237206	0.078584123	0.011387693	1.79154E-07	5.476354
Per m2				0.137164	0.018468	0.000125	4.13952E-05	5.99862E-06	9.43717E-11	0.002885

	Material	Quantity	Units	Fossil Fuel (MJ)	Global Warming (kg CO ₂ e)	Acidification (moles of)	Human Health (kg PM ₁₀ eq)	Eutrophication (kg Neq)	Ozone Layer (kg CFC-11eq)	Smog (kg O ₃ eq)
A22 Upper Floor Construction		3878.531	m2	1832.085	162.548	1.131531	0.300368331	0.117829518	6.57263E-07	24.07167
Per m2				0.472366	0.04191	0.000292	7.74438E-05	3.03799E-05	1.69462E-10	0.006206

	Material	Quantity	Units	Fossil Fuel (MJ)	Global Warming (kg CO ₂ e)	Acidification (moles of)	Human Health (kg PM ₁₀ eq)	Eutrophication (kg Neq)	Ozone Layer (kg CFC-11eq)	Smog (kg O ₃ eq)
A23 Roof Construction		1410.632	m2	1781.06	92.57821	0.533779	0.2329398	0.037230187	2.62094E-07	11.65936
Per m2				1.262597	0.065629	0.000378	0.000165132	2.63926E-05	1.85799E-10	0.008265

	Material	Quantity	Units	Fossil Fuel (MJ)	Global Warming (kg CO ₂ e)	Acidification (moles of)	Human Health (kg PM ₁₀ eq)	Eutrophication (kg Neq)	Ozone Layer (kg CFC-11eq)	Smog (kg O ₃ eq)
A31 Walls Below Grade		1049.674	m2	1236.876	124.8224	0.855751	0.216069104	0.045224057	4.49981E-07	16.93411
Per m2				1.178344	0.118915	0.000815	0.000205844	4.30839E-05	4.28686E-10	0.016133

	Material	Quantity	Units	Fossil Fuel (MJ)	Global Warming (kg CO ₂ e)	Acidification (moles of)	Human Health (kg PM ₁₀ eq)	Eutrophication (kg Neq)	Ozone Layer (kg CFC-11eq)	Smog (kg O ₃ eq)
A32 Walls Above Grade		3722.657	m2	1765.993	167.3911	1.262611	0.293207302	0.055991707	7.80883E-07	21.2197
Per m2				0.474391	0.044965	0.000339	7.87629E-05	1.50408E-05	2.09765E-10	0.0057

				Fossil Fuel	Global Warming	Acidification	Human Health	Eutrophication	Ozone Layer	Smog
	Material	Quantity	Units	(MJ)	(kg CO ₂ e)	(moles of)	(kg PM ₁₀ eq)	(kg Neq)	(kg CFC-11eq)	(kg O ₃ eq)
B11 Partitions		1296.132	m ²	765.7676	88.2392	0.657844	0.200436525	0.036606436	5.49591E-07	13.16877
Per m ²				0.59081	0.068079	0.000508	0.000154642	2.82428E-05	4.24023E-10	0.01016

Annex A – Interpretation of Assessment Results (18)

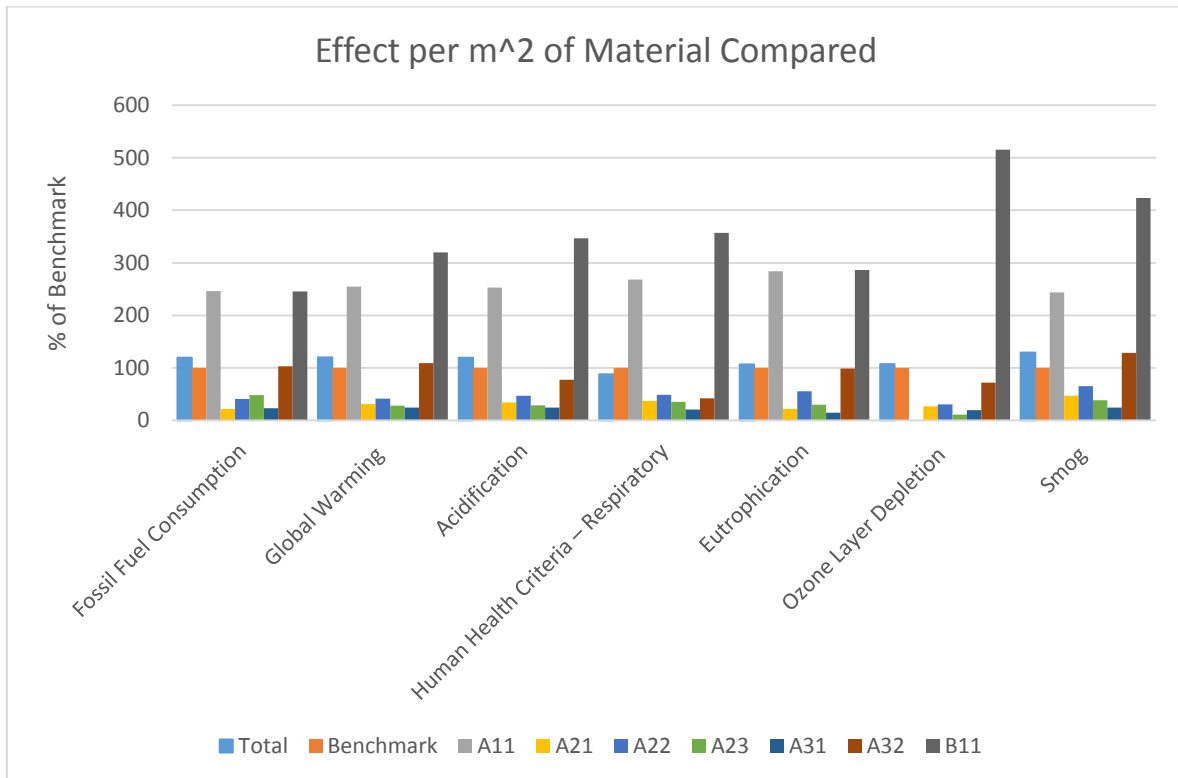
Benchmark Development

Benchmarking in LCA is a way of analysis in conjunction with other similar studies. With benchmarking, further applications of LCA are made possible such as environmental performance comparisons across the buildings in a region over time and between different materials, structural types and building functions. It may also form a powerful tool to help inform policy makers in establishing quantified sustainable development guidelines for future constructions such as a set amount of reduction in certain aspects per year.

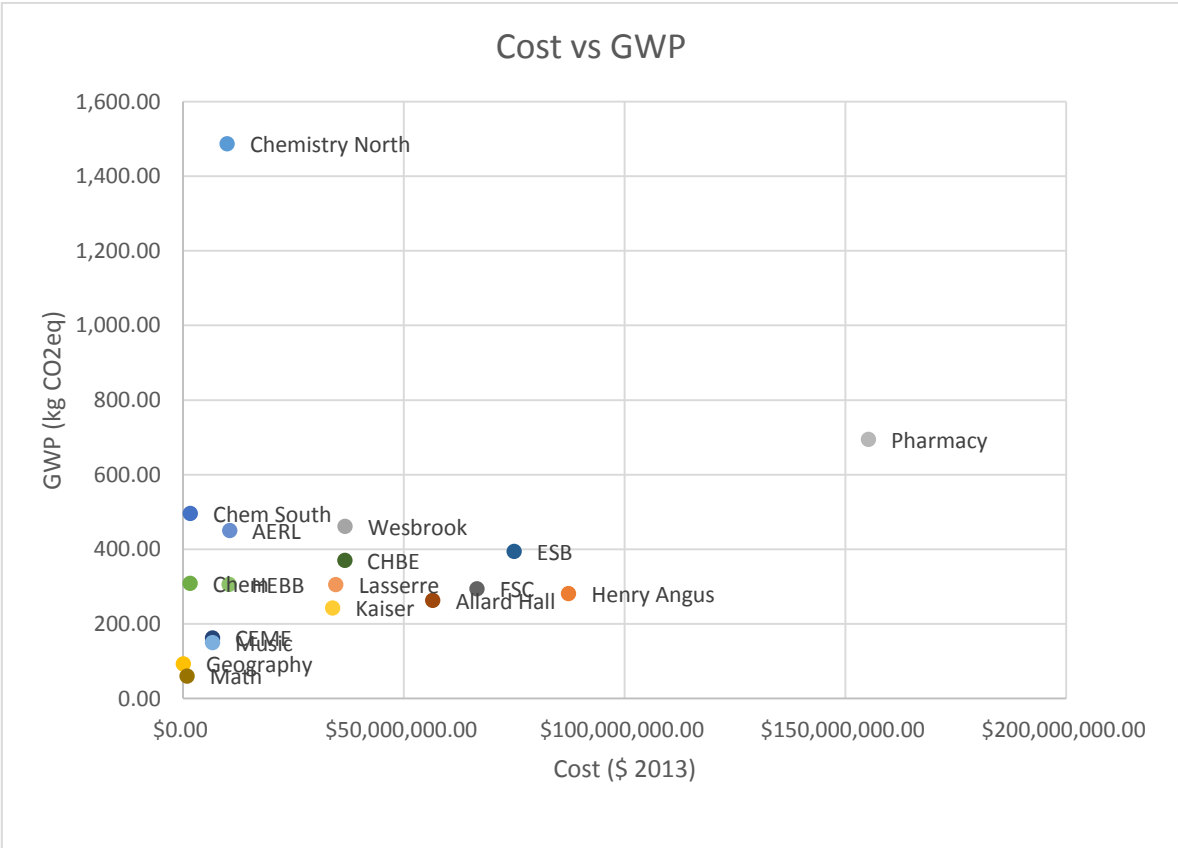
UBC Academic Building Benchmark (12)

-describe and show your building results compared against the class benchmark in figure.

-discuss these comparisons



The overall environmental performance is not too far off from the benchmark. But there exists a large discrepancy for partition walls as they were not listed correctly. Other than that, footings seem to be the largest contributor to the impact categories.



From the chart, we could see that some of the really old buildings have both low costs and low global warming potentials. But for the majority, there exists a pattern of lower GWP for higher costs. This is likely due to the higher expense for selecting specific materials that have low contribution to GWP.

Annex B – Recommendations for LCA Use (20)

Though only the product and construction stages are considered in this study, the other life cycle modules are as equally important as the initial two due to their nature and the possible issues that may arise as time passes by. A building is not a product for one time consumption. It requires maintenance throughout its life time, and there are disposal fees associated at the end. Because of the long service life of most buildings, the impacts it may have on the environment can accumulate greatly through use. Furthermore, there may actually be benefits beyond the system

boundary. Reuse, recycling, and recovery of material are all elements that may not be very apparent straight up.

With the help of LCA, the environmental performance of the building can be improved. The wall insulation, roof insulation, and window type could be changed to reduce energy consumption. For example, replacing the 1" extruded polystyrene with 2.5" of foam polyisocyanurate insulation, replacing the standard glazed windows with low E silver argon filled glazing, and adding 7" of extruded polystyrene to the roof insulation could produce a total energy savings of approximately 160,000Gj over the building's service life.

However, the building performance model is still only an approximate. Without high quality data and available benchmarks, the model's use is limited. Plus, factors such as economics and logistics concerns must be considered. Investing in the more expensive foam polyisocyanurate and low E silver argon filled windows may not always be feasible due to project budget constraints.

Another issue is the prioritizing of impact categories. The associated parties may not always have the same concerns. Reducing energy consumption may not be the goal of the owner or client. LCA is a lens through which the building elements and the environmental impacts are linked together. The life cycle assessment of HEBB is done by doing the takeoffs and modeling the building using the Impact Estimator. It is up to the stake holders to decide which impact category they want to focus on.

For UBC, LCA can be utilized to help develop guidelines for on campus constructions. By looking at and comparing the cost vs gwp relations for example, standards can be set incrementally by the policy makers for all future projects.

Annex C – Author Reflection (8)

As a student, I was briefly introduced to LCA in the 2nd year course, Introduction to Civil Engineering. Here in CIVL 498C, I gained further insight into the nature of the LCA and its applications. I took a look at its history, and understood its current state in North America. I went through the LCA section in the ISO standards, and completed a study following it. I familiarized myself with the CIQS elements format, the various tools including IE + OnScreen TakeOff, and used them in a LCA study for the UBC HEBB Building.

It interests me how important LCA can be in improving a design's environmental performance. By measuring the environmental performance of products over their life cycle, LCA can show us exactly we need to do to achieve what we want. It's a tool that everyone should care about.

6	Graduate Attribute			
7	Name	Description	Select the content code most appropriate for each attribute from the dropdown menu	Comments on which of the CEAB graduate attributes you believe you had to demonstrate during your final project experience.
8				
9	1 Knowledge Base	Demonstrated competence in university level mathematics, natural sciences, engineering fundamentals, and specialized engineering knowledge appropriate to the program.	A= applied	Demonstrated
10	2 Problem Analysis	An ability to use appropriate knowledge and skills to identify, formulate, analyze, and solve complex engineering problems in order to reach substantiated conclusions.	A= applied	Demonstrated
11	3 Investigation	An ability to conduct investigations of complex problems by methods that include appropriate experiments, analysis and interpretation of data, and synthesis of information in order to reach valid conclusions.	A= applied	Demonstrated
13	4 Design	An ability to design solutions for complex, open-ended engineering problems and to design systems, components or processes that meet specified needs with appropriate attention to health and safety risks, applicable standards, and economic, environmental, cultural	N/A= not applicable	
14	5 Use fo Engineering Tools	An ability to create, select, apply, adapt, and extend appropriate techniques, resources, and modern engineering tools to a range of engineering activities, from simple to complex, with an understanding of the associated limitations.	IA= introduced & applied	Demonstrated
17	6 Individual and Team Work	An ability to work effectively as a member and leader in teams, preferably in a multi-disciplinary setting.	DA= developed & applied	Demonstrated
18	7 Communication	An ability to communicate complex engineering concepts within the profession and with society at large. Such ability includes reading, writing, speaking and listening, and the ability to comprehend and write effective reports and design documentation, and to give and effectively respond to clear instructions.	A= applied	Demonstrated
20	8 Professionalism	An understanding of the roles and responsibilities of the professional engineer in society, especially the primary role of protection of the public and the public interest.	A= applied	Demonstrated
21	9 Impact of Engineering on Society and the Environment	An ability to analyze social and environmental aspects of engineering activities. Such ability includes an understanding of the interactions that engineering has with the economic, social, health, safety, legal, and cultural aspects of society, the uncertainties in the prediction of such interactions, and the concepts of sustainable design	A= applied	Demonstrated
22	10 Ethics and Equity	An ability to apply professional ethics, accountability, and equity.	N/A= not applicable	
27	11 Economics and Project Management	An ability to appropriately incorporate economics and business practices including project, risk, and change management into the practice of engineering and to understand their limitations.	N/A= not applicable	
28	12 Life-long Learning	An ability to identify and to address their own educational needs in a changing world in ways sufficient to maintain their competence and to allow them to contribute to the	N/A= not applicable	
29				
30				

Annex D – Impact Estimator Inputs and Assumptions (20)

HEBB TOWER Inputs

Element	Quantity	Units	Assembly Type	Assembly Name	Input Fields	Known/Measured Information	IE Inputs
A11 Foundations	222.3217	m ²					
			Footin g	1.2.1 Footin g_F1a_Basement	Length (ft)	4.25	4.25
					Width (ft)	2	8.42
					Thickn ess (in)	80	19
					Concr ete (psi)	-	4000
					Concr ete flyash %	-	average
					Rebar	#5	#5
				1.2.2 Footin g_F1b_Basement	Length (ft)	0.92	0.92
					Width (ft)	0.83	0.83
					Thickn ess (in)	12	12
					Concr ete (psi)	-	4000
					Concr ete flyash %	-	average
					Rebar	#5	#5

				1.2.3 Footings_F2a_Basement	Length (ft)	5.17	5.17
					Width (ft)	2.5	10.53
					Thickness (in)	80	19
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
				1.2.4 Footings_F2b_Basement	Length (ft)	3.92	3.92
					Width (ft)	1.125	1.125
					Thickness (in)	12	12
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
				1.2.5 Footings_FA_Basement	Length (ft)	152.5	152.5
					Width (ft)	3.5	3.5
					Thickness (in)	15	15
					Concrete (psi)	-	4000
					Concrete flyash %	-	average

					Rebar	#5	#5
				1.2.6 Footing_FB_Basement	Length (ft)	280.29	280.29
					Width (ft)	2	2
					Thickness (in)	12	12
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
				1.2.7 Footing_FC_Basement	Length (ft)	148.5	148.5
					Width (ft)	4	4
					Thickness (in)	15	15
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
				1.2.8 Footing_FD_Basement	Length (ft)	34	34
					Width (ft)	2	2
					Thickness (in)	12	12
					Concrete (psi)	-	4000
					Concrete flyash	-	average

					%		
					Rebar	#5	#5
				1.2.9 Footing_FE_Basement	Length (ft)	56.83	56.83
					Width (ft)	2.5	2.5
					Thickness (in)	12	12
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
				1.2.10 Footing_FF_Basement	Length (ft)	22.42	22.42
					Width (ft)	2	2
					Thickness (in)	12	12
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
				1.2.11 Footing_FG_Basement	Length (ft)	48.06	48.06
					Width (ft)	1.8	7.58
					Thickness (in)	80	19
					Concrete (psi)	-	4000

					Concrete flyash %	-	average
					Rebar	#5	#5
				1.2.12 Footing_FH_Basement	Length (ft)	25.08	25.08
					Width (ft)	1.5	6.32
					Thickness (in)	80	19
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
				1.2.13 Footing_FJ_Basement	Length (ft)	30.5	30.5
					Width (ft)	2.75	2.75
					Thickness (in)	12	12
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
				1.2.14 Footing_FK_Basement	Length (ft)	24.33	24.33
					Width (ft)	3	3
					Thickness (in)	12	12
					Concrete	-	4000

					(psi)		
					Concrete flyash %	-	average
					Rebar	#5	#5
				1.2.15 Footing_FL_Basement	Length (ft)	38.83	38.83
					Width (ft)	1.5	1.5
					Thickness (in)	12	12
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
				1.2.16 Footing_FM_Basement	Length (ft)	29.67	29.67
					Width (ft)	2	2
					Thickness (in)	12	12
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5

				1.2.17 Footing_FN_Basement	Length (ft)	16.42	16.42
					Width (ft)	1.5	1.5
					Thickness (in)	12	12
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
A21 Lowest Floor Construction	1241.926	m ²					
			SOG	1.1.1 SOG_5"_Tower	Length (ft)	115.62	115.62
					Width (ft)	115.62	115.62
					Thickness (in)	5	4
					Concrete (psi)	-	4000
					Concrete flyash %	-	average

A22 Upper Floor Constru ction	2783. 885	m^ 2					
			Stairs	1.2.18 Stairs_South/North_Platform	Length (ft)	141.74	141.74
					Width (ft)	5.33	4.26
					Thickn ess (in)	6	7.5
					Concr ete (psi)	-	4000
					Concr ete flyash %	-	average
					Rebar	#5	#5
				1.2.19 Stairs_South/North_Steps	Length (ft)	182.83	182.83
					Width (ft)	5.33	5.33
					Thickn ess (in)	8	8
					Concr ete (psi)	-	4000
					Concr ete flyash %	-	average
					Rebar	#5	#5

			Column Beam	3.1.1 Column_Beam_Concrete Basement	Number of Columns	25	25
					Number of Beams	5	5
					Bay Sizes (ft)	41.5	40
					Supported Span (ft)	12.5	12.5
					Floor to Floor Height (ft)	12	12
					Live Load (psf)	60, 100	75
				3.1.2 Column_Beam_Concrete_Gr ndFlr	Number of Columns	28	28
					Number of Beams	12	12
					Bay Sizes (ft)	41.5	40
					Supported Span (ft)	12.5	12.5
					Floor to Floor Height (ft)	12	12

					Live Load (psf)	60, 100	75
				3.1.3 Column_Beam_Concrete_SecondFlr	Number of Columns	28	28
					Number of Beams	12	12
					Bay Sizes (ft)	41.5	40
					Supported Span (ft)	12.5	12.5
					Floor to Floor Height (ft)	12	12
					Live Load (psf)	60, 100	75
				3.1.4 Column_Beam_Concrete_topFlr	Number of Columns	28	84
					Number of Beams	12	36
					Bay Sizes (ft)	41.5	40
					Supported Span (ft)	12.5	12.5

					Floor to Floor Height (ft)	12	12
					Live Load (psf)	60, 100	75
			Suspended Floor	4.1.1 Floor_ConcreteSuspendedSI ab_GrndFlr	Floor Width (ft)	797.08	797.08
					Span (ft)	12.5	12.5
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Life Load (psf)	60, 100	75
				4.1.2 Floor_ConcreteSuspendedSI ab_SecondFlr	Floor Width (ft)	681.41	681.41
					Span (ft)	12.5	12.5
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Life Load (psf)	60, 100	75

				4.1.3 Floor_ConcreteSuspendedSI ab_TypeFlr	Floor Width (ft)	595.39	1786.16
					Span (ft)	12.5	12.5
					Concr ete (psi)	-	4000
					Concr ete flyash %	-	average
					Life Load (psf)	60, 100	75
				4.1.4 Floor_ConcreteSuspendedSI ab_Penthouse	Floor Width (ft)	192.67	192.67
					Span (ft)	12	12
					Concr ete (psi)	-	4000
					Concr ete flyash %	-	average
					Life Load (psf)	60, 100	75
A23 Roof Constru	781.5 233	m [^] 2					

ction							
			Envelope	5.1.1 Roof_ConcreteSuspendedSI ab_Tower	Roof Width (ft)	672.98	672.98
					Span (ft)	12.5	12.5
					Concr ete (psi)	-	4000
					Concr ete flyash %	-	average
					Life Load (psf)	27	45
				Insulation	Categ ory	-	4-Ply Built-up Asphalt Roof System - Inverted
					Materi al	Rigid Insulation	Extrude d Polystyr ene, Glass Felt
					Thickn ess (in)	1	6
				Vapour Barrier	Categ ory	Vapour Barrier	Vapour Barrier
					Materi al	-	Polyeth ylene 5 mil
					Thickn ess (in)	-	-

A31 Walls Below Grade	1049. 674	m^ 2					
			Walls	2.1.1 Wall_Cast-In- Place_W1_Ext_BrickClad_B aseament_10"	Length (ft)	453.73	567.16
					Height (ft)	12	12
					Thickn ess (in)	10	8
					Concr ete (psi)	-	4000
					Concr ete flyash %	-	average
					Rebar	#5	#5
					Categ ory	Plaster	Gypsum Board
					Materi al	Plaster	Gypsum Regular
					Thickn ess (in)	-	0.5
					Categ ory	Insulation	Insulatio n
					Materi al	Styrofoam	Polystyr ene Extrude d

					Thickn ess (in)	1	1
					Categ ory	Vapour Barrier	Vapour Barrier
					Materi al	-	Polyeth ylene 6 mil
					Thickn ess (in)	-	-
					Categ ory	Cladding	Claddin g
					Materi al	Norman Glazed Brick	Brick - Ontario (standar d)
					Thickn ess (in)	4.75	-
					Categ ory	Paint	Paint
					Materi al	-	Alkyd Solvent Based
					Thickn ess (in)	-	-
				2.1.2 Wall_Cast-In- Place_W1_Ext_BrickClad_B aseament_11.75"	Length (ft)	29	28.4
					Height (ft)	12	12
					Thickn ess (in)	11.75	12
					Concr ete	-	4000

					(psi)		
					Concrete flyash %	-	average
					Rebar	#5	#5
					Category	Plaster	Gypsum Board
					Material	Plaster	Gypsum Regular
					Thickness (in)	-	0.5
					Category	Insulation	Insulation
					Material	Styrofoam	Polystyrene Extruded
					Thickness (in)	1	1
					Category	Vapour Barrier	Vapour Barrier
					Material	-	Polyethylene 6 mil
					Thickness (in)	-	-
					Category	Cladding	Cladding
					Material	Norman Glazed Brick	Brick - Ontario (standard)
					Thickness (in)	4.75	-
					Category	Paint	Paint

					ory		
					Material	-	Alkyd Solvent Based
					Thickn ess (in)	-	-
				2.1.3 Wall_Cast-In- Place_W1_Int_Basement_10 "	Length (ft)	157.75	197.19
					Height (ft)	12	12
					Thickn ess (in)	10	8
					Concr ete (psi)	-	4000
					Concr ete flyash %	-	average
					Rebar	#5	#5
					Numb er of Doors	4	4
					Door Type	Solid Wood Door	Solid Wood Door
				2.1.4 Wall_Cast-In- Place_W1_Int_Basement_8"	Length (ft)	301.07	301.07
					Height (ft)	12	12

					Thickn ess (in)	8	8
					Concr ete (psi)	-	4000
					Concr ete flyash %	-	average
					Rebar	#5	#5
					Numb er of Doors	7	7
					Door Type	Solid Wood Door	Solid Wood Door
A32 Walls Above Grade	2111. 86	m^ 2					
			Walls	2.1.5 Wall_Cast-In- Place_W2_Ext_BrickClad_Gr ndFlr_10"	Lengt h (ft)	336.67	420.84
					Height (ft)	12	12
					Thickn ess (in)	10	8
					Concr ete (psi)	-	4000
					Concr ete flyash %	-	average
					Rebar	#5	#5
					Numb er of Windo ws	9	9

					Total Window Area (ft2)	501.99	501.99
					Frame Type	Fixed, Aluminum Frame	Fixed, Aluminum Frame
					Glazing Type	-	Standard Glazing
					Category	Plaster	Gypsum Board
					Material	Plaster	Gypsum Regular
					Thickness (in)	-	0.5
					Category	Insulation	Insulation
					Material	Styrofoam	Polystyrene Extruded
					Thickness (in)	1	1
					Category	Vapour Barrier	Vapour Barrier
					Material	-	Polyethylene 6 mil
					Thickness (in)	-	-
					Category	Cladding	Cladding
					Material	Norman Glazed Brick	Brick - Ontario (standard)
					Thickness (in)	4.75	-
					Category	Paint	Paint

					ory		
					Material	-	Alkyd Solvent Based
					Thickn ess (in)	-	-
				2.1.6 Wall_Cast-In- Place_W2_Ext_BrickClad_Gr ndFlr_11.75"	Length (ft)	38.13	37.34
					Height (ft)	12	12
					Thickn ess (in)	11.75	12
					Concr ete (psi)	-	4000
					Concr ete flyash %	-	average
					Rebar	#5	#5
					Categ ory	Plaster	Gypsum Board
					Materi al	Plaster	Gypsum Regular
					Thickn ess (in)	-	0.5
					Categ ory	Insulation	Insulatio n
					Materi al	Styrofoam	Polystyr ene Extrude d
					Thickn ess (in)	1	1
					Categ ory	Vapour Barrier	Vapour Barrier
					Materi al	-	Polyeth ylen 6 mil

					Thickn ess (in)	-	-
					Categ ory	Cladding	Claddin g
					Materi al	Norman Glazed Brick	Brick - Ontario (standar d)
					Thickn ess (in)	4.75	-
					Categ ory	Paint	Paint
					Materi al	-	Alkyd Solvent Based
					Thickn ess (in)	-	-
				2.1.7 Wall_Cast-In-Place- W2_Ext_GrndFlr_8"	Len ^g th (ft)	156.97	156.97
					Height (ft)	12	12
					Thickn ess (in)	8	8
					Concr ete (psi)	-	4000
					Concr ete flyash %	-	average
					Rebar	#5	#5
					Numb er of Windo ws	7	7
					Total Windo w Area (ft2)	440.72	440.72

					Frame Type	Fixed, Aluminum Frame	Fixed, Aluminum Frame
					Glazing Type	-	Standard Glazing
					Category	Plaster	Gypsum Board
					Material	Plaster	Gypsum Regular
					Thickness (in)	-	0.5
					Category	Insulation	Insulation
					Material	Styrofoam	Polystyrene Extruded
					Thickness (in)	1	1
					Category	Vapour Barrier	Vapour Barrier
					Material	-	Polyethylene 6 mil
					Thickness (in)	-	-
				2.1.8 Wall_Cast-In-Place_W2_Ext_Grndflr_AdditionalWall	Length (ft)	175.81	175.81
					Height (ft)	4	4
					Thickness (in)	12	12
					Concrete (psi)	-	4000
					Concrete flyash	-	average

					%		
					Rebar	#5	#5
				2.1.13 Wall_Cast-In-Place_W3_Ext_BrickClad_TypeFlr_10"	Length (ft)	281.83	1056.87
					Height (ft)	12	12
					Thickness (in)	10	8
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
					Number of Windows	13	39
					Total Window Area (ft2)	570.2	1710.6
					Frame Type	Fixed, Aluminum Frame	Fixed, Aluminum Frame
					Glazing Type	-	Standard Glazing
					Category	Plaster	Gypsum Board
					Material	Plaster	Gypsum Regular
					Thickness (in)	-	0.5
					Category	Insulation	Insulation

					Material	Styrofoam	Polystyrene Extruded
					Thickness (in)	1	1
					Category	Vapour Barrier	Vapour Barrier
					Material	-	Polyethylene 6 mil
					Thickness (in)	-	-
					Category	Cladding	Cladding
					Material	Norman Glazed Brick	Brick - Ontario (standard)
					Thickness (in)	4.75	-
					Category	Paint	Paint
					Material	-	Alkyd Solvent Based
					Thickness (in)	-	-
				2.1.14 Wall_Cast-In-Place_W3_Ext_BrickClad_TypeFlr_7.5"	Length (ft)	32.92	92.58
					Height (ft)	12	12
					Thickness (in)	7.5	8
					Concrete (psi)	-	4000

					Concrete flyash %	-	average
					Rebar	#5	#5
					Category	Plaster	Gypsum Board
					Material	Plaster	Gypsum Regular
					Thickness (in)	-	0.5
					Category	Insulation	Insulation
					Material	Styrofoam	Polystyrene Extruded
					Thickness (in)	1	1
					Category	Vapour Barrier	Vapour Barrier
					Material	-	Polyethylene 6 mil
					Thickness (in)	-	-
					Category	Cladding	Cladding
					Material	Norman Glazed Brick	Brick - Ontario (standard)
					Thickness (in)	4.75	-
					Category	Paint	Paint
					Material	-	Alkyd Solvent Based
					Thickness (in)	-	-

				2.1.15 Wall_Cast-In-Place_W3_Ext_Brickclad_TypeFlr_8"	Length (ft)	93.48	280.44
					Height (ft)	12	12
					Thickness (in)	8	8
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
					Number of Windows	6	18
					Total Window Area (ft2)	341	1023
					Frame Type	Fixed, Aluminum Frame	Fixed, Aluminum Frame
					Glazing Type	-	Standard Glazing
					Category	Plaster	Gypsum Board
					Material	Plaster	Gypsum Regular
					Thickness (in)	-	0.5
					Category	Insulation	Insulation
					Material	Styrofoam	Polystyrene Extruded

					Thickn ess (in)	1	1
					Categ ory	Vapour Barrier	Vapour Barrier
					Materi al	-	Polyeth ylene 6 mil
					Thickn ess (in)	-	-
					Categ ory	Cladding	Claddin g
					Materi al	Norman Glazed Brick	Brick - Ontario (standar d)
					Thickn ess (in)	4.75	-
					Categ ory	Paint	Paint
					Materi al	-	Alkyd Solvent Based
					Thickn ess (in)	-	-
				2.1.19 Wall_Cast-In- Place_W4_Ext_BrickClad_S econdFlr_10"	Lengt h (ft)	280.08	350.1
					Height (ft)	12	12
					Thickn ess (in)	10	8
					Concr ete (psi)	-	4000
					Concr ete flyash %	-	average
					Rebar	#5	#5

					Number of Windows	13	13
					Total Window Area (ft2)	570.2	570.2
					Frame Type	Fixed, Aluminum Frame	Fixed, Aluminum Frame
					Glazing Type	-	Standard Glazing
					Category	Plaster	Gypsum Board
					Material	Plaster	Gypsum Regular
					Thickness (in)	-	0.5
					Category	Insulation	Insulation
					Material	Styrofoam	Polystyrene Extruded
					Thickness (in)	1	1
					Category	Vapour Barrier	Vapour Barrier
					Material	-	Polyethylene 6 mil
					Thickness (in)	-	-
					Category	Cladding	Cladding
					Material	Norman Glazed Brick	Brick - Ontario (standard)
					Thickness (in)	4.75	-

					Category	Paint	Paint
					Material	-	Alkyd Solvent Based
					Thickness (in)	-	-
				2.1.20 Wall_Cast-In-Place_W4_Ext_BrickClad_SecondFlr_7.5	Length (ft)	194.53	182.37
					Height (ft)	12	12
					Thickness (in)	7.5	8
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
					Number of Windows	6	6
					Total Window Area (ft2)	373.08	373.08
					Frame Type	Fixed, Aluminum Frame	Fixed, Aluminum Frame
					Glazing Type	-	Standard Glazing
					Category	Plaster	Gypsum Board
					Material	Plaster	Gypsum Regular

					Thickn ess (in)	-	0.5
					Categ ory	Insulation	Insulatio n
					Materi al	Styrofoam	Polystyr ene Extrude d
					Thickn ess (in)	1	1
					Categ ory	Vapour Barrier	Vapour Barrier
					Materi al	-	Polyeth ylene 6 mil
					Thickn ess (in)	-	-
					Categ ory	Cladding	Claddin g
					Materi al	Norman Glazed Brick	Brick - Ontario (standar d)
					Thickn ess (in)	4.75	-
					Categ ory	Paint	Paint
					Materi al	-	Alkyd Solvent Based
					Thickn ess (in)	-	-
				2.1.21 Wall_Cast-In- Place_W4_Ext_BrickClad_S econdFlr_8"	Length (ft)	93.5	93.5
					Height (ft)	12	12
					Thickn ess	8	8

					(in)		
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
					Number of Windows	6	6
					Total Window Area (ft2)	341	341
					Frame Type	Fixed, Aluminum Frame	Fixed, Aluminum Frame
					Glazing Type	-	Standard Glazing
					Category	Plaster	Gypsum Board
					Material	Plaster	Gypsum Regular
					Thickness (in)	-	0.5
					Category	Insulation	Insulation
					Material	Styrofoam	Polystyrene Extruded
					Thickness (in)	1	1
					Category	Vapour Barrier	Vapour Barrier
					Material	-	Polyethylene 6 mil
					Thickness (in)	-	-

					Category	Cladding	Cladding
					Material	Norman Glazed Brick	Brick - Ontario (standard)
					Thickness (in)	4.75	-
					Category	Paint	Paint
					Material	-	Alkyd Solvent Based
					Thickness (in)	-	-
				2.1.24 Wall_Cast-In-Place_W5_Ext_BrickClad_Penthouse_7.5"	Length (ft)	33.17	31.1
					Height (ft)	12	12
					Thickness (in)	7.5	8
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
					Category	Plaster	Gypsum Board
					Material	Plaster	Gypsum Regular
					Thickness (in)	-	0.5
					Category	Insulation	Insulation

					Material	Styrofoam	Polystyrene Extruded
					Thickness (in)	1	1
					Category	Vapour Barrier	Vapour Barrier
					Material	-	Polyethylene 6 mil
					Thickness (in)	-	-
					Category	Cladding	Cladding
					Material	Norman Glazed Brick	Brick - Ontario (standard)
					Thickness (in)	4.75	-
					Category	Paint	Paint
					Material	-	Alkyd Solvent Based
					Thickness (in)	-	-
				2.1.25 Wall_Cast-In-Place_W5_Ext_BrickClad_Penthouse_8"	Length (ft)	294.44	294.44
					Height (ft)	12	12
					Thickness (in)	8	8
					Concrete (psi)	-	4000

					Concrete flyash %	-	average
					Rebar	#5	#5
					Number of Windows	18	18
					Total Window Area (ft2)	1003.14	1003.14
					Frame Type	Fixed, Aluminum Frame	Fixed, Aluminum Frame
					Glazing Type	-	Standard Glazing
					Category	Plaster	Gypsum Board
					Material	Plaster	Gypsum Regular
					Thickness (in)	-	0.5
					Category	Insulation	Insulation
					Material	Styrofoam	Polystyrene Extruded
					Thickness (in)	1	1
					Category	Vapour Barrier	Vapour Barrier
					Material	-	Polyethylene 6 mil
					Thickness (in)	-	-
					Category	Cladding	Cladding

					Material	Norman Glazed Brick	Brick - Ontario (standard)
					Thickness (in)	4.75	-
					Category	Paint	Paint
					Material	-	Alkyd Solvent Based
					Thickness (in)	-	-
B11 Partitions	990.1639	m ²					
			Walls	2.1.9 Wall_Cast-In-Place_W2_Int_Grndflr_10"	Length (ft)	91.67	114.59
					Height (ft)	12	12
					Thickness (in)	10	8
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
					Number of Doors	4	4
					Door Type	Solid Wood Door	Solid Wood Door

				2.1.10 Wall_Cast-In-Place_W2_Int_GrndFlr_6"	Length (ft)	73.22	54.92
					Height (ft)	12	12
					Thickness (in)	6	8
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
				2.1.11 Wall_Cast-In-Place_W2_Int_GrndFlr_7.5"	Length (ft)	28.08	26.33
					Height (ft)	12	12
					Thickness (in)	7.5	8
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
				2.1.12 Wall_Cast-In-Place_W2_Int_GrndFlr_8"	Length (ft)	260.48	260.48
					Height (ft)	12	12
					Thickness (in)	8	8

					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
					Number of Doors	7	7
					Door Type	Solid Wood Door	Solid Wood Door
				2.1.16 Wall_Cast-In-Place_W3_Int_TypFlr_10"	Length (ft)	101.47	380.52
					Height (ft)	12	12
					Thickness (in)	10	8
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
					Number of Doors	14	42
					Door Type	Solid Wood Door	Solid Wood Door
				2.1.17 Wall_Cast-In-Place_W3_Int_TypFlr_5.75"	Length (ft)	54.26	117
					Height (ft)	12	12
					Thickness (in)	5.75	8

					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
					Number of Windows	6	18
					Total Window Area (ft2)	373.08	1119.24
					Frame Type	Fixed, Aluminum Frame	Fixed, Aluminum Frame
					Glazing Type	-	Standard Glazing
				2.1.18 Wall_Cast-In-Place_W3_Int_TypFlr_8"	Length (ft)	89.83	269.49
					Height (ft)	12	12
					Thickness (in)	8	8
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
					Number of Doors	7	21
					Door Type	Solid Wood Door	Solid Wood Door

				2.1.22 Wall_Cast-In-Place_W4_Int_SecondFlr_10"	Length (ft)	101.08	126.35
					Height (ft)	12	12
					Thickness (in)	10	8
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
					Number of Doors	8	8
					Door Type	Solid Wood Door	Solid Wood Door
				2.1.23 Wall_Cast-In-Place_W4_Int_SecondFlr_8"	Length (ft)	88.08	88.08
					Height (ft)	12	12
					Thickness (in)	8	8
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
					Number of Doors	7	7

					Door Type	Solid Wood Door	Solid Wood Door
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HEBB Theatre Inputs

Element	Quantity	Units	Assembly Type	Assembly Name	Input Fields	Known/Measured Information	IE Inputs
A11 Foundations	147.1 752	m ² 2					
			Footing	1.2.1 Footing_L01&02_Lobby	Length (ft)	47.83	47.83
					Width (ft)	2	2.58
					Thickness (in)	24.5	19
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5
				1.2.2 Footing_L03a&05a_Lobby	Length (ft)	58	58
					Width (ft)	5	5
					Thickness (in)	18	18
					Concrete (psi)	-	4000
					Concrete flyash %	-	average
					Rebar	#5	#5

1.2.3 Footing_L03b_Lobby	Length (ft)	21.17	21.17
	Width (ft)	2	2
	Thickn ess (in)	18	18
	Concr ete (psi)	-	4000
	Concr ete flyash %	-	average
	Rebar	#5	#5
1.2.4 Footing_L04_Lobby	Length (ft)	77.75	77.75
	Width (ft)	2	6.32
	Thickn ess (in)	60	19
	Concr ete (psi)	-	4000
	Concr ete flyash %	-	average
	Rebar	#5	#5
1.2.5 Footing_L05b&14_Lobby	Length (ft)	52.75	52.75
	Width (ft)	2	2
	Thickn ess (in)	12	12
	Concr ete (psi)	-	4000
	Concr ete flyash %	-	average

	Rebar	#5	#5
1.2.6 Footing_L06a_Lobby	Length (ft)	20	20
	Width (ft)	3	3
	Thickn ess (in)	12	12
	Concr ete (psi)	-	4000
	Concr ete flyash %	-	average
	Rebar	#5	#5
1.2.7 Footing_L06b_Lobby	Length (ft)	18.25	18.25
	Width (ft)	5	5
	Thickn ess (in)	18	18
	Concr ete (psi)	-	4000
	Concr ete flyash %	-	average
	Rebar	#5	#5
1.2.8 Footing_L08_Lobby_1'x1'6"	Length (ft)	247.48	247.48
	Width (ft)	1.5	1.5
	Thickn ess (in)	12	12
	Concr ete (psi)	-	4000
	Concr ete flyash	-	average

		%	
	Rebar	#5	#5
1.2.9 Footing_L12_Lobby	Length (ft)	32.08	32.08
	Width (ft)	7.833333	6.26
	Thickn ess (in)	6	7.5
	Concr ete (psi)	-	4000
	Concr ete flyash %	-	average
	Rebar	#5	#5
1.2.10 Footing_LA_Lobby	Length (ft)	10.92	10.92
	Width (ft)	5.5	5.5
	Thickn ess (in)	18	18
	Concr ete (psi)	-	4000
	Concr ete flyash %	-	average
	Rebar	#5	#5
1.2.11 Footing_LB_Lobby	Length (ft)	7.92	7.92
	Width (ft)	4	4
	Thickn ess (in)	18	18
	Concr ete (psi)	-	4000

	Concrete flyash %	-	average
	Rebar	#5	#5
1.2.12 Footing_LC_Lobby	Length (ft)	6.67	6.67
	Width (ft)	3.25	3.25
	Thickness (in)	18	18
	Concrete (psi)	-	4000
	Concrete flyash %	-	average
	Rebar	#5	#5
1.2.13 Footing_LD_Lobby	Length (ft)	4	4
	Width (ft)	2	2
	Thickness (in)	12	12
	Concrete (psi)	-	4000
	Concrete flyash %	-	average
	Rebar	#5	#5

A21	656.4	m^				
Lowest	604	2				
Floor						
Constru						
ction						
	SOG	1.1.1	SOG_5"_Lobby	Length (ft)	84.06	84.06
				Width (ft)	84.06	84.06
				Thickn ess (in)	5	4
				Concr ete (psi)	-	4000
				Concr ete flyash %	-	average
A22	1094.	m^				
Upper	646	2				
Floor						
Constru						
ction						
	Stairs	1.2.14	Stairs_Theatre	Length (ft)	65.42	65.42
				Width (ft)	65.5	82.74
				Thickn ess (in)	24	19
				Concr ete (psi)	-	4000
				Concr ete flyash %	-	average
				Rebar	#5	#5

Column Beam	3.1.1 Column_Beam_Concrete_ Lobby	Number of Columns	10	10
		Number of Beams	10	10
		Bay sizes (ft)	20.83333	20.83
		Suppo rted span (ft)	14.25	14.25
		Floor to floor height (ft)	10.5	10.5
		Live load (psf)	60, 100	75
	3.1.2 Column_Beam_Concrete_ Theatre	Number of Columns	12	12
		Number of Beams	32	32
		Bay sizes (ft)	21	21
		Suppo rted span (ft)	9.5	9.5
		Floor to floor height (ft)	26	26
		Live load (psf)	60, 100	75

			Suspen ded Floor	4.1.1 Floor_ConcreteSuspended Slab_Theatre	Floor Width (ft)	789.2284	789.228 4
					Span (ft)	9.5	9.5
					Concr ete (psi)	-	4000
					Concr ete flyash %	-	average
					Life load (psf)	60, 100	75
A23 Roof Constru ction	629.1 085	m^ 2					
			Suspen ded Slab	5.1.1 Roof_ConcreteSuspended Slab_Theatre	Roof Width (ft)	497.7644	497.764 4
					Span (ft)	13.60417	13.6041 7
					Concr ete (psi)	-	4000
					Concr ete flyash %	-	average
					Life load (psf)	27	45

				Category	-	4-Ply Built-up Asphalt Roof System - Inverted
				Material	Rigid Insulation	Extruded Polystyrene, Glass Felt
				Thickness (in)	1	6
				Category	Vapour Barrier	Vapour Barrier
				Material	-	Polyethylene 6 mil
				Thickness	-	-
A31 Walls Below Grade						
A32 Walls Above Grade	1610.797	m^2				
			Walls	2.1.1 Wall_Cast-In-Place_L01_Lobby_8"	Length (ft)	34.54
						34.54

	Height (ft)	17.3125	17.3125
	Thickness (in)	8	8
	Concrete (psi)	-	4000
	Concrete flyash %	-	average
	Rebar	#5	#5
2.1.2 Wall_Cast-In-Place_L02_Lobby_8"	Length (ft)	14.17	14.17
	Height (ft)	14.63542	14.63542
	Thickness (in)	8	8
	Concrete (psi)	-	4000
	Concrete flyash %	-	average
	Rebar	#5	#5
2.1.3 Wall_Cast-In-Place_L03a_Lobby_8"	Length (ft)	39.58	39.58
	Height (ft)	25.5	25.5

	Thickn ess (in)	8	8
	Concr ete (psi)	-	4000
	Concr ete flyash %	-	average
	Rebar	#5	#5
2.1.4 Wall_Cast-In- Place_L03b_Lobby_8"	Length (ft)	5.92	5.92
	Height (ft)	25.5	25.5
	Thickn ess (in)	8	8
	Concr ete (psi)	-	4000
	Concr ete flyash %	-	average
	Rebar	#5	#5
2.1.5 Wall_Cast-In- Place_L04_Lobby_8"	Length (ft)	81.4	81.4
	Height (ft)	16.47917	16.5

	Thickn ess (in)	8	8
	Concr ete (psi)	-	4000
	Concr ete flyash %	-	average
	Rebar	#5	#5
2.1.6 Wall_Cast-In- Place_L05_Lobby_1'8"	Length (ft)	4.75	7.92
	Height (ft)	10.25	10.3
	Thickn ess (in)	20	12
	Concr ete (psi)	-	4000
	Concr ete flyash %	-	average
	Rebar	#5	#5
2.1.7 Wall_Cast-In- Place_L06_Lobby_1'8"	Length (ft)	6.58	11
	Height (ft)	10.25	10.3

	Thickn ess (in)	20	12
	Concr ete (psi)	-	4000
	Concr ete flyash %	-	average
	Rebar	#5	#5
2.1.8 Wall_Cast-In- Place_L07_Lobby_8"	Length (ft)	42.72	42.72
	Height (ft)	18.25	18.3
	Thickn ess (in)	8	8
	Concr ete (psi)	-	4000
	Concr ete flyash %	-	average
	Rebar	#5	#5
2.1.9 Wall_Cast-In- Place_L08_Lobby_6"	Length (ft)	24.81	18.61
	Height (ft)	12	12
	Thickn ess (in)	6	8

	Concrete (psi)	-	4000
	Concrete flyash %	-	average
	Rebar	#5	#5
2.1.10 Wall_Cast-In-Place_L09-10_Lobby_8"	Length (ft)	113.12	113.12
	Height (ft)	12	12
	Thickness (in)	8	8
	Concrete (psi)	-	4000
	Concrete flyash %	-	average
	Rebar	#5	#5
2.1.11 Wall_Cast-In-Place_L11_Lobby_10"	Length (ft)	42.32	52.9
	Height (ft)	12	12
	Thickness (in)	10	8

	Concrete (psi)	-	4000
	Concrete flyash %	-	average
	Rebar	#5	#5
2.1.12 Wall_Cast-In-Place_L12a_Lobby_8"	Length (ft)	38	38
	Height (ft)	3	3
	Thickness (in)	8	8
	Concrete (psi)	-	4000
	Concrete flyash %	-	average
	Rebar	#5	#5
2.1.13 Wall_Cast-In-Place_L12b_Lobby_8"	Length (ft)	31.92	31.92
	Height (ft)	4.5	4.5
	Thickness (in)	8	8
	Concrete	-	4000

	(psi)		
	Concrete flyash %	-	average
	Rebar	#5	#5
2.1.14 Wall_Cast-In-Place_L13_Lobby_10"	Length (ft)	27.5	34.38
	Height (ft)	10.3	10.3
	Thickness (in)	10	8
	Concrete (psi)	-	4000
	Concrete flyash %	-	average
	Rebar	#5	#5
2.1.15 Wall_Cast-In-Place_L14_Lobby_11.75"	Length (ft)	89.57	87.7
	Height (ft)	10.3	10.3
	Thickness (in)	11.75	12
	Concrete (psi)	-	4000
	Concrete flyash %	-	average
	Rebar	#5	#5

2.1.16 Wall_Cast-In-Place_W6_Ext_BrickClad_Theatre_8"	Length (ft)	365.74	365.74
	Height (ft)	26	26
	Thickness (in)	8	8
	Concrete (psi)	-	4000
	Concrete flyash %	-	average
	Rebar	#5	#5
	Number of Doors	2	2
	Door Type	Steel Exterior Door	Steel Exterior Door
	Category	Plaster	Gypsum Board
	Material	Plaster	Gypsum Regular
	Thickness (in)	-	0.5
	Category	Insulation	Insulation
	Material	Styrofoam	Polystyrene Extrude

				d
		Thickn ess (in)	1	1
		Categ ory	Vapour Barrier	Vapour Barrier
		Materi al	-	Polyethy lene 6 mil
		Thickn ess (in)	-	-
		Categ ory	Cladding	Claddin g
		Materi al	Norman Glazed Brick	Brick - Ontario (standar d)
		Thickn ess (in)	4.75	-
		Categ ory	Paint	Paint
		Materi al	-	Alkyd Solvent Based
		Thickn ess (in)	-	-
B11 Partitions	305.9 686	m [^] 2		

Walls	2.1.17 Wall_Cast-In-Place_W6_Int_Theatre_6"	Length (ft)	51.75	38.81
		Height (ft)	26	26
		Thickness (in)	6	8
		Concrete (psi)	-	4000
		Concrete flyash %	-	average
		Rebar	#5	#5
	2.1.18 Wall_Cast_In_Place_W6_Int_Theatre_8"	Length (ft)	74.92	74.92
		Height (ft)	26	26
		Thickness (in)	8	8
		Concrete (psi)	-	4000
		Concrete flyash %	-	average
		Rebar	#5	#5

HEBB TOWER Assumptions

Element	Assembly Type	Assembly Name	Assumptions
A11 Foundations			

	Footing	1.2.1 Footing_F1a_Basement	<p>The width of this slab was adjusted to accommodate the Impact Estimator limitation of footing thicknesses to be under 19.7". The measured length was maintained, thicknesses were set at 19" and the widths were increased using the following calculations;</p> $= [(Cited Width) \times (Cited Thickness)] / (19"/12)$ $= [(2') \times (80"/12)] / (19"/12)$ $= 8.42 \text{ feet}$ <p>The height from the bottom of the footing to the top of the footing, at an elevation of 365'3", is taken to be 6'8", as determined from measuring the structural drawings.</p>
		1.2.2 Footing_F1b_Basement	<p>The depth of this deep mass concrete footing was taken to be 1'0".</p>

		<p>1.2.3 Footing_F2a_Basement</p>	<p>The width of this slab was adjusted to accommodate the Impact Estimator limitation of footing thicknesses to be under 19.7". The measured length was maintained, thicknesses were set at 19" and the widths were increased using the following calculations;</p> $= [(Cited Width) \times (Cited Thickness)] / (19"/12)$ $= [(2.5') \times (80"/12)] / (19"/12)$ $= 10.53 \text{ feet}$ <p>The height from the bottom of the footing to the top of the footing, at an elevation of 365'3", is taken to be 6'8", as determined from measuring the structural drawings.</p>

		1.2.6 Footing_FB_Basement	
		1.2.7 Footing_FC_Basement	
		1.2.8 Footing_FD_Basement	

		<p>1.2.11 Footing_FG_Basement</p>	<p>Dimensions of the L-shaped footing determined from having a cross-sectional footing area of 12sf, setting thickness to 6'8", and from this calculating width to be 1.8' (from structural drawing).</p> <p>The width of this slab was adjusted to accommodate the Impact Estimator limitation of footing thicknesses to be under 19.7". The measured length was maintained, thicknesses were set at 19" and the widths were increased using the following calculations;</p> <p>= [(Cited Width) x (Cited Thickness)] / (19"/12)</p> <p>= [(1.8') x (80"/12)] / (19"/12)</p> <p>= 7.58 feet</p>

		<p>1.2.12 Footing_FH_Basement</p>	<p>Dimensions of the L-shaped footing determined from having a cross-sectional footing area of 10sf, setting thickness to 6'8", and from this calculating width to be 1.5' (from structural drawing).</p> <p>The width of this slab was adjusted to accommodate the Impact Estimator limitation of footing thicknesses to be under 19.7". The measured length was maintained, thicknesses were set at 19" and the widths were increased using the following calculations;</p> <p>= [(Cited Width) x (Cited Thickness)] / (19"/12)</p> <p>= [(1.5') x (80"/12)] / (19"/12)</p> <p>= 6.32 feet</p>
		<p>1.2.13 Footing_FJ_Basement</p>	
		<p>1.2.14 Footing_FK_Basement</p>	

		1.2.15 Footing_FL_Basement	

A21 Lowest Floor Construction			<p>The Impact Estimator, SOG inputs are limited to being either a 4" or 8" thickness. Since the actual SOG thicknesses for the HEBB building were not exactly 4" or 8" thick, the areas measured in OnScreen required calculations to adjust the areas to accommodate this limitation.</p> <p>The Impact Estimator limits the thickness of footings to be between 7.5" and 19.7" thick. As there are a number of cases where footing thicknesses are not within these limitations, their widths were adjusted accordingly to maintain the same volume of footing. Concrete strength was set to 4000psi and an average % of concrete flyash was assumed. Lastly, the North and South concrete staircases were modelled as footings.</p>
	SOG	1.1.1 SOG_5"_Tower	<p>The area of this slab had to be adjusted so that the thickness fit into the 4" thickness specified in the Impact Estimator. The following calculation was done in order to determine appropriate Length and Width (in feet) inputs for this slab;</p> $= \text{sqrt}[\frac{(\text{Measured Slab Area}) \times (\text{Actual Slab Thickness})}{(4"/12)}]$ $= \text{sqrt}[(10,695.07 \times (5"/12))/(4"/12)]$ $= 115.62 \text{ feet}$

	Stairs	1.2.18 Stairs_South/North_Platform	<p>The width of this slab was adjusted to accommodate the Impact Estimator limitation of footing thicknesses to be greater than 7.5". The measured length was maintained, thickness was set to 7.5" and the width was decreased using the following calculation;</p> $= [(Cited Width) \times (Cited Thickness)] / (7.5"/12)$ $= [(5.33') \times (6"/12)] / (7.5"/12)$ $= 4.26 \text{ feet}$

	Column Beam	3.1.1 Column_Beam_Concrete Basement	<p>It is modeled as if there are columns located along the load bearing wall along line B in the same fashion as the columns along line A (refer to structural drawings), even though they are not shown on the structural drawings.</p> <p>Since the bay size is limited to a maximum of 40 feet in the Impact Estimator, 40 feet is used as the approximate bay size, whereas the actual bay size is 41.5 feet.</p>

		3.1.2 Column_Beam_Concrete_GrndFlr	<p>It is modeled as if there are columns located along the load bearing wall along line B in the same fashion as the columns along line A (refer to structural drawings), even though they are not shown on the structural drawings.</p> <p>Since the bay size is limited to a maximum of 40 feet in the Impact Estimator, 40 feet is used as the approximate bay size, whereas the actual bay size is 41.5 feet.</p>

		3.1.3 Column_Beam_Concrete_SecondFlr	<p>It is modeled as if there are columns located along the load bearing wall along line B in the same fashion as the columns along line A (refer to structural drawings), even though they are not shown on the structural drawings.</p> <p>Since the bay size is limited to a maximum of 40 feet in the Impact Estimator, 40 feet is used as the approximate bay size, whereas the actual bay size is 41.5 feet.</p>

		<p>3.1.4 Column_Beam_Concrete_typFlr</p>	<p>It is modeled as if there are columns located along the load bearing wall along line B in the same fashion as the columns along line A (refer to structural drawings), even though they are not shown on the structural drawings.</p> <p>Since the bay size is limited to a maximum of 40 feet in the Impact Estimator, 40 feet is used as the approximate bay size, whereas the actual bay size is 41.5 feet.</p> <p>Typical Floor (TypFlr) values for number of columns and beams, were multiplied by 3 for EIE inputs to represent all typical floors (typical floor = 3rd, 4th, and 5th floors).</p>

	Suspended Floor	4.1.1 Floor_ConcreteSuspendedSlab_GrndFlr	<p>The Impact Estimator calculated the thickness of the material based on floor width, span, concrete strength, concrete flyash content and live load. Concrete strength was set to 4000psi and an average % of concrete flyash was assumed. As stated on the structural drawings, the live loads for floors are as follows: labs, classrooms, and theatre have specified live loads of 60psf; corridors, entrances, and stairs have specified live loads of 100psf. An average of these values of 75psf is used for EIE Inputs.</p> <p>Typical Floor (TypFlr) value for floor width was multiplied by 3 for EIE input to represent all typical floors (typical floor = 3rd, 4th, and 5th floors).</p> <p>All stated about roof envelope from architectural drawings is that it is comprised of 1" rigid insulation. For EIE Model, it is assumed to have a 4-Ply Built-up Asphalt Roof System - Inverted with Extruded Polystyrene, Glass Felt envelope material. Vapour barrier assumed to be polyethylene 6mil.</p>

		4.1.2 Floor_ConcreteSuspendedSlab_SecondFir	
		4.1.3 Floor_ConcreteSuspendedSlab_TypeFir	

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		4.1.4 Floor_ConcreteSuspendedSlab_Penthouse	

A23 Roof Construction

The live load was assumed to be 45 psf instead of the specified 27 psf and the concrete strength was set to 4,000psi with average flyash content. All stated about roof envelope from architectural drawings is that it is comprised of 1" rigid insulation. For EIE Model, it is assumed to have a 4-Ply Built-up Asphalt Roof System - Inverted with Extruded Polystyrene, Glass Felt envelope material. Vapour barrier assumed to be polyethylene 6mil.

	Envelope	5.1.1 Roof_ConcreteSuspendedSlab_Tower	
		Insulation	
		Vapour Barrier	

A31 Walls Below Grade

The length of the concrete cast-in-place walls needed adjusting to accommodate the wall thickness limitation in the Impact Estimator (8" or 12").

Concrete strength was set to 4000psi and an average % of concrete flyash was assumed.

The wall envelopes consisting of plaster are modelled as consisting of Regular Gypsum 1/2" due to the unavailability of plaster as a material in Athena EIE.

The vapour barrier is assumed to be Polyethylene 6 mil.

For the external walls of the tower, the exterior envelope consists of 4.75" Norman Glazed Brick on 90% of the height of the wall, and 3.75" concrete cladding on 10% of the height of the wall. For the model to be inputted into Athena EIE, it is assumed that the exterior envelope consists of Standard Ontario Brick on 100% of the height of the wall. The glazing on the Norman Brick is modeled as Alkyd Solvent Based Paint in Athena EIE.

Doors have an actual size of 36"x7', but are modeled assuming they are of standard size in Athena EIE of 32"x7'. Windows are modeled as standard glazing with fixed aluminum framing, which is the closest estimation to the observed windows.

Typical Floor (TypFlr) values for measured wall length, number of windows, window area, and number

			of doors, were multiplied by 3 for EIE inputs to represent all typical floors (typical floor = 3rd, 4th, and 5th floors).
	Walls	2.1.1 Wall_Cast-In-Place_W1_Ext_BrickClad_Basement_10"	<p>This wall was increased by a factor in order to fit the 8" thickness limitation of the Impact Estimator. This was done by increasing the length of the wall using the following equation;</p> $= (\text{Measured Length}) * [(\text{Cited Thickness})/8"]$ $= (453.73') * [(10")/8"]$ $= 567.16 \text{ feet}$

		<p>2.1.2 Wall_Cast-In-Place_W1_Ext_BrickClad_Basement_11.75"</p>	<p>This wall was reduced by a factor in order to fit the 12" thickness limitation of the Impact Estimator. This was done by reducing the length of the wall using the following equation;</p> $= (\text{Measured Length}) * [(\text{Cited Thickness})/12"]$ $= (29') * [(11.75")/12"]$ $= 28.40 \text{ feet}$

		2.1.19 Wall_Cast-In-Place_W4_Ext_BrickClad_SecondFlr_10"	This wall was increased by a factor in order to fit the 8" thickness limitation of the Impact Estimator. This was done by increasing the length of the wall using the following equation; = (Measured Length) * [(Cited Thickness)/8"] = (280.08') * [(10")/8"] = 350.10 feet

	Walls	2.1.9 Wall_Cast-In-Place_W2_Int_Grndflr_10"	<p>This wall was increased by a factor in order to fit the 8" thickness limitation of the Impact Estimator. This was done by increasing the length of the wall using the following equation;</p> $= (\text{Measured Length}) * [(\text{Cited Thickness})/8"]$ $= (91.67') * [(10")/8"]$ $= 114.59 \text{ feet}$

		<p>2.1.10 Wall_Cast-In-Place_W2_Int_GrndFlr_6"</p>	<p>This wall was reduced by a factor in order to fit the 8" thickness limitation of the Impact Estimator. This was done by reducing the length of the wall using the following equation;</p> $= (\text{Measured Length}) * [(\text{Cited Thickness})/8"]$ $= (73.22') * [(6")/8"]$ $= 54.92 \text{ feet}$

		<p>2.1.11 Wall_Cast-In-Place_W2_Int_GrndFlr_7.5"</p>	<p>This wall was reduced by a factor in order to fit the 8" thickness limitation of the Impact Estimator. This was done by reducing the length of the wall using the following equation;</p> $= (\text{Measured Length}) * [(\text{Cited Thickness})/8"]$ $= (28.08') * [(7.5")/8"]$ $= 26.33 \text{ feet}$
		<p>2.1.12 Wall_Cast-In-Place_W2_Int_GrndFlr_8"</p>	

		<p>2.1.17 Wall_Cast-In-Place_W3_Int_TypFlr_5.75"</p>	<p>This wall was reduced by a factor in order to fit the 8" thickness limitation of the Impact Estimator. This was done by reducing the length of the wall using the following equation;</p> $= (\text{Measured Length}) * [(\text{Cited Thickness})/8"]$ $= (54.26') * [(5.75")/8"]$ $= 39.00 \text{ feet}$ <p>Multiply by 3 (typical floor = floors 3,4,5);</p> $= 39.00' * 3$ $= 117.00 \text{ feet}$
		<p>2.1.18 Wall_Cast-In-Place_W3_Int_TypFlr_8"</p>	

		2.1.23 Wall_Cast-In-Place_W4_Int_SecondFlr_8"
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HEBB Theatre Assumption

Element	Assembly Type	Assembly Name	Assumption
A11	Foundations		

Footings 1.2.1 Footing_L01&02_Lobby

The width of this slab was adjusted to accommodate the Impact Estimator limitation of footing thicknesses to be under 19.7". The measured length was maintain, thicknesses were set at 19" and the widths were increased using the following calculations;

$$= [(Cited Width) \times (Cited Thickness)] / (19"/12)$$

$$= [(2') \times (24.5"/12)] / (19"/12)$$

$$= 2.58 \text{ feet}$$

1.2.2 Footing_L03a&05a_Lobby

1.2.3 Footing_L03b_Lobby

1.2.4 Footing_L04_Lobby

The width of this slab was adjusted to accommodate the Impact Estimator limitation of footing thicknesses to be under 19.7". The measured length was maintain, thicknesses were set at 19" and the widths were increased using the following calculations;

$$= [(Cited Width) \times (Cited Thickness)] / (19"/12)$$

$$= [(2') \times (60"/12)] / (19"/12)$$

$$= 6.32 \text{ feet}$$

1.2.5 Footing_L05b&14_Lobby

1.2.6 Footing_L06a_Lobby

1.2.7 Footing_L06b_Lobby

1.2.8 Footing_L08_Lobby_1'x1'6"

1.2.9 Footing_L12_Lobby

The width of this slab was adjusted to accommodate the Impact Estimator limitation of footing thicknesses to be greater than 7.5". The measured length was maintain, thicknesses were set at 7.5" and the widths were decreased using the following calculations;

$$= [(Cited Width) \times (Cited Thickness)] / (7.5"/12)$$

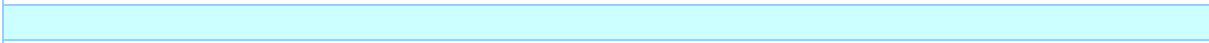
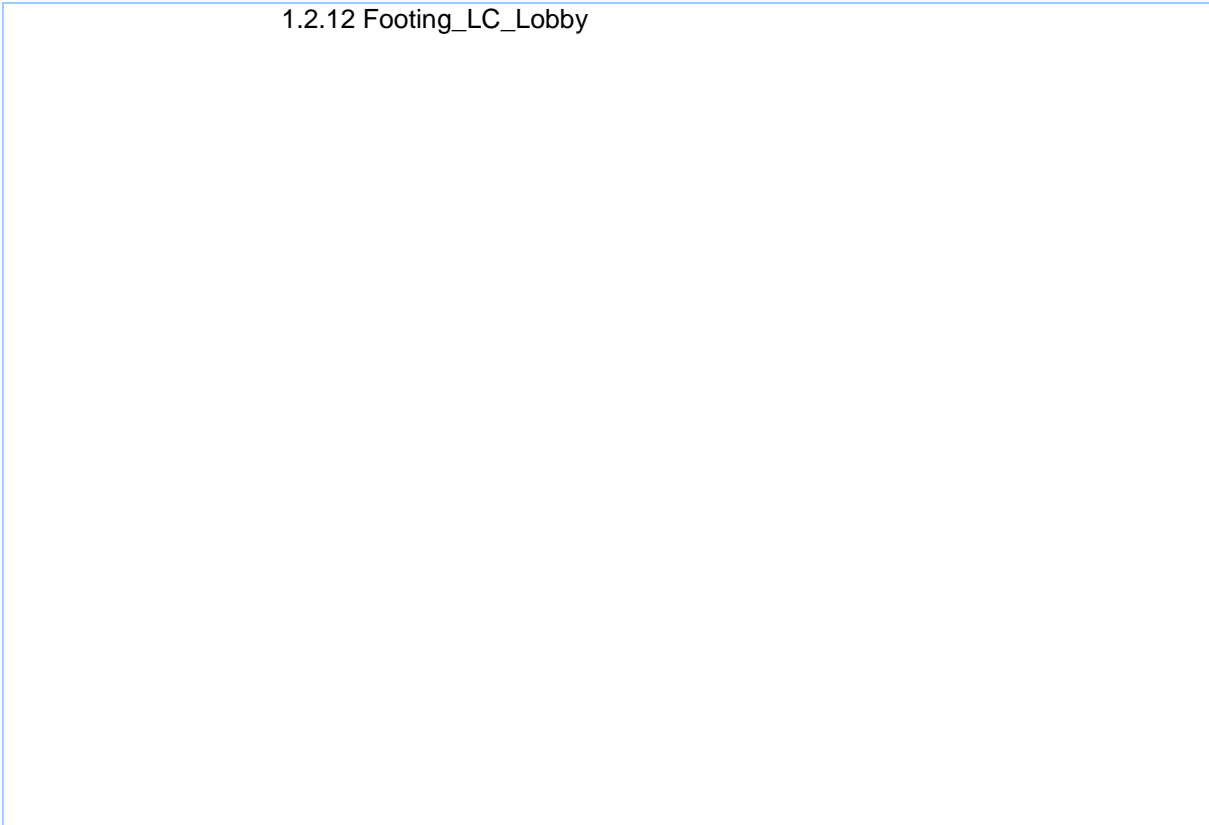
$$= [(7.83') \times (6"/12)] / (7.5"/12)$$

$$= 6.26 \text{ feet}$$

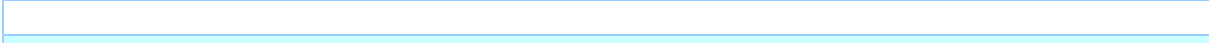
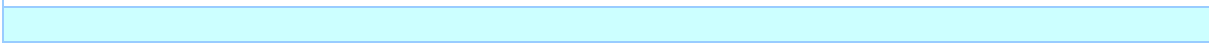
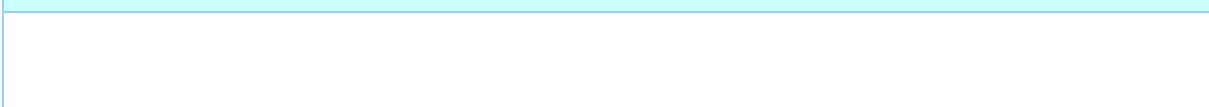
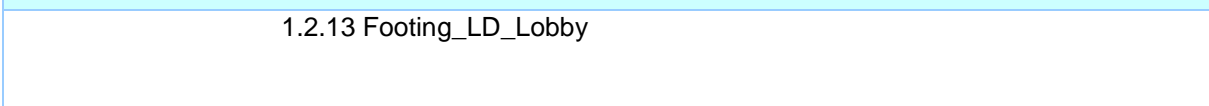
1.2.10 Footing_LA_Lobby

1.2.11 Footing_LB_Lobby

1.2.12 Footing_LC_Lobby



1.2.13 Footing_LD_Lobby



A21 Lowest Floor Construction

The Impact Estimator, SOG inputs are limited to being either a 4" or 8" thickness. Since the actual SOG thicknesses for the HEBB theatre were not exactly 4" or 8" thick, the areas measured in OnScreen required calculations to adjust the areas to accommodate this limitation.

The Impact Estimator limits the thickness of footings to be between 7.5" and 19.7" thick. As there are a number of cases where footing thicknesses are not within these limitations, their widths were adjusted accordingly to maintain the same volume of footing.

Concrete strength was set to 4000psi and an average % of concrete flyash was assumed.

Lastly, the concrete stairs were modelled as footings.

SOG

1.1.1 SOG_5" _Lobby

The area of this slab had to be adjusted so that the thickness fit into the 8" thickness specified in the Impact Estimator. The following calculation was done in order to determine appropriate Length and Width (in feet) inputs for this slab;

$$= \text{sqrt}[\frac{(\text{Measured Slab Area}) \times (\text{Actual Slab Thickness})}{(4"/12)}]$$

$$= \text{sqrt}[\frac{5,653.31 \times (5"/12)}{(4"/12)}]$$

$$= 84.06 \text{ feet}$$

A22 Upper Floor Construction

Stairs

1.2.14 Stairs_Theatre

The thickness of the stairs was estimated to be 24 inches based on the cross-section architectural drawings.

The width of this slab was adjusted to accommodate the Impact Estimator limitation of footing thicknesses to be under 19.7". The measured length was maintain, thicknesses were set at 19" and the widths were increased using the following calculations;

$$= [(Cited Width) \times (Cited Thickness)] / (19"/12)$$

$$= [(65.5') \times (24"/12)] / (19"/12)$$

$$= 82.74 \text{ feet}$$

Column 3.1.1
Beam Column_Beam_Concrete_Lobby

An average floor to floor height of 10.5' was used throughout lobby, as determined from architectural drawings;

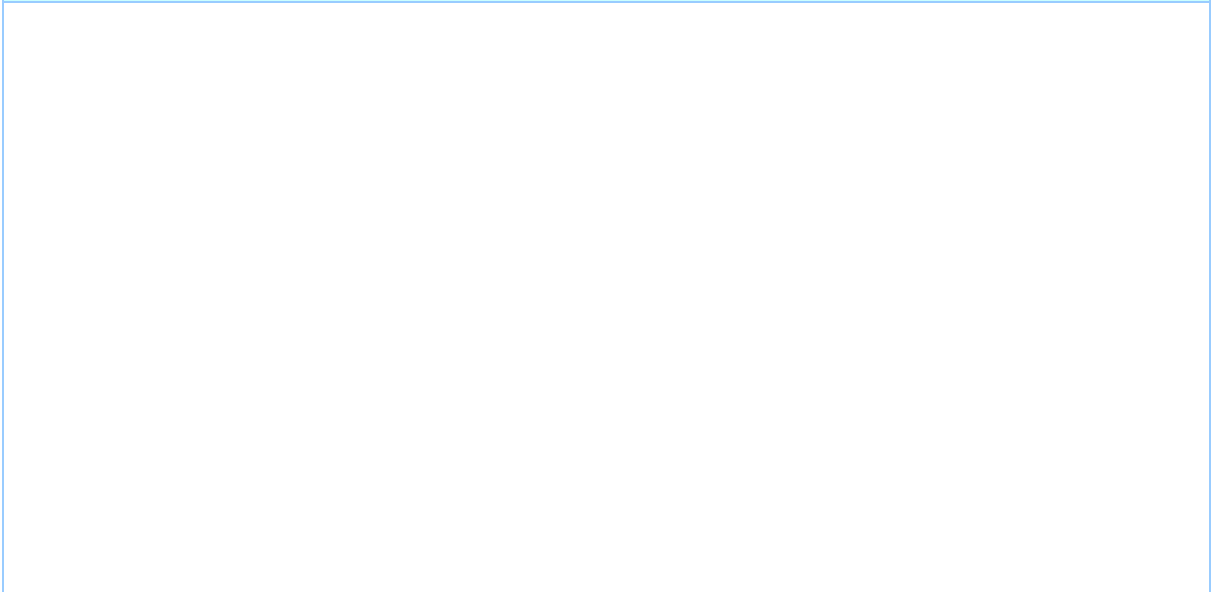
$$= (8.5+9.5+7+9+12+17)/6 = 10.5'$$



3.1.2
Column_Beam_Concrete_Theatre

An average floor to floor height of 26' was used throughout theatre, as determined from architectural drawings;

$$= (19'+32.5'+36'+33'+30'+26'+21'+15'+19.5')/9 = 26'$$



Suspended Floor 4.1.1
Floor_ConcreteSuspendedSlab_Theatre

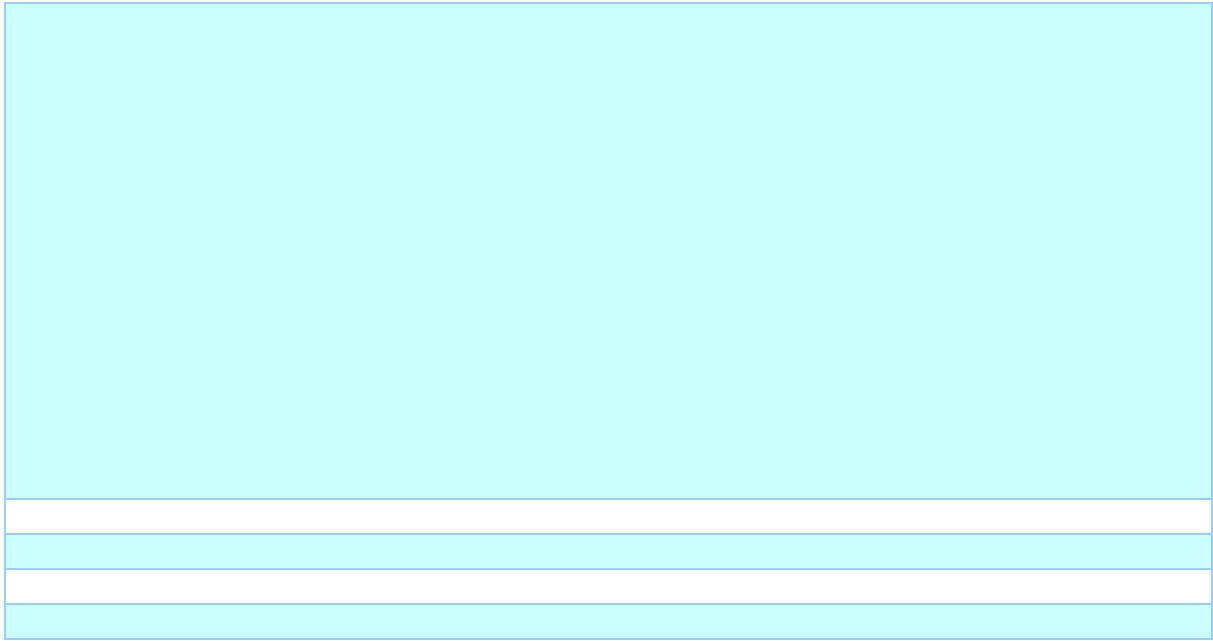
The Impact Estimator calculated the thickness of the material based on floor width, span, concrete strength, concrete flyash content and live load. Concrete strength was set to 4000psi and an average % of concrete flyash was assumed.

As stated on the structural drawings, the live loads for floors are as follows: labs, classrooms, and theatre have specified live loads of 60psf; corridors, entrances, and stairs have specified live loads of 100psf. An average of these values of 75psf is used for EIE Inputs.

A23 Roof
Construction

The live load was assumed to be 45 psf instead of the specified 27 psf and the concrete strength was set to 4,000psi with average flyash content. All stated about roof envelope from architectural drawings is that it is comprised of 1" rigid insulation. For EIE Model, it is assumed to have a 4-Ply Built-up Asphalt Roof System - Inverted with Extruded Polystyrene, Glass Felt envelope material. Vapour barrier assumed to be polyethylene 6mil.

Suspend
ed Slab 5.1.1 Roof_ConcreteSuspendedSlab_Theatre



A31 Walls Below
Grade

The length of the concrete cast-in-place walls needed adjusting to accommodate the wall thickness limitation in the Impact Estimator (8" or 12").

Concrete strength was set to 4000psi and an average % of concrete flyash was assumed.

The wall envelopes consisting of plaster are modelled as consisting of Regular Gypsum 1/2" due to the unavailability of plaster as a material in Athena EIE.

The vapour barrier is assumed to be Polyethylene 6 mil.

For the external wall of the theatre, the exterior envelope consists of 4.75" Norman Glazed Brick on 90% of the height of the wall, and 3.75" concrete cladding on 10% of the height of the wall. For the model to be inputted into Athena EIE, it is assumed that the exterior envelope consists of Standard Ontario Brick on 100% of the height of the wall. The glazing on the Norman Brick is modeled as Alkyd Solvent Based Paint in Athena EIE.

Doors are modeled as steel exterior doors, which is the closest estimation to the observed doors. The number and location of doors are as determined from site exploration.

Wall heights for the lobby determined from dimensioning of structural drawings and given elevations.

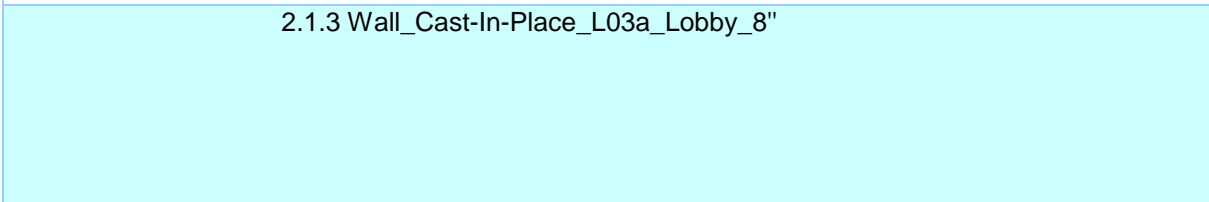
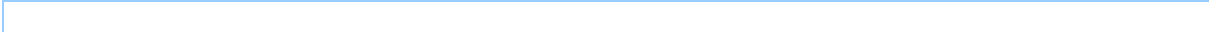
A32 Walls Above
Grade

Walls 2.1.1 Wall_Cast-In-Place_L01_Lobby_8"

2.1.2 Wall_Cast-In-Place_L02_Lobby_8"



2.1.3 Wall_Cast-In-Place_L03a_Lobby_8"



2.1.4 Wall_Cast-In-Place_L03b_Lobby_8"

2.1.5 Wall_Cast-In-Place_L04_Lobby_8"

2.1.6 Wall_Cast-In-Place_L05_Lobby_1'8"

This wall was increased by a factor in order to fit the 12" thickness limitation of the Impact Estimator. This was done by increasing the length of the wall using the following equation;

$$= (\text{Measured Length}) * [(\text{Cited Thickness})/12"]$$

$$= (4.75') * [(20")/12"]$$

$$= 7.92 \text{ feet}$$

2.1.7 Wall_Cast-In-Place_L06_Lobby_1'8"

This wall was increased by a factor in order to fit the 12" thickness limitation of the Impact Estimator. This was done by increasing the length of the wall using the following equation;

$$= (\text{Measured Length}) * [(\text{Cited Thickness})/12"]$$

$$= (6.58') * [(20")/12"]$$

$$= 11.00 \text{ feet}$$

2.1.8 Wall_Cast-In-Place_L07_Lobby_8"

2.1.9 Wall_Cast-In-Place_L08_Lobby_6"

The height of this wall varies along its length; therefore, the average height of 12' is used.

This wall was reduced by a factor in order to fit the 8" thickness limitation of the Impact Estimator. This was done by reducing the length of the wall using the following equation;

$$= (\text{Measured Length}) * [(\text{Cited Thickness})/8"]$$

$$= (24.81') * [(6")/8"]$$

$$= 18.61 \text{ feet}$$



2.1.10 Wall_Cast-In-Place_L09-10_Lobby_8"

The height of this wall varies along its length; therefore, the average height of 12' is used.

2.1.11 Wall_Cast-In-Place_L11_Lobby_10"

The height of this wall varies along its length; therefore, the average height of 12' is used.

This wall was increased by a factor in order to fit the 8" thickness limitation of the Impact Estimator. This was done by increasing the length of the wall using the following equation;

$$= (\text{Measured Length}) * [(\text{Cited Thickness})/8"]$$

$$= (42.32') * [(10")/8"]$$

$$= 52.90 \text{ feet}$$

2.1.12 Wall_Cast-In-Place_L12a_Lobby_8"

2.1.13 Wall_Cast-In-Place_L12b_Lobby_8"

2.1.14 Wall_Cast-In-Place_L13_Lobby_10"

This wall was increased by a factor in order to fit the 8" thickness limitation of the Impact Estimator. This was done by increasing the length of the wall using the following equation;

$$= (\text{Measured Length}) * [(\text{Cited Thickness})/8"]$$

$$= (27.50') * [(10")/8"]$$

$$= 34.38 \text{ feet}$$

2.1.15 Wall_Cast-In-Place_L14_Lobby_11.75"

This wall was reduced by a factor in order to fit the 12" thickness limitation of the Impact Estimator. This was done by reducing the length of the wall using the following equation;

$$= (\text{Measured Length}) * [(\text{Cited Thickness})/12"]$$

$$= (89.57) * [(11.75")/12"]$$

$$= 87.70 \text{ feet}$$

2.1.16 Wall_Cast-In-Place_W6_Ext_BrickClad_Theatre_8"

An average floor to floor height of 26' was used throughout theatre, as determined from architectural drawings;

$$= (19'+32.5'+36'+33'+30'+26'+21'+15'+19.5')/9 = 26'$$

B11 Partitions

Walls

2.1.17 Wall_Cast-In-Place_W6_Int_Theatre_6"

An average floor to floor height of 26' was used throughout theatre, as determined from architectural drawings;

$$= (19'+32.5'+36'+33'+30'+26'+21'+15'+19.5')/9 = 26'$$

This wall was increased by a factor in order to fit the 8" thickness limitation of the Impact Estimator. This was done by increasing the length of the wall using the following equation;

$$= (\text{Measured Length}) * [(\text{Cited Thickness})/8"]$$

$$= (51.75') * [(6")/8"]$$

$$= 38.81 \text{ feet}$$

2.1.18
Wall_Cast_In_Place_W6_Int_Theat
re_8"

An average floor to floor height of 26'
was used throughout theatre, as
determined from architectural
drawings;

$$= \\ (19'+32.5'+36'+33'+30'+26'+21'+15'+19.5')/9 = 26'$$