

University of British Columbia

Social Ecological Economic Development Studies (SEEDS) Sustainability Program

Student Research Report

# East Mall Redesign between Agronomy Road and W16th Avenue

Prepared by: Deepinder Bajwa, Ray Han, Johnson Hu, Thomson Mai, Bastien Moy, Kyle Tam

Prepared for:

Course Code: CIVL 446

University of British Columbia

Date: 16 April 2021

*Disclaimer: "UBC SEEDS Sustainability Program provides students with the opportunity to share the findings of their studies, as well as their opinions, conclusions and recommendations with the UBC community. The reader should bear in mind that this is a student research project and is not an official document of UBC. Furthermore, readers should bear in mind that these reports may not reflect the current status of activities at UBC. We urge you to contact the research persons mentioned in a report or the SEEDS Sustainability Program representative about the current status of the subject matter of a report".*



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# EXECUTIVE SUMMARY

Our team has been retained by UBC Social Economic Development Studies (UBC SEEDS) to redesign East Mall between Stadium Road and Agronomy Road in attempt to better accommodate sustainable transportation modes. The corridor's current conditions do not accommodate the high amount of pick-up/drop-off traffic during the evenings, and do not promote sustainable modes of transportation.

This report will provide an in-depth review for the detailed design of the transportation, structural, municipal, and environmental disciplines. Our recommended concept involves shifting the existing median East to separate vehicle travel lanes and bike lanes, reconfiguring the intersection of Thunderbird Boulevard and East Mall and upgrading the existing signal, and widening the segment from Thunderbird Boulevard to Agronomy Road to accommodate a new bi-directional bike lane. This design will improve the safety of cyclists, provide an abundance of green space for pedestrians, and reduce conflicts between vehicles and cyclists at drop-off pick-up zones while retaining parking for residents and users of the nearby facilities.

An assessment of the existing utilities was conducted to identify impacts on the existing utility networks. The proposed reconfiguration is not expected to affect the system demands the water distribution and sanitary sewer systems. A stormwater management strategy has been developed on site, and the final corridor reduces the captured stormwater volumes within the project area. Specifications for the new permeable concrete cycling lanes and sidewalks have been developed, including an aggregate reservoir base to detain major storm flows for natural infiltration into the subgrade.

The new pedestrian canopy consists of W200x31 section profiles for the columns and cantilevers with tempered glass panels mounted as the decking. The structure is 66.86-metres in length and will be constructed along the South side of Agronomy Road.

The greenspace consists of the plantation of several new tree species to further improve the aesthetic of the corridor. Additionally, the greenspace has a community garden composed of various flowers to encourage people to gather and enjoy the surrounding landscape hence building the community.

Estimated budget for the proposed solution will be \$5,163,449 which includes labour, materials, operation & maintenance and a 15% contingency. Construction work will begin on May 2021 with a completion date of December 2021 with a duration of around 9 months.

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# 1. INTRODUCTION

Our team has been retained by UBC Social Ecological Economic Development Studies (SEEDS) to redesign East Mall between Stadium Road and Agronomy Road. This section will introduce the project site and the project scope. Our team member contributions are provided below.

Table 1: Team member contributions to the Design Report

Team Member	Contributions To	Review and Edited By
Johnson Hu	<ul style="list-style-type: none"> <li>Report formatter and editor</li> <li>Detailed design and analysis of pedestrian canopy</li> <li>Canopy drawings</li> <li>Canopy construction specifications</li> </ul>	<ul style="list-style-type: none"> <li>Final Design Report</li> <li>Municipal design and calculations</li> <li>Cost estimate and schedule</li> <li>Greenspace design</li> </ul>
Bastien Moy	<ul style="list-style-type: none"> <li>Design Objectives and Key Issues</li> <li>Road Configuration</li> <li>Roadway design</li> <li>Signage plan</li> </ul>	<ul style="list-style-type: none"> <li>Final Design Report</li> <li>Risk analysis</li> <li>Existing and future traffic condition analysis</li> <li>Greenway design</li> </ul>
Ray Han	<ul style="list-style-type: none"> <li>Utilities review</li> <li>Utilities design and calculations</li> <li>Drawing formatting</li> <li>Utilities drawings</li> <li>Service life maintenance plan</li> <li>Cross-section drawings</li> </ul>	<ul style="list-style-type: none"> <li>Final Design Report</li> <li>Detailed design and analysis of pedestrian canopy</li> <li>Cost estimate and schedule</li> <li>Road configuration</li> </ul>
Kyle Tam	<ul style="list-style-type: none"> <li>Cost estimate &amp; schedule</li> <li>Risk Analysis</li> <li>Revised plan view drawings</li> <li>Traffic Management Plan Drawings</li> <li>Plan view details</li> </ul>	<ul style="list-style-type: none"> <li>Final Design Report</li> <li>Utilities design</li> <li>Synchro modelling</li> <li>Stakeholder engagement</li> </ul>
Deepinder Bajwa	<ul style="list-style-type: none"> <li>Stakeholder engagement</li> <li>Service life maintenance plan</li> <li>Greenway design</li> </ul>	<ul style="list-style-type: none"> <li>Final Design Report</li> <li>Canopy site preparation requirements</li> <li>Construction sequencing</li> <li>Traffic management plan</li> </ul>
Thomson Mai	<ul style="list-style-type: none"> <li>Existing traffic condition analysis</li> <li>Future traffic volume growths</li> <li>Synchro modelling</li> <li>Greenway design</li> </ul>	<ul style="list-style-type: none"> <li>Final Design Report</li> <li>Final drawing package</li> <li>Signage plan</li> <li>Service life maintenance plan</li> </ul>

## 1.1. SITE OVERVIEW

Located on the University Endowment Lands, East Mall runs parallel to Westbrook Mall and is an important point of access for the UBC campus and bears a high volume of traffic on a day-to-day basis. It is a wide road with a large median strip separating single travel lanes. From 16th Avenue to Agronomy Road, East Mall contains two shuttle bus stops, a street bike lane, and a generous amount of curb side parking that also serves as a pick-up/drop-off zone to numerous sports fields and recreation centres. The current design poses several issues including speeding, cyclist safety, overdemand for curb side parking, pedestrian crossing safety, and lack of usable green space. Figure 1 and Figure 2 below show the current conditions and project site location.



Figure 1: East Mall

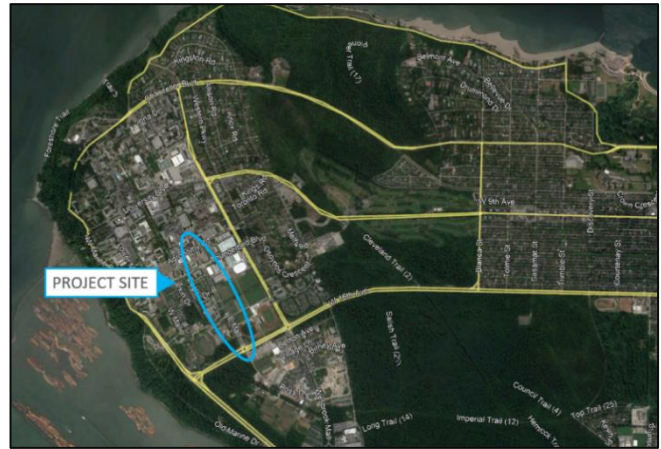


Figure 2: Project Location

## 1.2. PROJECT SCOPE

The scope of work for this project consists of client required objectives as identified below. This report will address each objective and provide some insight on the design process, including calculations, technical drawings, and construction specifications. A summary of the major components of this project are:

1. Upgrade the existing East Mall corridor to promote sustainable modes of transportation and incorporate traffic calming measures to reduce travel speeds
2. Improve liveability along the corridor by reducing the possibility of vehicle conflicts with pick-up/drop-offs, pedestrians, and cyclists
3. Minimize impacts to the existing utility networks and prepare a stormwater management strategy aligned with UBC's sustainability initiatives



4. Incorporate a pedestrian canopy along Agronomy Road that prioritizes comfort, safety, campus aesthetics, and cost
5. Prepare a Class A cost estimate and detailed construction schedule

### 1.3. STAKEHOLDER MANAGEMENT

A stakeholder study has been completed to ensure the project accounts for all requirements. Our team identified the relevant stakeholders, developing a consulting plan, and reviewing feedback. Table 2 outlines the relevant stakeholders and their importance to the project.

*Table 2: Stakeholder Identification*

<b>Stakeholder</b>	<b>Association to the project</b>
UBC Social, Ecological, Economic Development Studies (SEEDS)	The client
UBC Students, Faculty, and Staff	Primary users of the corridor and pedestrian canopy
Ministry of Transportation and Infrastructure	Governs transportation policies within BC
TransLink	Provides transit services along and nearby the corridor
UBC Water & Energy Services	Major utility owners within the corridor
Musqueam First Nations	Are the traditional, ancestral habitants of the territory
UBC Neighbourhood Association	Residents that live near the construction project
UBC Properties Trust	Manage the lands adjacent to the corridor

The feedback provided by the stakeholders was critical to establishing an effective final design. Contact has been established with each of the stakeholder to gather information regarding their issues and concerns. Based on the feedback our team received from stakeholders, our team is confident that the project will receive full support during construction. We will continue to reach out to our identified stakeholders before, during and after construction and address any issues that arise.

## 2. KEY DESIGN COMPONENTS

During the design phase of this project, our team utilized a number of engineering standards, specifications, and software. The table below outlines them organized by project discipline.

Table 3: Standards, Specifications, and Software used during design

Discipline	Standard / Code Used	Software Packages Used
<b>Transportation</b>	<ul style="list-style-type: none"> <li>• BC Active Transportation Design Guide</li> <li>• TAC Geometric Design Guide for Canadian Roads</li> <li>• City of Vancouver Engineering Design Manual</li> </ul>	<ul style="list-style-type: none"> <li>• Synchro 10</li> <li>• AutoCAD</li> <li>• Civil 3D</li> </ul>
<b>Structural</b>	<ul style="list-style-type: none"> <li>• CSA A23.3-14</li> <li>• CSA S16-19</li> <li>• NBC 2015</li> </ul>	<ul style="list-style-type: none"> <li>• S-Frame</li> <li>• S-Steel</li> <li>• AutoCAD</li> </ul>
<b>Utilities</b>	<ul style="list-style-type: none"> <li>• City of Vancouver Engineering Design Manual</li> <li>• City of Surrey Design</li> <li>• UBC Integrated Stormwater Management Plan</li> <li>• UBC Utilities Technical Guidelines</li> <li>• UNHSC Design Specifications for Porous Asphalt Pavement and Infiltration Beds</li> </ul>	<ul style="list-style-type: none"> <li>• Civil 3D</li> </ul>
<b>Greenspace</b>	<ul style="list-style-type: none"> <li>• UBC Exterior Improvements Technical Guidelines</li> </ul>	<ul style="list-style-type: none"> <li>• Bluebeam Revu</li> </ul>
<b>Construction</b>	<ul style="list-style-type: none"> <li>• BC Traffic Management Manual for Work on Roadways 2015</li> </ul>	<ul style="list-style-type: none"> <li>• AutoCAD</li> <li>• Bluebeam Revu</li> </ul>

### 2.1. DESIGN CONCEPT



Figure 3: Streetmix cross section of our East Mall Design

Our redesign of East Mall features a full reconstruction of the boulevard. The main feature of this configuration is the shifting of the existing median to the east side of East Mall and moving all the vehicle travel lanes to the west side. Additionally, new traffic calming measures will also be implemented along East Mall to reduce the speed of traffic. This new location of the median will improve the safety of pedestrians and cyclists as it creates a natural separation from the vehicular traffic. Improved access to this area also adds a variety of land use options, and will function as a greenspace featuring new landscaping and space for community garden boxes or public art. A new pedestrian canopy will also be constructed along Agronomy Road and provide shelter for bystanders. A stormwater management strategy has also been prepared centred around the use of permeable pavement for new cycling paths and sidewalks.

Table 4: Summary of design objectives and features

<b>Discipline</b>	<b>Design Objective</b>	<b>Design Feature</b>
<b>Transportation</b>	<ul style="list-style-type: none"> <li>• Encourage use of active transportation modes</li> <li>• Reduce speeding along East Mall</li> <li>• Reduce vehicle – cyclist conflicts at pick - up drop – off zones</li> <li>• Retain ease of access for current residents</li> </ul>	<ul style="list-style-type: none"> <li>• New 4.0m bi-directional greenway</li> <li>• Reduced travel lane widths</li> <li>• Dedicated drop off pick zones with no parking at any time</li> <li>• Retains parking on both sides of the road</li> </ul>
<b>Structural</b>	<ul style="list-style-type: none"> <li>• Encourage walking along Agronomy Rd. by implementing a pedestrian canopy</li> <li>• Comfortable and safe to use</li> <li>• Cost considerations</li> <li>• Fit with campus architecture</li> </ul>	<ul style="list-style-type: none"> <li>• Spans the full width of sidewalk</li> <li>• Design was inspired from existing UBC bus loop to fit campus architecture</li> <li>• All structural components are the same size and thickness in order to save cost</li> </ul>
<b>Utilities</b>	<ul style="list-style-type: none"> <li>• Ensure post-development demands on UBC utility networks are within pre-development levels</li> <li>• Capture and keep stormwater on-site wherever possible</li> </ul>	<ul style="list-style-type: none"> <li>• Reduce travel lane widths and introduce permeable concrete sidewalks and cycling lanes</li> <li>• Provide stormwater detention reservoir in aggregate base of permeable concrete</li> </ul>
<b>Greenspace</b>	<ul style="list-style-type: none"> <li>• Encourages active modes of transportation</li> <li>• Creates a barrier from vehicle traffic increasing safety of users</li> <li>• Minimize demand on UBC distribution networks and capture stormwater on-site</li> </ul>	<ul style="list-style-type: none"> <li>• Plantation of new tree species long median</li> <li>• Community gardens at various points throughout median</li> <li>• Use absorbent topsoil in landscaped areas to promote infiltration</li> </ul>
<b>Construction</b>	<ul style="list-style-type: none"> <li>• Minimize disturbances to surrounding residents</li> </ul>	<ul style="list-style-type: none"> <li>• Existing utilities will remain in place and in-service during construction</li> </ul>

## 3. TRANSPORTATION DESIGN

This section will describe the design considerations relating to the roadway including roadway dimensions, intersections upgrades, and signage plans.

### 3.1. ROADWAY DESIGN

Roadway design was done in accordance with the Geometric Design Guide for Canadian Roads, written by the Transportation Association of Canada (TAC), Engineering Design Manual from the City of Vancouver, as well as the British Columbia Active Transportation Design Guide. Key requirements include: all roadways to have a minimum crossfall of 2.0%, minimum vehicle travel lane width must be 3.25m or greater, grade of proposed alignment must not exceed 10%, and minimum sidewalk widths of 1.8m. Other factors considered in the detailed design include sightline requirements, driver comfort for sag and crest curves, as well as signal timing plans for the proposed signal upgrades at the intersection of East Mall and Thunderbird Boulevard. Software packages utilized in roadway design include AutoCAD and Civil 3D, and intersection analysis and timing plans were done with the aid of Synchro 6. Traffic signs were designed in accordance to the Manual of Traffic Signs and Pavement Markings from the British Columbia Ministry of Transportation and Highways.

#### 3.1.1. ROADWAY CROSS SECTIONS

Roadway cross sections for the newly designed East Mall segment must meet the requirements set out in section 410 in the TAC Geometric Design Guide for Canadian roads. In the proposed design, travel lane widths are set to be 3.30m wide, which satisfies the 3.25m minimum lane width for road segments with a design speed between 50km/h to 70km/h. Roadway crossfall in the design is 2.5%, which satisfies the TAC requirement of having a crossfall of 2% or greater, which is needed in order to provide adequate drainage for the road surface. 2.5% crossfall was chosen in consideration with the climate of the area which experiences high amounts of annual precipitation, and the higher crossfall will assist in facilitating drainage. Existing parking is retained in the new design with 2.4m parking lanes on both sides of the road. 2.4m was chosen to balance the goal of keeping vehicle speeds down on the segment by reducing the amount of space available to drivers, while providing enough room for parked vehicles. Sidewalk widths for the new segment are designed to be a minimum of 1.8m throughout the segment. 1.8m provides enough space for pedestrians to feel comfortable, safe, and allows for movement in both directions. A good sidewalk network is vital in encouraging more users to choose active transportation modes such as walking or cycling. Lastly, the multi-

use pathway in the design is 4.0m, surpassing the required 2.7m as required by the British Columbia Active Transportation Guide (BCATG). A wide facility provides users more space to travel on the corridor and encourages more users to make trips with modes like cycling, walking, skateboarding, and rollerblading safely and comfortably. Having good a greenway network is also beneficial for the UBC campus as it allows for better accessibility for the future Stadium development, which is projected to add thousands of units of occupancy.

Table 5: TAC Geometric Design Guide – Roadway Width Requirements

Design Speed (km/h)	Lane Width <sup>(1)</sup> (m)		Unpaved <sup>(1)</sup> Shoulder (m)	Normal X-Fall (m/m)	Fill Slope <sup>(2)</sup>
	ADTT>15 <sup>(3)</sup>	ADTT<15 <sup>(3)</sup>			
80 - 90	3.6	3.5	0.5	0.02	2:1
50 - 60 - 70 <sup>(5)</sup>	3.5	3.25 <sup>(4)</sup>	0.5	0.02	2:1
30 -40 <sup>(5)</sup>	3.25 <sup>(4)</sup>	3.25 <sup>(4)</sup>	0.5	0.02	2:1

### 3.1.2. ROADWAY PROFILE

The roadway profile was also designed to meet the requirements set out in the TAC Geometric Design Guide. Key requirements for the profile of the roadway include grade requirements and sightline requirements. The roadway profile primarily depends on the existing natural topography of the area, which is mostly flat. Hence the proposed roadway will largely overlap with the existing roadway profile and does not contain large elevation changes, with the biggest grade change at 4%, which is below the 10% maximum grade requirement outlined in the TAC Geometric Design Guide. When designing the roadway profile, sightline distances were also taken into consideration in order to satisfy the 65m sight distance for a roadway with a design speed of 50km/h. The length of the crests and sags were also calculated in accordance with best practices currently used in North America. Crest and sag lengths are important to rider comfort as well as stopping distances. Sample calculations can be found in the attached Appendix C. The figure below showcases the roadway profile of the proposed design.

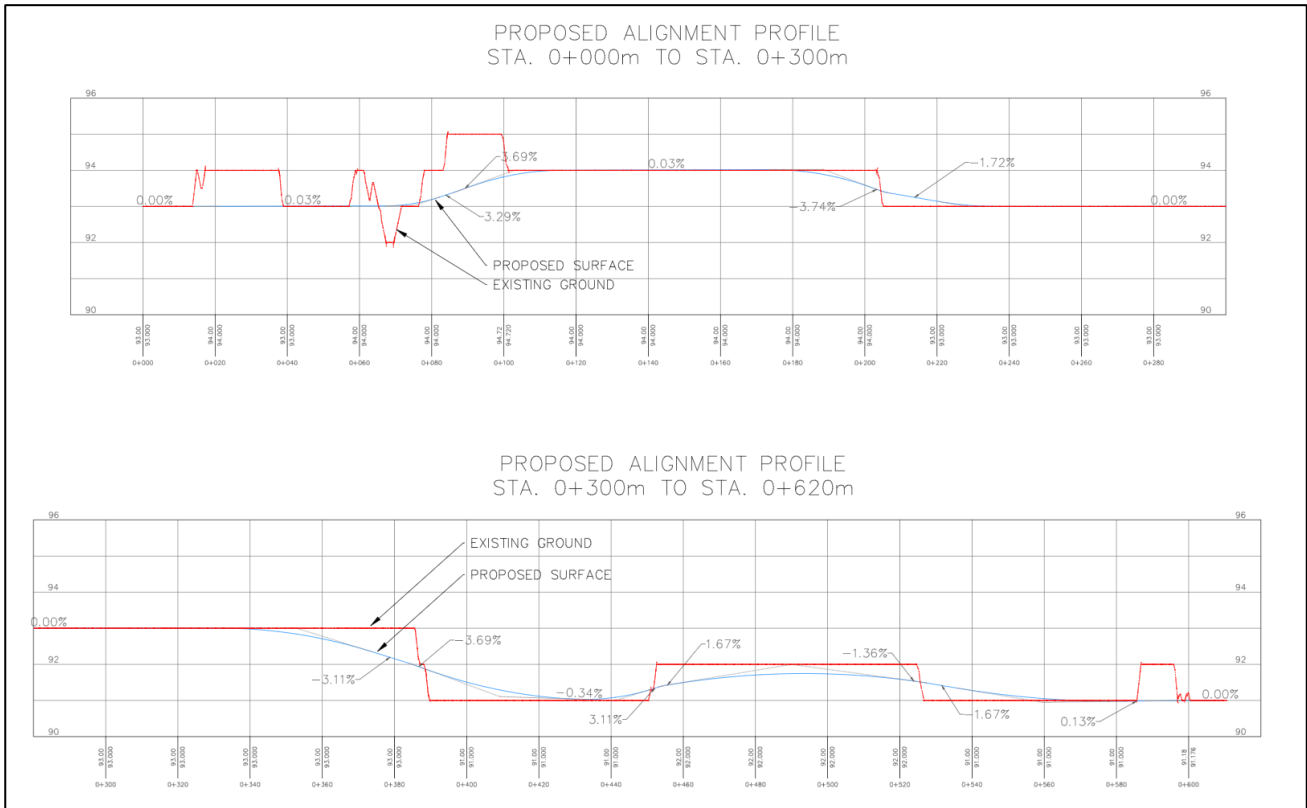


Figure 4: Roadway Profile of Proposed Design

## 3.2. THUNDERBIRD BOULEVARD AND EAST MALL

East Mall runs parallel to Westbrook Mall and Marine Drive and is one of the few roads that run North-South on the UBC Campus, providing key connections to locations such as the Health Sciences Parkade and Thunderbird Stadium. A traffic analysis on the intersection of Thunderbird Boulevard and East Mall will be provided in detail throughout this section.

### 3.2.1. EXISTING CONDITIONS AND ISSUES

Currently, the intersection of Thunderbird Boulevard and East Mall is controlled by an existing pre-timed signal. The intersection services around 800 vehicles in the AM peak period and around 1150 vehicles in the PM peak. A majority of the vehicle traffic in the AM period are vehicles heading northbound into the campus, while in the PM period most vehicles are heading south and leaving the campus. The existing configuration is as follows: The South, West, and North approaches all have one receiving and departing lane, while the East approach has one receiving lane and two departing lanes, one dedicated to a left turn movement and the other for through and right movements. The intersection also sees high pedestrian volumes, with around 300 crossings in both the AM peak and PM peak periods. Cyclist volumes should also be accounted, as there are

around 130 cyclists in both the AM and PM peak periods. The following figure shows the vehicle volumes serviced by the intersection:



Figure 5: Existing Vehicle Volumes at intersection of Thunderbird Boulevard and East Mall

As shown in Figure 5, there are many vehicles making the westbound-left movement in the PM peak period, and the current traffic signal is not capable of providing a protected left turn movement for those motorists and is a bottleneck in the system.

### 3.2.2. PROPOSED DESIGN CHANGES AT THUNDERBIRD BLVD AND EAST MALL

To better facilitate pedestrian and cyclist movements, it is proposed that vehicle travel lanes on the North approach to be moved to the west side of East Mall, allowing the existing northbound lane to be converted into a dedicated bi-direction bicycle lane with bollards acting as a barrier to vehicle traffic. The goal behind this design is to prioritize active transportation modes and provide additional capacity for cyclists and pedestrians. Having dedicated conflict paint will provide users of the greenway a safer experience crossing the intersection by making drivers more aware. A bi-directional bicycle lane makes full use of the existing road space and encourages drivers to slow down due to having less buffer space. The proposed design also includes a full

signal upgrade on the intersection to allow for protected westbound left turn movements in the PM peak period to alleviate total intersection delays. To accommodate this, induction loops are to be installed on the westbound left turning bay on the East approach. Section 3.2.3 will discuss the rationale behind this upgrade and provide additional analysis and justification. The figure below highlights the proposed changes to the intersection.

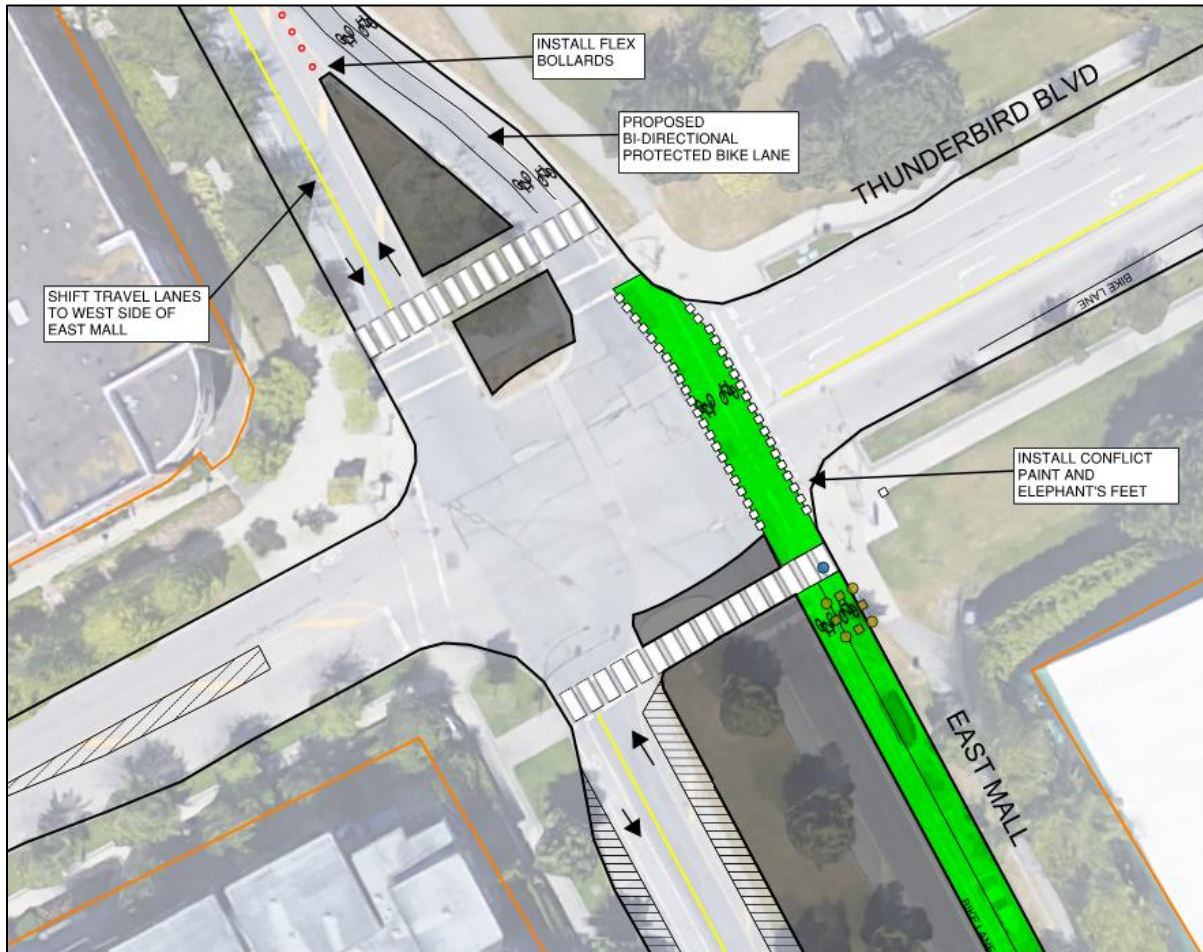


Figure 6: Proposed Design at Thunderbird Boulevard and East Mall

### 3.2.3. SYNCHRO ANALYSIS

Intersection performance analysis at Thunderbird Boulevard and East Mall was performed using Synchro. The performance of the intersection with the addition of a protected westbound left movement was compared to the existing conditions. The results from the Synchro model showed that in the AM peak period, having a protected westbound left phase decreased the performance of the intersection due to the low volumes. Therefore, it is recommended that the AM peak period retain its current timing configuration. However, in the PM peak period, having a dedicated phase for vehicles making the westbound left movement decreases the delay from an estimated 43 seconds to 22 seconds while maintaining the same overall intersection delay. The



results from the Synchro analysis are shown in the table below. A sample Synchro report can be found in Appendix I.

Table 6: Intersection LOS and delays with Existing and Upgraded Signal

Movement	Intersection LOS			Intersection Delays				
	Existing Signal	Upgraded Signal		Existing Signal		Upgraded Signal		
		AM	PM	AM	PM	AM	PM	AM
EBL	B	B	B	B	18.5	11.3	16.4	18.1
EBT	B	B	B	B	18.5	11.3	16.4	18.1
EBR	B	B	B	B	18.5	11.3	16.4	18.1
WBL	B	D	A	C	19.2	43.2	9.7	22.3
WBT	B	B	B	A	19.1	11.8	10.0	8.9
WBR	B	B	C	A	19.1	11.8	10.0	8.9
NBL	B	B	C	B	16.3	11.6	27.1	14.6
NBT	B	B	C	B	16.3	11.6	27.1	14.6
NBR	B	B	C	B	16.3	11.6	27.1	14.6
SBL	A	C	B	C	7.5	21.1	12.8	30.1
SBT	A	C	B	C	7.5	21.1	12.8	30.1
SBR	A	C	B	C	7.5	21.1	12.8	30.1
Overall	B	C	B	C	16.3	21.6	19.9	21.6

### 3.3. AGRONOMY ROAD AND EAST MALL

The intersection of Agronomy Road and East Mall is north of Thunderbird Boulevard and is the next intersection for users heading north on East Mall after passing Thunderbird Boulevard. This section will highlight the challenges currently posed on the intersection and the proposed changes to tackle these challenges.

#### 3.3.1. EXISTING CONDITIONS

Unlike the intersection at Thunderbird Boulevard, the intersection of Agronomy Road is much narrower and supports larger volumes of pedestrian activity due to its proximity to the UBC Centre for Advance Wood Processing and nearby businesses such as the Starbucks at the southeast corner of the intersection. For this report, vehicle volumes on the intersection are assumed to be lower than the intersection of Thunderbird Boulevard due to pedestrian activity as count data was not available at the time of the study.

#### 3.3.2. PROPOSED CHANGES

Sticking with the goal of improving active transportation along the corridor, improvements at the intersection of Agronomy Road and East Mall include installing conflict paint and elephant’s feet to help facilitate crossing of cyclists and continuing the bi-directional protected bicycle lane originating from Thunderbird Boulevard. The bi-directional bicycle lane is set to terminate at the Agronomy, but the conflict paint markings will allow cyclists

to continue northbound on East Mall and provide southbound cyclists a safe connection onto the greenway. The figure below shows the proposed changes at the intersection.

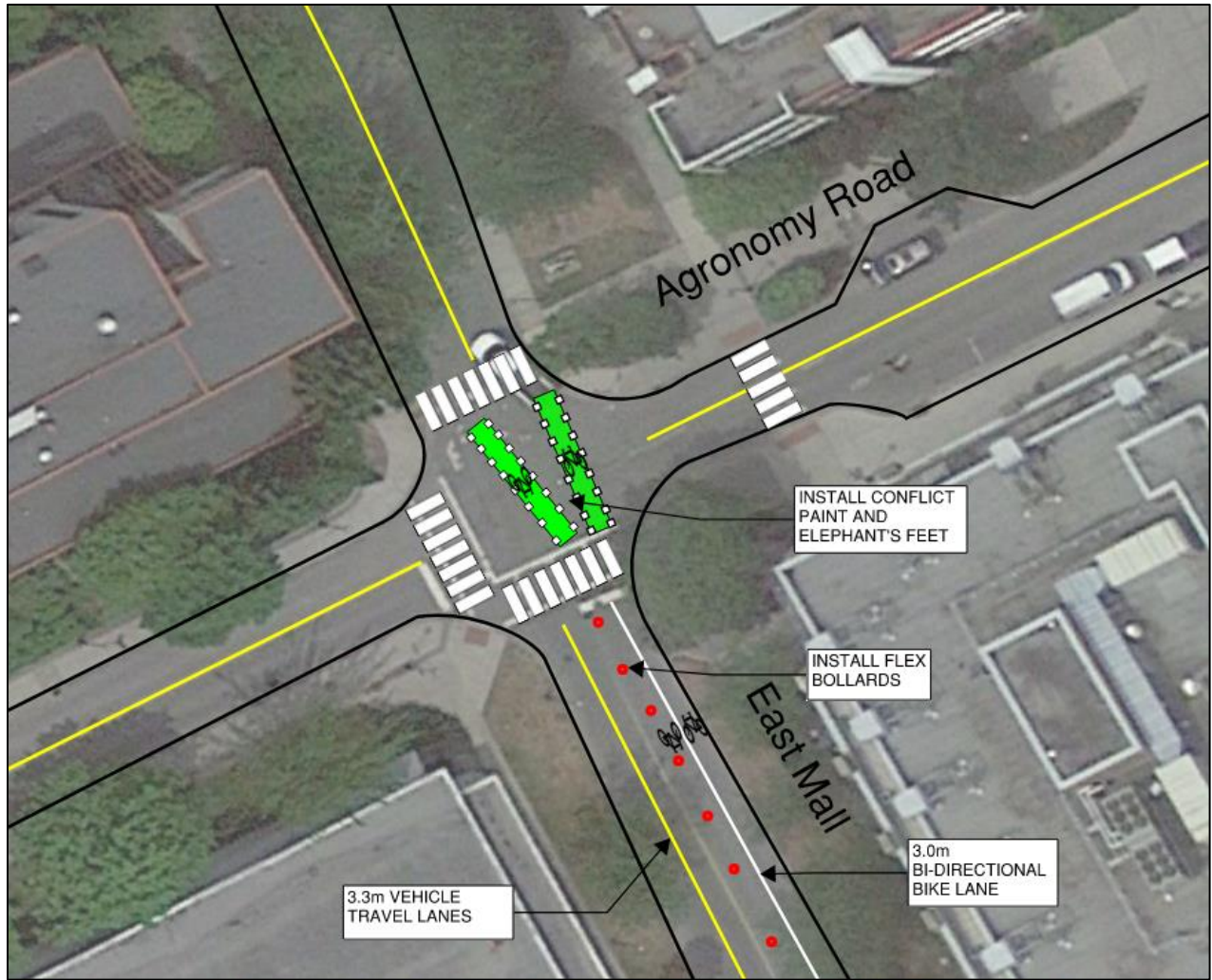


Figure 7: Proposed Changes at the Intersection of Agronomy Road and East Mall

### 3.4. SIGNAGE PLAN

The signage plan was designed in accordance with the Manual of Standard Traffic Signs & Pavement Markings from the British Columbia Ministry of Transportation and Highways. Many of the new proposed traffic signs are due to the greenway shifting the travel lanes to the east side of the boulevard. Due to the future Stadium Neighbourhood changes, two zebra crosswalks will be added to facilitate anticipated foot traffic growth on the south end. Additional time-limited parking spots will follow the current design, indicated by white paint. The proposed signage plan can be found in Appendix A.

## 4. STRUCTURAL CANOPY DESIGN

The detailed structural design and analysis of the proposed pedestrian canopy is outlined in this section. The canopy structure will be made up of wide flange steel beams and columns with tempered glass panels. The structure will be constructed on the south side of Agronomy Road, due to the existing awnings and trees/shrubs on the north side the north side that would obstruct the proposed canopy. As shown in Figure 8 below, the canopy will have one 12.73-metre section and one 54.13-metre section separated by the parking lot driveway. The total length of the structure will be 66.86-metres.

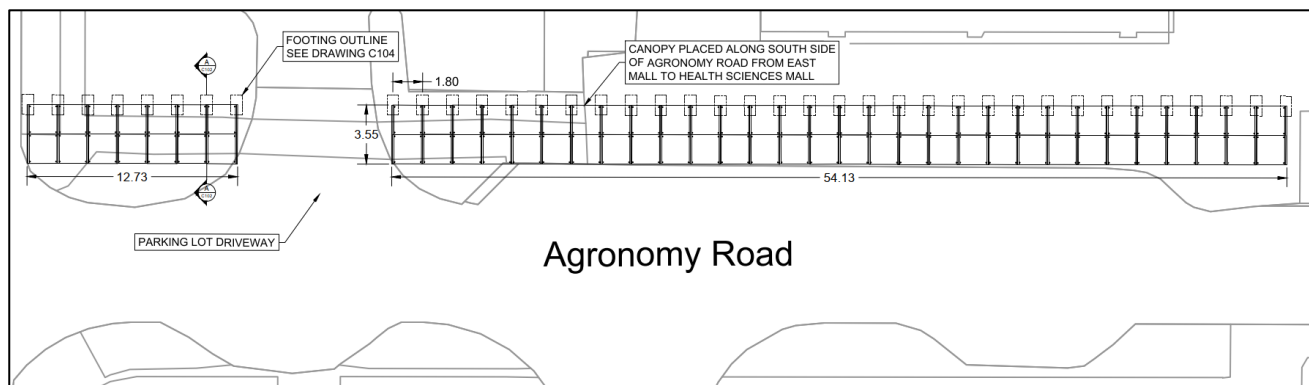


Figure 8: Pedestrian canopy plan

The detailed design process consists of sizing the main structural members, designing the connections, and sizing the foundations. Technical drawings and specifications for the canopy can be found in Appendix A.

### 4.1. DESIGN LOADINGS

The loading on the structure was determined in accordance with NBC 2015 and consists of dead, snow, and wind loads. Live loads and earthquake loads were not included in this analysis. The considered loads will determine the member sizes and connection detail based on Ultimate Limit States or Serviceability Limit States. Since the canopy structure will not have live loading, the design of the members and connections will be governed by serviceability requirements. A summary of loads is given below:

Table 7: Summary of load combinations used for analysis

Case	NBC 2015 Load Combination	Load on Cantilever [kN/m]	Load on Column [kN]
1	1.4D	1.06	5.85
2	1.25D + 1.0S or 0.4W	2.42	10.54
<b>3</b>	<b>1.25D + 1.5S + 0.4W</b>	<b>3.59</b>	<b>14.75</b>
4	1.25D + 1.4W + 0.5S	3.19	13.31
<b>Serv.</b>	<b>1.0D + 1.0S + 1.0W</b>	<b>3.31</b>	<b>13.37</b>

#### 4.1.1. SNOW LOAD

Snow loading for the structure were determined in accordance with NBC 2015 Clause 4.1.6. NBC specified a 1.8-kPa 1-in-50-year ground snow load for the Vancouver City Hall region. The importance factor for this structure was assumed to be 1.0. The final snow load to be used for analysis was 1.64-kPa. Further detailed calculations can be found in Appendix D.

#### 4.1.2. WIND LOAD

Wind loading for the structure was determined in accordance with NBC 2015 Clause 4.1.7. The external and internal pressure cases were calculated, and both resulted in a wind uplift of 1.20kPa. The reference velocity pressure used was 0.45-kPa for the Vancouver City Hall region and the assumed importance factor was 1.0. Further detailed calculations can be found in Appendix D.

### 4.2. STRUCTURAL ANALYSIS

The analysis completed on the structure consisted of a typical section (ie. cantilever and column) with fixed joints and supports. Loads from the previous section were applied as shown in Figure 8 below. The snow load was applied with global projected coordinate system, wind load was applied in the local coordinate system, and dead load was applied with global coordinate system. The analysis model is shown in Figure 9.

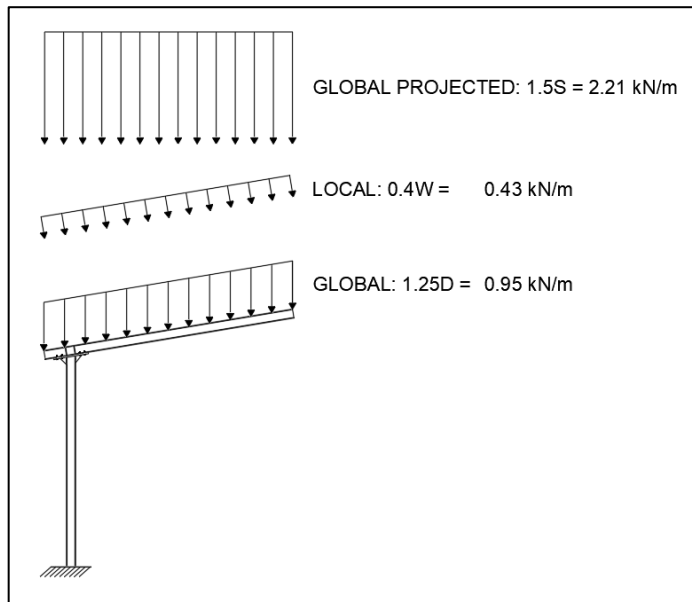


Figure 9: Loads inputted into S-Frame

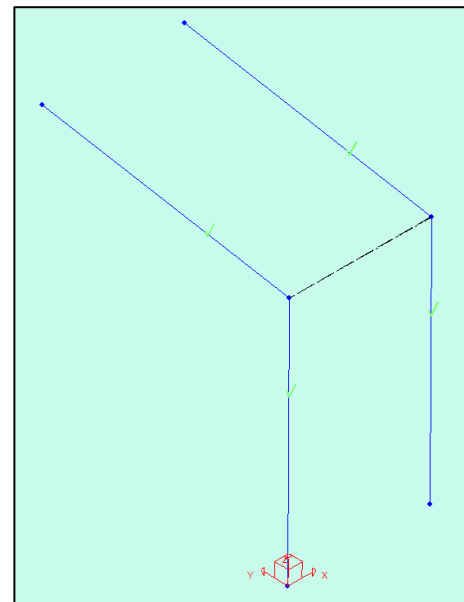


Figure 10: S-Frame analysis model

All ultimate limit states requirements as specified by NBC 2015 were met. See Appendix D for the code checks from S-Frame. The wide flange section that resulted from serviceability limit states was a W200x31 section profile. The deflection at the outer edge of the cantilever beam due to the serviceability load combinations was 33mm. A L/120 deflection requirement results in a maximum displacement of 30mm. As a result, a standard 10-millimetre thick, 100-millimetre-high stiffener plate will be added on both sides of the top and bottom connection. See Appendix A for detail drawings.

### 4.3. CONNECTION DESIGN

The top and bottom connections as identified in Figure 9 above will be a fixed moment end plate design with similar hex bolt layouts. The end plates will be welded to the column using a fillet weld 6-millimetres thick all around the wide flange section. Three checks on the connection capacities due to internal bending transfers were completed. The prying force on the end plate, yielding of the end plate, and strength of the welds were all passed for both connections. See Appendix A for connection details and Appendix D for calculations.

### 4.4. FOOTING DESIGN

The plan dimensions of the footing were initially determined based on the soil type obtained from the Piteau Geotechnical Report. The specified soil type was dense sand with a soil bearing capacity of 150-kPa (based on NBC 2015 Table 9.4.4.1). The resulting plan dimensions are 0.7-meters wide by 1.2-meters long. The depth of the footing was found based on the required overturning resistance of the canopy loads. A depth of

1.3-meters was found to be sufficient to resist the overturning moment. See Appendix A for connection details and Appendix D for calculations.

## 4.5. CONSTRUCTION CONSIDERATIONS

A construction plan was developed in accordance with NBC 2015. Since the location of the pedestrian canopy will be in a relatively high traffic area, construction fencing, and barricades will adhere to Clause 8.2.1 of NBC 2015 during weekdays. Construction of the canopy shall occur inside an enclosed area with at least 2.0-meters of distance between any adjacent pedestrian areas. Additionally, excavations for the canopy footing shall be kept clear of water to prevent soil and water contamination, and necessary shoring or bracing shall be installed. Proper pedestrian and vehicular traffic management should be implemented as necessary and construction waste materials should be disposed of appropriately.

## 5. UTILITIES DESIGN

The following section details the municipal utilities engineering design including the water, sanitary, and stormwater network components.

### 5.1. EXISTING UTILITIES

An initial assessment of the existing utilities has been conducted, based on information provided by the client. While a PDF displaying a plan view of the underground utilities was provided by UBC Seeds, titled UtilityMasterMap2019, it is not up to date nor high enough resolution to determine accurate alignments and dimensions. As-built drawings for the project area were not available, and so no detailed location and depth information could be found. Figure 11 below shows a snippet of the master utility map. Utility relocations and diversions do not fall under the original scope, and so were not considered for this project. Further, certain utilities are likely to fall under different ownership groups such as FortisBC, and the decision to conduct realignment ultimately does not fall under the project teams' control. The proposed design is generally limited to the road surface and does not introduce any major underground elements that would require the current alignments to be moved. However, an analysis of the water, sanitary, and stormwater systems was conducted to determine if upsizing will be required and can be found in the subsequent report sections.

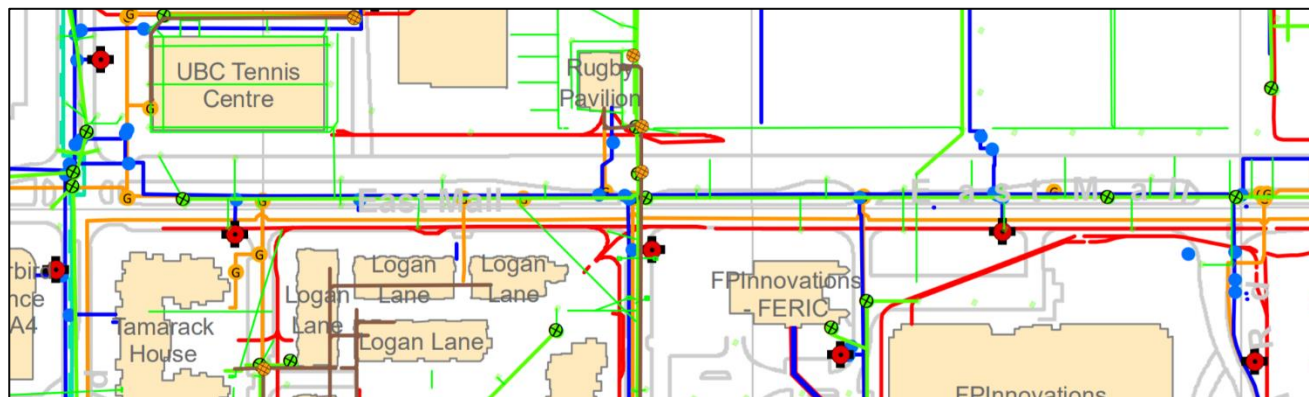


Figure 11: Existing underground utilities

#### 5.1.1. UTILITIES DESIGN

The following table summarizes the existing utilities identified based on available resources, as well as approximate dimensions, typical depths of cover, and key comments:

Table 8: Existing Utility Summary

Utility	Dimensions (mm)	Typical Depth of Cover (mm)	Comments
Communications	400 x 600	600	<ul style="list-style-type: none"> <li>Not shown on master utilities plan, but identified by UBC SEEDS</li> <li>Likely third-party owned</li> </ul>
Electrical	400 x 600	600	<ul style="list-style-type: none"> <li>Not shown on master utilities plan, but identified by UBC SEEDS</li> <li>Likely third-party owned</li> </ul>
Natural Gas	Ø 50 to Ø 100	600	<ul style="list-style-type: none"> <li>Service connections not shown</li> <li>Likely third-party owned</li> </ul>
Water	Ø 200 to Ø 250	900	<ul style="list-style-type: none"> <li>Likely to be small diameter</li> <li>Service connections not shown</li> </ul>
District Energy (Water)	Unknown	Unknown	<ul style="list-style-type: none"> <li>Not shown on master utilities plan, but identified on UBC Energy publications</li> <li>Located along Thunderbird Boulevard</li> <li>High-temperature pressurized main</li> </ul>
Sanitary	Ø 200 to Ø 450	1500 to 3000	<ul style="list-style-type: none"> <li>Manholes, service connections, and cleanout information not available</li> <li>No distinction made between gravity and pressurized mains</li> </ul>
Storm	Ø 300 to Ø 900	1500 to 3000	<ul style="list-style-type: none"> <li>Likely to be large diameter mains along East Mall</li> <li>Manhole and service connection information not available</li> </ul>

While the communications and electrical duct banks were not shown on the plan view sheet, typical construction practice is to install close to the surface and underneath the main roadway or sidewalk. Based on an inspection of the project area, most buildings directly facing East Mall are only reachable by mains along the corridor and so must have service connections not shown in the mastery utility map. Service connections are generally installed perpendicular to the main utility with less depth of cover. Other major infrastructure components like manholes are visibly present in the project area, though they are not indicated in the utility map.

### 5.1.2. CONSTRUCTION CONSIDERATIONS

Based on the City of Vancouver’s Engineering Design Guides, the geotechnical requirements for bus lanes call for a minimum of 50mm of surface mix, 180mm of base of mix, 150mm of 19mm crushed granular base, and 300mm of 17mm crushed granular base for a total excavation depth of 680mm beneath the road surface. Communications, electrical, and natural gas conduits will fall directly in the excavation zone and water mains



are likely to be encountered where over excavation is required. Information on the district energy system is not available but is likely to have similar specifications as the water mains. Based on the estimated depth of cover, sanitary and storm mains are unlikely to be encountered during construction. However, service connections to adjacent properties are generally found at shallower depths and could be located in the excavation area. Sanitary and storm sewer manholes also fall within the reconfiguration area, though are identifiable prior to construction. As such, safety during construction is the primary concern, and our team has outlined considerations in the General Notes of the drawing package and the Construction Specifications including the following key requirements:

- The Contractor will perform a detailed utility locate to confirm the alignments and depths of existing utilities prior to commencing construction
- Hand excavation will be required within 300mm of any pressurized utilities
- The Consultant will be contacted prior to any construction work requiring the removal or shutdown of an existing utility

## 5.2. WATER AND SANITARY

UBC owns and operates both the water distribution and sanitary sewer networks on campus. Both have been identified within the East Mall corridor, as well as the Academic District Energy System which intersects along Thunderbird Boulevard. Sheets W101 and S101 in the drawing package provide plan-view drawings of these systems, as well as construction comments and notes. The focus of this project is a road reconfiguration for East Mall and does not introduce any new developments to the project area that need to be serviced by the existing water or sanitary networks. As such, the post-development demands on these underground utilities will be unchanged from the pre-development demand. A survey of the existing hydrants was conducted, and no relocation will be required for the final design. No improvements will be required, and thus the emphasis will be to maintain service and minimize disturbances during the construction phase.

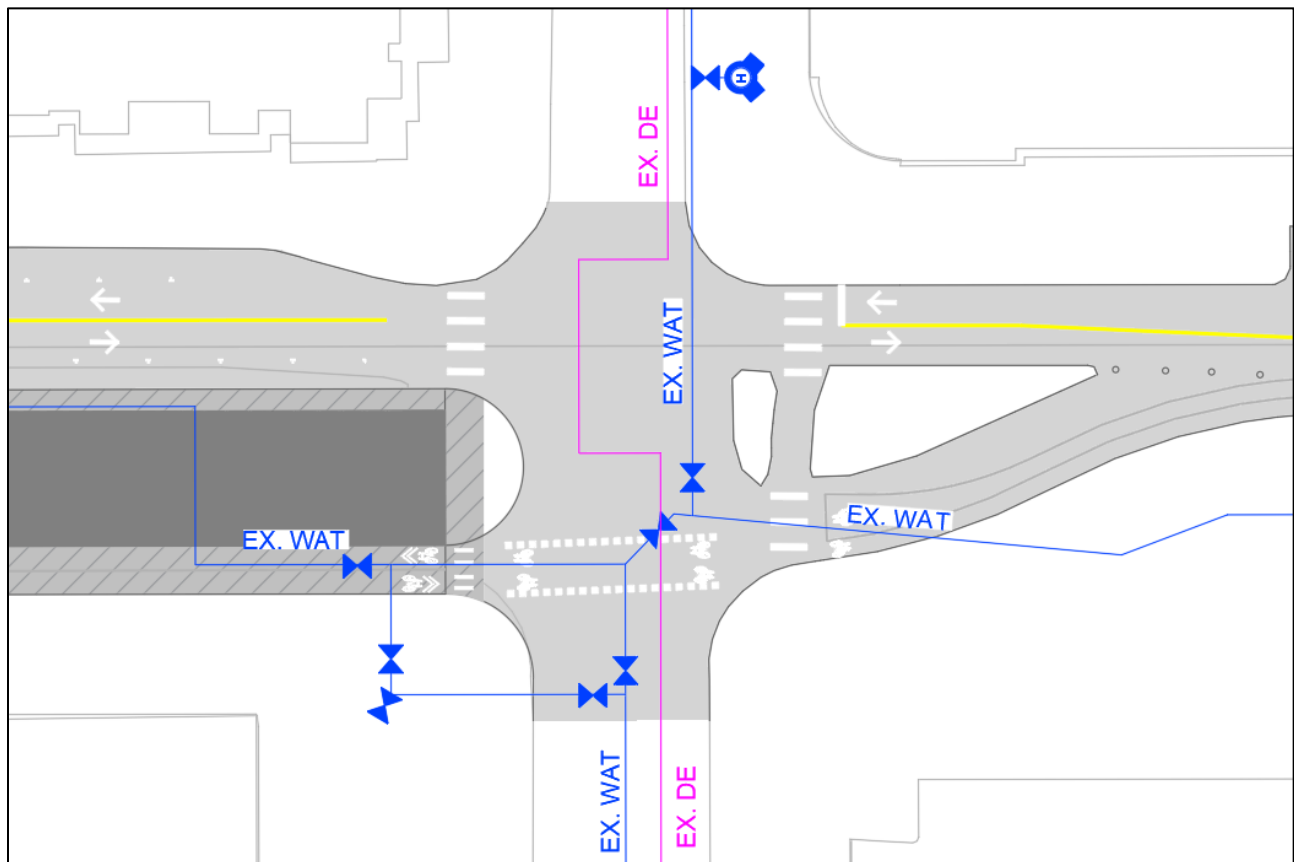


Figure 12: Water Utilities Map at Thunderbird Blvd. and East Mall

In addition to the previously identified construction considerations, stub lengths and pipe loops have also been identified in the water distribution system. Flow can often become stagnant in these areas, and potentially lead to health concerns if the system is not adequately maintained. UBC will be contacted to determine if these sections should be removed or grouted. Hydrants, manholes, and other ground-level infrastructure

should remain in place during construction. Service should not be stopped without first getting approval from both the Consultant as well as UBC. Without further information, the sanitary and district energy mains should both be considered to be pressurized and treated as high-risk. Excavation should be done by hand around the mains to avoid potentially damaging them.

### 5.3. STORMWATER

Ensuring that UBC's sustainability initiatives were met was one of the main design objectives, and proper stormwater management plays a critical role in this. The existing corridor has a paved roadway with a shared bicycle lane and an adjacent sidewalk drained through catch basins along the curb line. Rainfall is then directed into the stormwater sewer system, which is owned and operated by UBC. From Thunderbird Blvd. to Agronomy, runoff is directed into the University's Western catchment and out through a creek adjacent to Wreck Beach. South of Thunderbird, runoff is directed along into the University's 16th Avenue Catchment area and the majority drains out within Pacific Spirit Park. While a detailed control plan is not required based on UBC's technical guidelines, the following section outlines the management philosophy for the site.

#### 5.3.1. MANAGEMENT

Throughout the design process, our team minimized runoff and the amount of impermeable area introduced wherever possible. Decreasing the travel lane widths and specifying permeable pavement for the new sidewalks and bicycle paths are two key features of the new corridor that reduces the impermeable area. These impermeable surfaces are associated with the fast runoff response in the system and reducing the tributary area that drains into pipe network reduces the total runoff volume and by extension reduces the peak flow entering the system. The capture method for the roadway has remained the same as before, with both directions sloped towards the adjacent gutter line. According to the City of Surrey's Design criteria, catch basins should serve a maximum catchment area of 500m<sup>2</sup>. With a typical road width of 12.2m, catch basins will be spaced every 35m including a factor of safety. However, this spacing is actually less than what is currently being provided by the existing catch basins. Furthermore, as the stormwater main does not need to be upsized, removing the existing basin leads then installing new ones is redundant and adds unnecessary construction complexity. As a result, catch basins on the roadway will be relocated to follow the new curb line and the leads will be adjusted to suit. Existing basins should be reused wherever possible as long as they are in adequate condition to reduce construction waste.

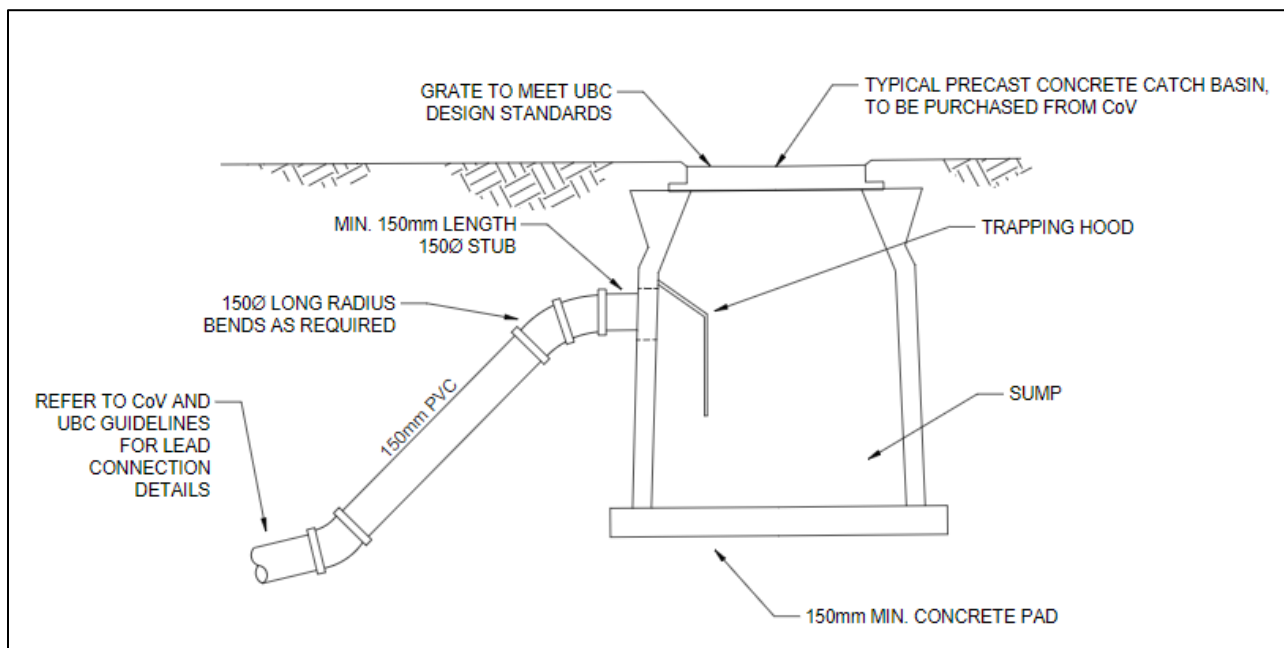


Figure 13: Typical Catch Basin

Landscaped areas like the greenway do not drain into UBC's system, and precipitation is expected to percolate into the groundwater. In accordance with UBC's technical guidelines, the greenspace will also feature a 450mm layer of absorbent topsoil to promote infiltration. More extensive gardening and planting on the proposed greenspace helps to improve stormwater quality by acting as a filter prior to percolation. Similarly, the permeable concrete also allows stormwater to be kept on site instead of captured into the sewer system and conveyed away. From the Integrated Stormwater Management Plan, UBC's preferred implementation strategy is to use detention to capture flooding. As such, the permeable concrete was also designed to have a base aggregate reservoir capable of storing a major storm event. Drawing D101 shows a plan view of the stormwater utilities in the project area, including landscaped and permeable areas.

### 5.3.2. PERMEABLE CONCRETE

Permeable concrete is still a relatively developing field, and there are currently no widely accepted standards. The design for the permeable concrete was developed based on best practices and guidelines from the City of Vancouver, National Ready Mixed Concrete Association, UNH Stormwater Centre, and Flood Testing Labs. Layer depths were determined based on the capacity required to store a 10-year 24-hour duration intensity storm, assuming no infiltration into the subgrade. The final design offers 95.2mm of storage compared to an expected 67.2mm of precipitation. This contingency can help to detain excess rainfall from the adjacent landscaped areas and prevent ponding in extreme events. Detailed calculations are available in Appendix E.

Table 9 summarizes the target construction specifications for the permeable concrete, and Figure 14 below illustrates the required layers for construction:

Table 9: Permeable Concrete Specifications

Specification	Requirement
28 Day Compressive Strength	20 MPa
Infiltration Rate	8600 mm/hr
Void Space	15%
Unit Weight	1500 kg/m <sup>3</sup> to 2000 kg/m <sup>3</sup>
Slump	15cm to 18cm

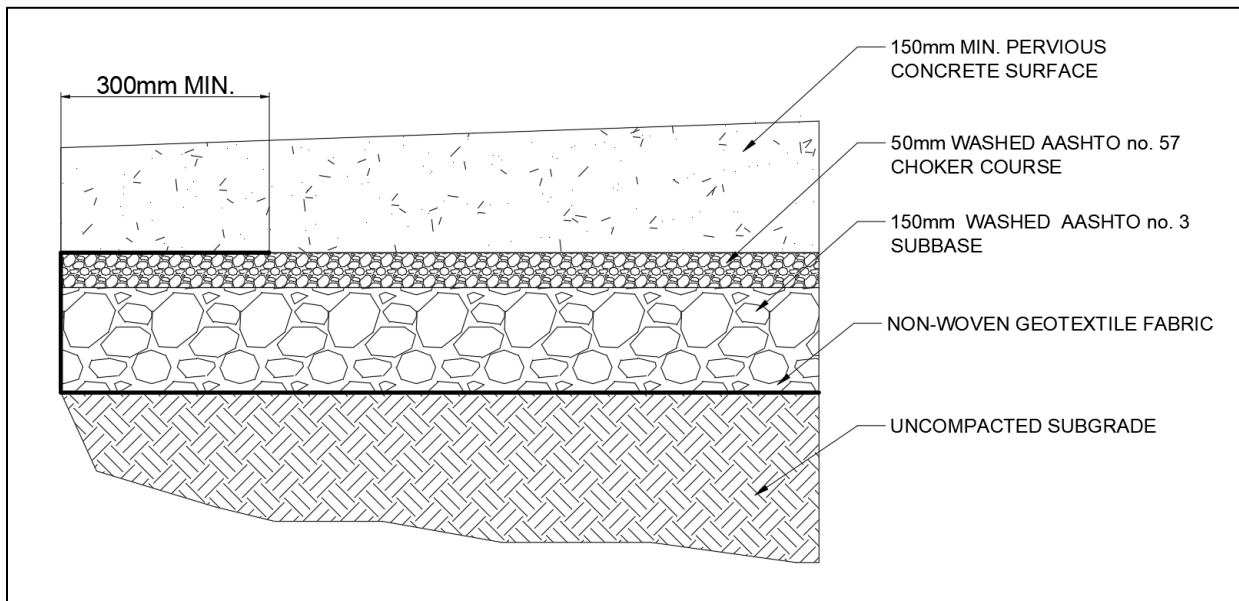


Figure 14: Required permeable concrete layers

A detailed mix design was considered to be outside of the scope of the project, and the Contractor will be expected to develop a final mix design meeting the above specifications. Due to differences in load response, permeable concrete requires slightly different procedures than conventional concrete. Detailed specifications are provided in the Construction Specifications, but the following key points are identified:

- Conventional strength tests are not recommended as compaction is highly variable in cylinder tests for permeable concrete. Instead, a void-density curve should be established for the final mix-design and used for quality assurance during construction
- Concrete should be moistened then covered for curing within 20 minutes of initial placement and compaction

- A minimum of two panel tests should be conducted on site according to ACI 522.1-13 to establish acceptable ranges for hardened concrete
- Three cores will be tested every 75 m<sup>3</sup> poured to verify infiltration rate, dimensions, and average hardened density are within values obtained from the test panels in accordance with ASTM C1754

## 6. GREENSPACE

The final design includes a multi-purpose green space separating the travel lanes and the cycling path. One of the primary objectives is to encourage use active and sustainable modes of transportation. This new greenspace encourages provides a place for people to gather and enjoy the surrounding landscape, thereby improving the sense of community and health of residents. The landscape architecture design for this area was based on UBC's sustainability recommendations and past examples of integrated spaces like the Arbutus Greenway.

The final greenspace design involves the transplanting the existing maple trees and the planting of 4 new trees at each crossing to further improve on the aesthetic of the corridor. The four new trees to be planted are the Saucer Magnolia, Weeping Cherry, Eastern Redbud, and Red Oak. Additionally, the greenspace features a community garden consisting of several different species of plants at various locations of the median. A summary of the plants utilized in the final design is summarized in the figures below.



Figure 15: Hydrangeas ([gardeningknowhow.com](http://gardeningknowhow.com))



Figure 16: Rudbeckia ([oscseeds.com](http://oscseeds.com))



Figure 17: Fountain Grass ([gardeningknowhow.com](http://gardeningknowhow.com))



Figure 18: Meadow Sage ([americanmeadows.com](http://americanmeadows.com))



Figure 19: Tulips ([americanmeadows.com](http://americanmeadows.com))

The overall layout and locations of the various components of the greenspace is shown in Figure 20 and 21 below. Figure 20 displays the greenspace plan from Thunderbird Blvd to Eagles Dr, and Figure 21 displays Eagles Dr. to Stadium Rd.

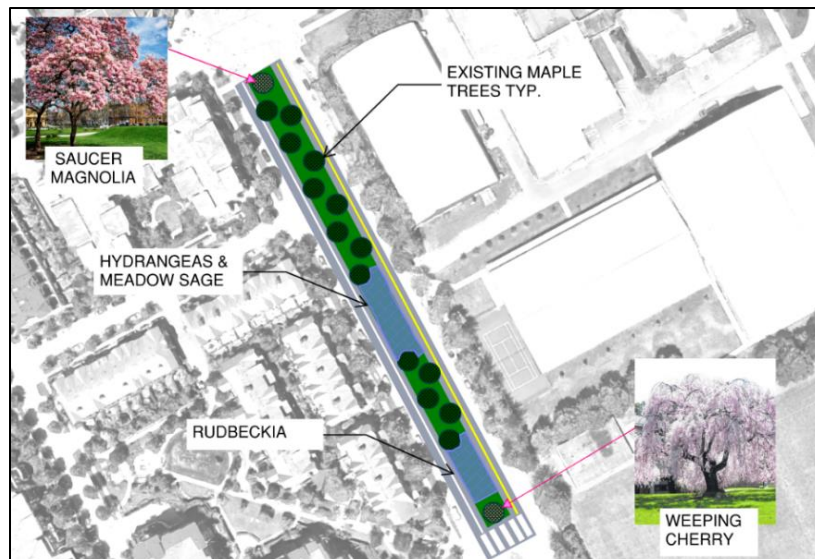


Figure 20: Greenspace Plan from Thunderbird Blvd to Eagles Dr.



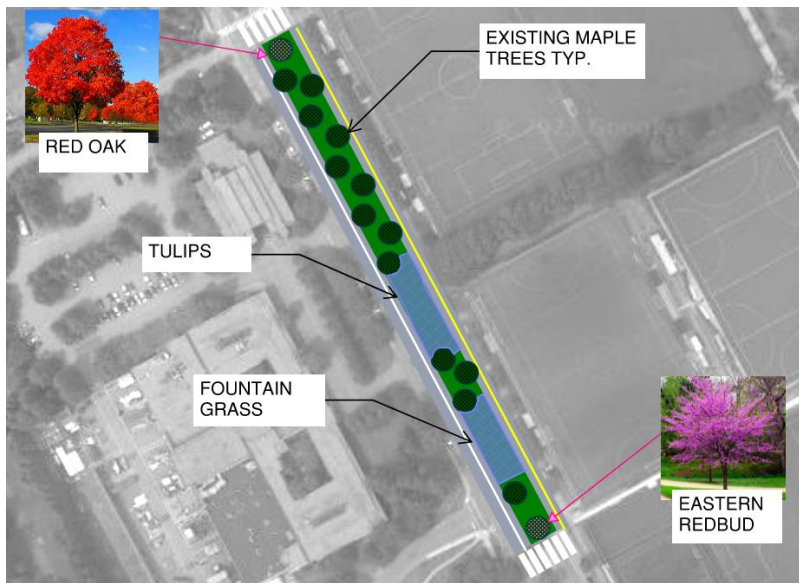


Figure 21: Greenspace Plan from Eagles Dr. to Stadium Rd.

Construction requirements for the greenspace include the following:

Construction for the greenspace is expected to be done in accordance with the UBC Exterior Improvements Technical Guidelines. In conjunction with current best practices the following key requirements have been identified:

- Where possible, existing trees along the current median are expected to be transplanted to their new proposed locations
- Newly planted and transplanted trees must be spaced apart according to their mature canopy spread
- Erosion control devices such as silt fencing shall be installed to prevent siltation and/or erosion within the tree protection zone
- Ensure that soil texture, fertility and drainage at the new planting site by laying composted bark mulch and absorbent topsoil
- Soil should be tested prior to installation to ensure acidity and nutrient composition is adequate for the specified plants

# 7. CONSTRUCTION MANAGEMENT

This section will provide information regarding construction sequencing, anticipated issues during construction, the construction schedule, and our traffic management plan.

## 7.1. SEQUENCING

To mitigate disruptions to the overall network, construction activity has been sequenced into five sections, each relating to a specific portion of East Mall. The bulk of the work has also been further divided into three phases. Figure 22 details the scope of each specific sequence. For full breakdown of tasks and timelines, refer to Section 7.3. Materials and equipment rentals will be procured at the start of each section. Reviews will be undertaken at the end of each activity, with an audit at project turnover.



Figure 22: Construction phases and sequencing

## 7.2. ANTICIPATED ISSUES

A detailed risk assessment was conducted to outline potential setbacks during construction. Table 10 provided below presents several key hazards identified, along with their likelihood of occurrence and impact to the project. A more detailed description of the hazards is also provided in this section. Refer to Appendix H for the risk register in its entirety.

Table 10: Risk analysis of construction method

Risk	Likelihood	Impact
Design changes	Low	High
On-site incidents	Moderate	Moderate
Interrupting Buried Utilities	Low	High
Traffic Delays	Moderate	Moderate
Damage during tree transplant	Moderate	Low

### Design changes

Due to continuous stakeholder engagement, there is potential for varying magnitudes of design changes.

Unforeseen site conditions might also require change orders during construction. A substantial change could greatly impact the traffic and stormwater analysis, resulting in schedule delays and cost revisions. To mitigate

this, site constraints will be clearly communicated to stakeholders and contractors. Our team will also address issues case by case to mitigate design changes.

### **On site incidents**

This hazard includes both worker and pedestrian accidents on site. Due to the sheer number of days worked, it was deemed a moderately probable occurrence. Impacts would vary depending on the incident. To mitigate this, procedures will be developed with worker safety at the forefront. A daily hazard assessment of the site must be conducted prior to start of work by the supervisor. Routine site inspections will be conducted to ensure WorkSafeBC compliance. Equipment will only be operated by qualified personnel. Adequate signage and fencing will block off public spaces and minimize contact with pedestrians.

### **Interrupting Buried Utilities**

Due to the limited information regarding buried utilities, there is potential for accidental contact during construction work. Depending on the affected system, the impact can range from moderate to high. Mitigation will require detailed confirmation of pipe depths at areas with substantial earthwork. Amount of excavation has also been optimized in the design. Hand digging will also be done when in proximity to known utility locations. Given the new development proposed at Stadium Road, it is likely utility owners may already have upgrade works planned. In this case, construction could be coordinated so that the upgrade works can happen in conjunction with the road reconstruction to minimize disruption to the community.

### **Traffic Delays**

Congestion induced by site work will limit access and result in project delays. As such, the East Mall corridor must be able to shoulder a majority of the usual volumes despite construction. Traffic delays were classified as a moderate probability; it will be lowered through the phasing of construction work. Mitigation will consist of the provided Traffic Management Plan and ensuring clear communication with contractors. A bulk of the work is also schedule for the summer with lower volumes. Equipment transport will also occur outside of peak hours when possible.

### **Damage to trees**

With 47 existing trees requiring uplift, there is a moderate probability of damage during the process. To mitigate this, work will be done in accordance with the Tree Protection Guidelines outlined in the UBC Vancouver Campus Plan Part 3: Design Guidelines (2014).

### 7.3. CONSTRUCTION SCHEDULE

Commencing May 3<sup>rd</sup>, 2021, construction duration was estimated at around nine months, completing on December 16<sup>th</sup>, 2021. Workdays were taken as Monday to Friday, eight-hour days with statutory holidays off. A schedule summary is provided in Table 11. For a full task breakdown and Gantt chart, refer to Appendix G.

Table 11: Key construction dates

Activity	Start (2021)	End (2021)
Site Preparation	May 3 <sup>rd</sup>	May 7 <sup>th</sup>
Phase 1 Construction	May 10 <sup>th</sup>	June 11 <sup>th</sup>
Canopy Installation	June 14 <sup>th</sup>	July 23 <sup>rd</sup>
Phase 2 Construction	June 14 <sup>th</sup>	September 2 <sup>nd</sup>
Phase 3 Construction	September 2 <sup>nd</sup>	December 6 <sup>th</sup>
Site Clean-up	December 7 <sup>th</sup>	December 16 <sup>th</sup>

To prevent congestion along East Mall, construction was sectioned into chronological phases. Figure 23 below presents the scope for each phase. Phase one includes the Thunderbird & East Mall intersection upgrades along with roadwork north to Agronomy Road and the pedestrian canopy. Canopy installation will begin mid-June with to minimize roadway disruption. The structure will be complete and inspected by August, allow for immediate use during the fall months. The remaining work along East Mall is divided into two phases. Phase two details the median removal while phase three is dedicated to the new median and greenspace installation. Dividing the work allows traffic to be shifted onto the open lane with capacity for two lane flow. Meeting the usual capacity is essential as phase three will extend into the 2021 winter semester. Temporary parking and traffic control measures will be required.

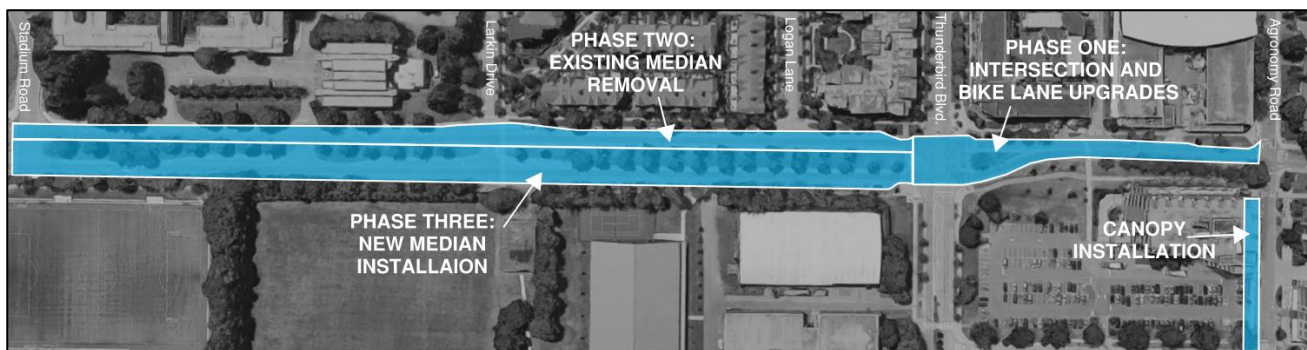


Figure 23: Construction phases

### 7.4. TRAFFIC MANAGEMENT PLAN

Under project classifications set out by the Ministry of Transportation and Infrastructure, the redesign falls under Category 2: moderate impacts on the travelling public and involves some complexity. As such, a full

traffic control plan will be required. The figures below provide our management plan for all phases of the project. Temporary signage codes are derived from the BC Traffic Management Manual for Work on Roadways (2016)

### 7.4.1. PHASE 1

Work zones will be divided into halves of road. The first half will require the closing of the southbound lane. While work is in progress, the adjacent lane will allow for two-way traffic flow, with a total width of 18ft. Traffic flow operators and temporary 15 mph speed limit signs will be posted at appropriate intervals to regulate traffic. Figure 17 details the first half of phase one and the required signage and personal on site.

Occurring synchronously with phase 1 is the construction of the pedestrian canopy. To prevent congestion, equipment and operational vehicles will detour down Agronomy and Health Science Mal into the highlighted alleyway. The southern sidewalk of Agronomy will be closed with pedestrian demand relocated to the north.

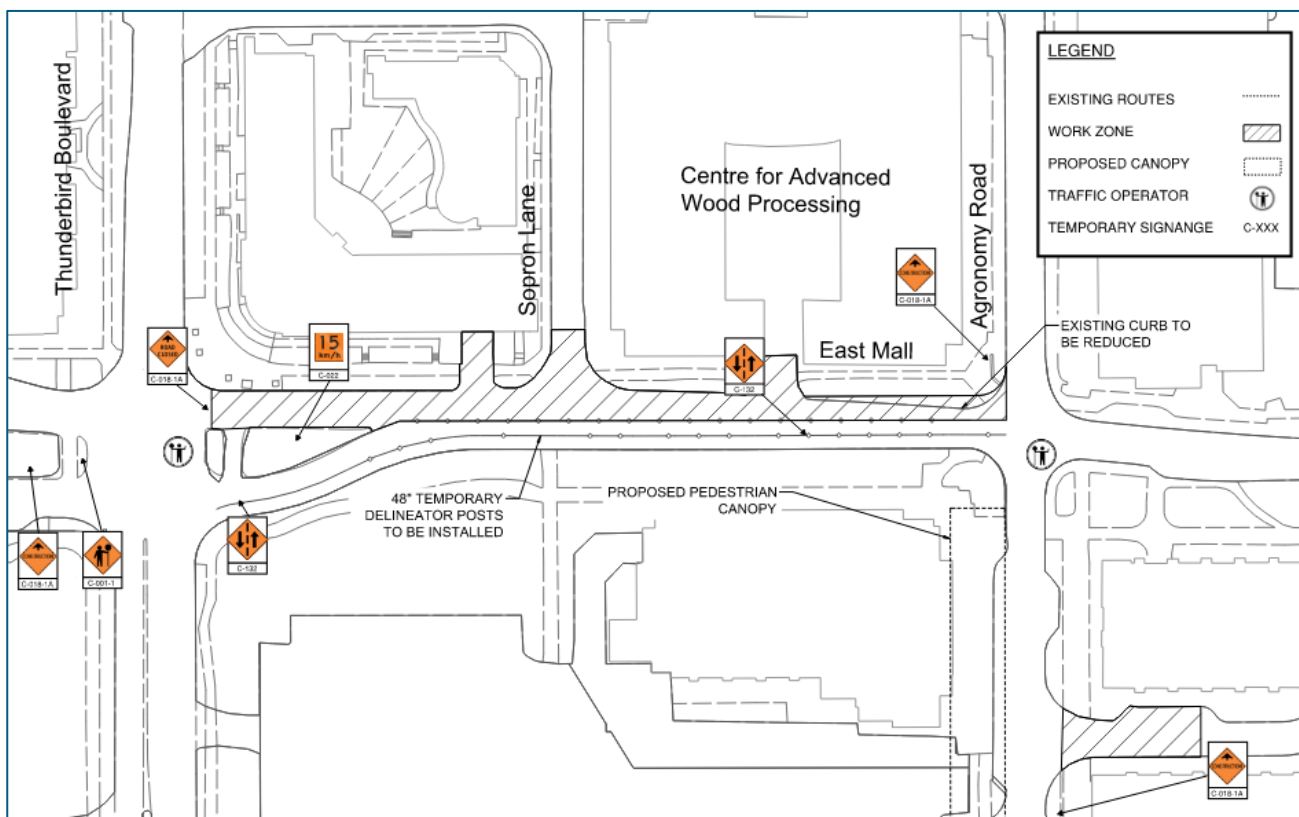


Figure 24: Phase 1 traffic management plan

### 7.4.2. PHASE 2

Existing median removal headlines phase two which will require work on the southbound lane of East Mall. The wide roadway easily allows for two-way traffic flows on the adjacent lane. Parking will be restricted to meet demands. Adequate signage and pylons will be placed alongside traffic flow operators. Figure 18 below

details the phase two configuration. A temporary 15 mph vehicle speed limit will be imposed for pedestrian and worker safety.

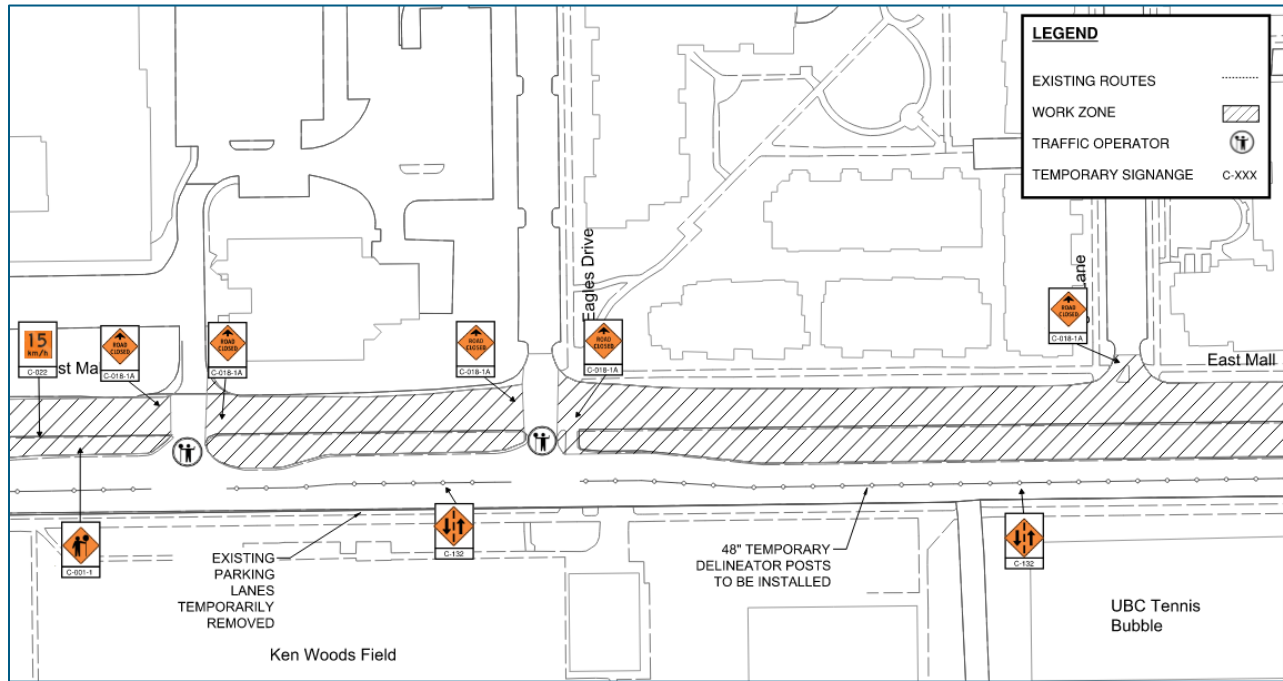


Figure 25: Phase 2 traffic management plan

### 7.4.3. PHASE 3

Phase three will require the closing of the northbound lane, with the volume shifted on the finished southbound lane. Similar to phase two, a temporary no parking limit on the southbound lane will be enacted to meet capacity. A 15-mph vehicle speed limited will also be imposed for worker and pedestrian safety.

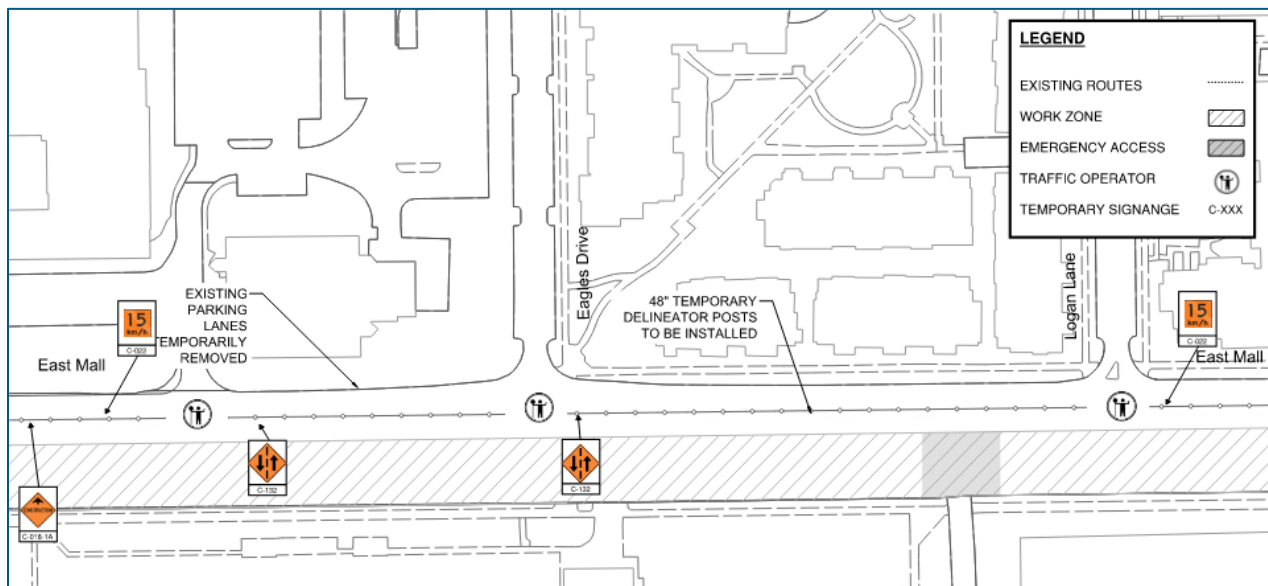


Figure 26: Phase 3 traffic management plan

## 8. COST ESTIMATE

The total project is estimated to cost \$5,163,449, with an annual operations & maintenance cost of \$23,500. A high-level cost breakdown is provided in Table 12. To account for potential uncertainty during construction, a 15% contingency has been assigned to overall costs. For the full detailed Class A Cost Estimate, refer to Appendix F. Unit cost for specific materials has been derived from cost guides from different locales and times. As such, RSMean Cost Indices were used to normalize costs when applicable.

Table 12: Cost Summary

<b>Design</b>		<b>\$179,600</b>
	Development	\$179,600
<b>Construction</b>		<b>\$3,826,224</b>
	General Permitting	\$28,100
	On-Site Personnel	\$324,000
	General Construction	\$450,000
	Site Preparation	\$690,730
	Road Replacement	\$797,875
	Median Installation	\$131,725
	Bike Lanes & Sidewalks	\$118,025
	Stormwater Facilities	\$100,000
	Greenspace	\$646,650
	Permanent Traffic Controls	\$177,035
	Structural	\$188,084
	End of Construction	\$174,000
<b>Maintenance &amp; Operations</b>		<b>\$23,500</b>
<b>Contingency (15%)</b>		<b>\$604,399</b>
	Total Cost	\$4,610,222
	PST (7%)	\$322,716
	GST (5%)	\$230,511
	<b>Total Cost + Tax</b>	<b>\$5,163,449</b>

## 9. SERVICE LIFE MAINTENANCE PLAN

This section will outline the potential maintenance concerns associated with the new roadway, canopy, utility, and greenspace upgrades. The items below are only common issues and therefore not exhaustive. Additional issues may arise throughout the lifecycle of the project.

### 9.1. TRANSPORTATION

The main component of the road requiring maintenance is the asphalt. The asphalt road in our final design has a design life of 18 years, after which the road will require repaving. However, to achieve this design life maintaining the driving surface and other roadside upkeep is required. The road maintenance plan consists of the following:

Table 13: Maintenance summary and frequency for roadway

Activity	Maintenance Frequency
Crack sealing	As required with annual inspections
Snow and ice control	As required seasonally
Pothole patching	As required with annual inspections
Signage repair	As required with annual inspections
Pavement marking repair	As required with annual inspections

Effective road maintenance addresses damage early. Preventive maintenance for the road will be performance based. This approach maximizes the service life and reduces long term costs of the project.

### 9.2. STRUCTURAL

The hot dip galvanized steel canopy has a design life of 70 years. Hot dip galvanized steel structures provide long-term durability. The main concern for the steel canopy is corrosion due to it being located outdoors in a wet climate. That is why a zinc coating was selected since it would be able to provide the proper protection. A Hot Dip Galvanized coating is known for its durability and low maintenance; therefore, the maintenance plan is not overly involved and consists of the following:

Table 14: Maintenance frequency and summary for canopy

Activity	Frequency
Inspect and repair damaged welds	As required with annual inspections
Repair corrosion on the steel by brushing off any rust with a hard plastic bristle brush and repainting with Zingalu spray	As required with semi-annual inspections



### 9.3. UTILITIES

No new utility mains are installed as part of this project, and so the service life of the existing mains should be unchanged. New catch basins are specified to replace the existing, and the lifespan of a typical precast concrete catch basin including its service lead is estimated to be around 75 years. The on-site utilities do not require any special servicing plans, and the following suggestions are made on the basis of UBC’s Technical Guidelines to preserve utility lifespan:

Table 15: Maintenance summary and frequency for utilities

Activity	Maintenance Frequency
CCTV inspection of underground utility services shall be conducted every 5 years to identify potential leaks, root intrusion, among other damage in accordance with UBC Technical Guidelines Section 33 82 01	Once every 5 years
Sewers should be flushed in accordance with UBC Technical Guidelines Section 33 01 30.41	Yearly
Clear out catch basin sumps and surrounding grate area	Twice a year or whenever ponding is observed
Vacuum permeable concrete areas with regenerative vacuum sweeper	Yearly or whenever ponding is observed

### 9.4. GREENSPACE

The greenspace including its plants and trees all have an indefinite design life and should not require replacement as long proper care and maintenance is provided. Maintenance services are necessary to ensure that the landscape is healthy and looking good. The maintenance plan for the greenspace is the most intensive and consists of the following:

Table 16: Maintenance summary and frequency for greenspace

Activity	Maintenance Frequency
Standard lawn care of the land surrounding the garden including lawn mowing and other techniques to maintain the overall appearance of the garden itself	Bi-weekly during necessary seasons
Watering of all trees and plants along the greenspace	Daily
Renewing mulch to protect roots and soil moisture	Bi-weekly
Lawn fertilization and pest control	Annually
Tree and shrub insect treatments	As required with annual inspections
Leaf removal and trimming	Annually
Aeration and over seeding of the grass	Annually

# 10. REFERENCES

## Documents and Articles

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Streetsblog USA. “*Compelling Evidence That Wider Lanes Make City Streets More Dangerous*” <https://usa.streetsblog.org/2015/05/27/compelling-evidence-that-wider-lanes-make-city-streets-more-dangerous/#:~:text=Roads%20with%20the%20widest%20lanes,and%20crash%20severity%20into%20a%20count.>

The University of British Columbia. “*Guidelines by Division Specification*” [http://www.technicalguidelines.ubc.ca/technical/divisional\\_specs.html#Div03](http://www.technicalguidelines.ubc.ca/technical/divisional_specs.html#Div03)

The University of British Columbia. “*Integrated Stormwater Management Plan*” [https://planning.ubc.ca/sites/default/files/2019-11/PLAN\\_UBC\\_ISMP\\_Final2017.pdf](https://planning.ubc.ca/sites/default/files/2019-11/PLAN_UBC_ISMP_Final2017.pdf)

The University of British Columbia. “*Vancouver Campus Plan*” [https://planning.ubc.ca/sites/default/files/2019-11/PLAN\\_UBC\\_CampusPlanDesignGuidelines.pdf](https://planning.ubc.ca/sites/default/files/2019-11/PLAN_UBC_CampusPlanDesignGuidelines.pdf)

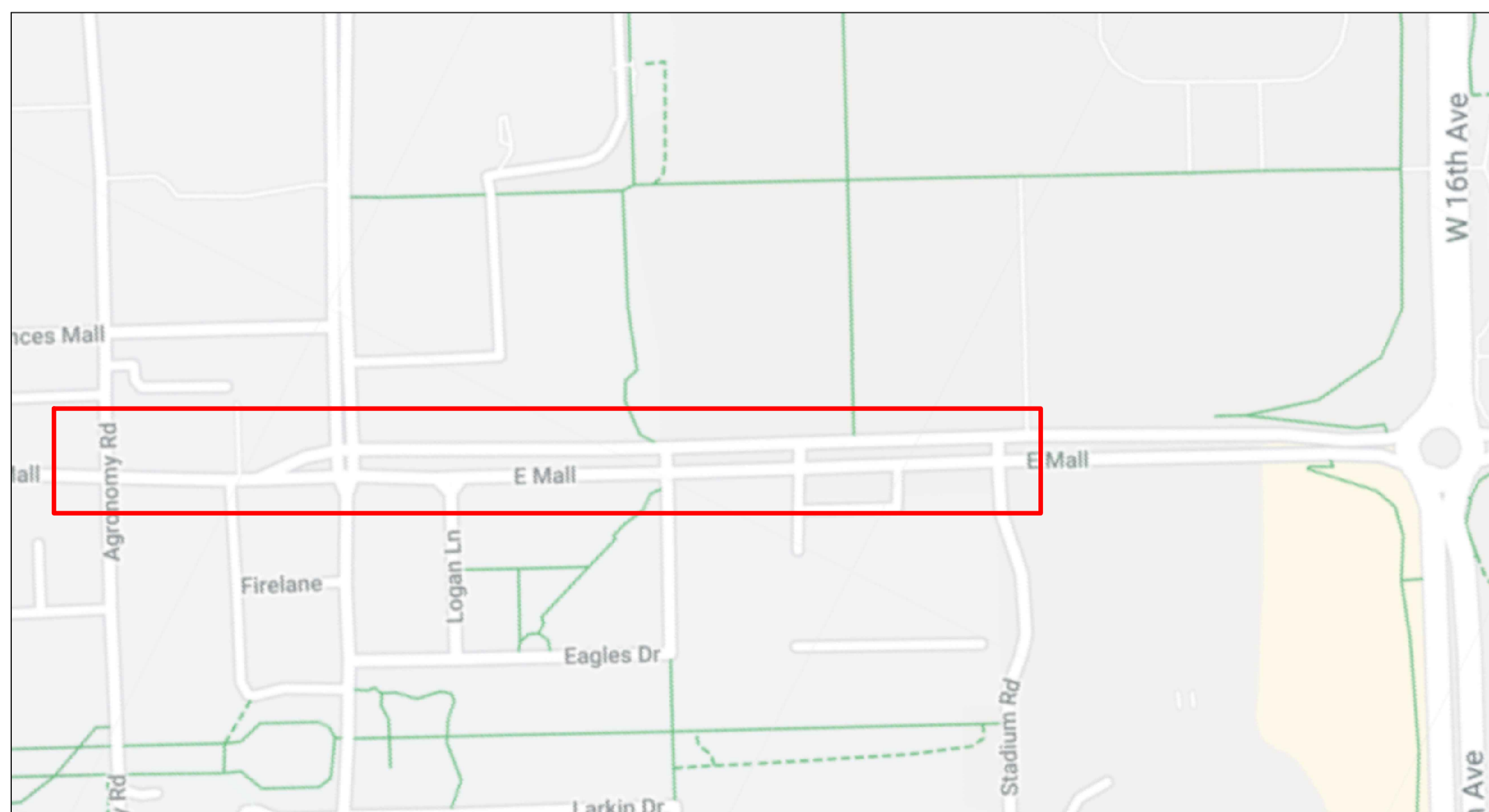
University of New Hampshire Stormwater Center, “*UNHSC Design Specifications for Porous Asphalt Pavement and Infiltration Beds*” [https://www.unh.edu/unhsc/sites/unh.edu.unhsc/files/pubs\\_specs\\_info/unhsc\\_pa\\_spec\\_10\\_09.pdf](https://www.unh.edu/unhsc/sites/unh.edu.unhsc/files/pubs_specs_info/unhsc_pa_spec_10_09.pdf)

# APPENDIX A – ISSUED FOR CONSTRUCTION DRAWINGS

# EAST MALL RECONFIGURATION

UBC ENDOWMENT LANDS  
VANCOUVER BC

## ISSUED FOR CONSTRUCTION



### DRAWING INDEX:

#### GENERAL:

- G101 Existing Site Overview
- G102 Notes

#### TRANSPORTATION:

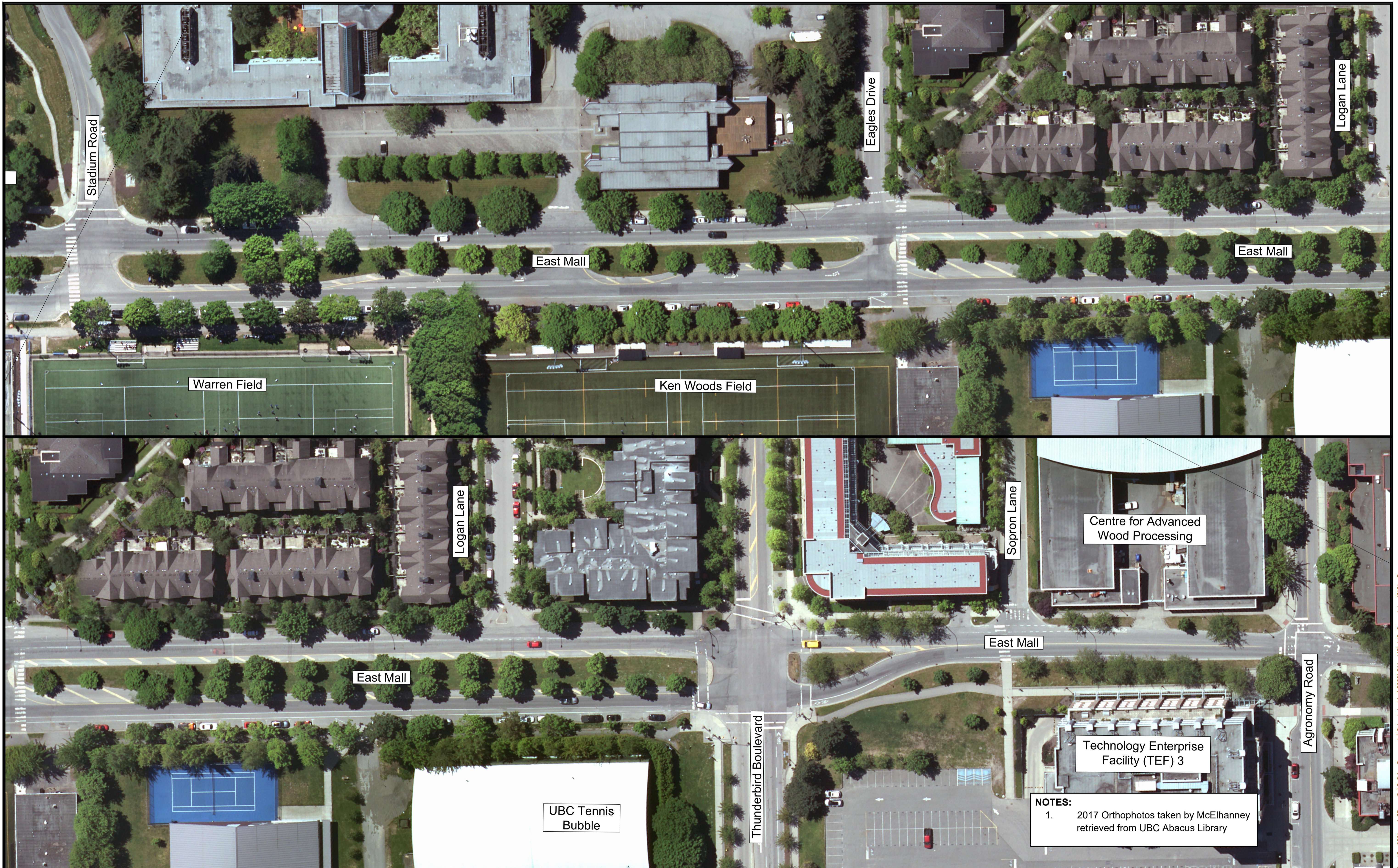
- R101 Roadway Plan View (Sheet 1 of 3)
- R102 Roadway Plan View (Sheet 2 of 3)
- R103 Roadway Plan View (Sheet 3 of 3)
- R104 Roadway Cross-Section (Sheet 1 of 3)
- R105 Roadway Cross-Section (Sheet 2 of 3)
- R106 Roadway Cross-Section (Sheet 3 of 3)
- R107 Roadway Profile
- R108 Roadway Details
- R109 Signage Plan (Sheet 1 of 2)
- R110 Signage Plan (Sheet 2 of 2)

#### STRUCTURAL:

- C101 Canopy Plan View
- C102 Canopy Typical Cross-Section
- C103 Canopy Connection Details (Sheet 1 of 2)
- C104 Canopy Connection Details (Sheet 2 of 2)

#### UTILITIES:

- W101 Utilities Plan - Water
- S101 Utilities Plan - Sanitary
- D101 Utilities Plan - Stormwater
- D102 Stormwater Details
- U101 Utilities Cross-Sections (Sheet 1 of 2)
- U102 Utilities Cross-Sections (Sheet 2 of 2)



**NOTES:**  
 1. 2017 Orthophotos taken by McElhanney retrieved from UBC Abacus Library

REV.	DATE	DESCRIPTION	BY
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4			
3			
2			
1	2021/04/16	EXISTING SITE OVERVIEW	RH

"BY SEALING AND SIGNING THIS DRAWING, I CERTIFY THAT THE INFORMATION CONTAINED IN THESE DRAWINGS ACCURATELY REFLECTS THE ORIGINAL DESIGN, ADDENDA, CHANGE ORDERS AND MATERIAL DESIGN CHANGES MADE DURING CONSTRUCTION AND FIELD REVIEWED BY ME, OR MY REPRESENTATIVE, AND THAT THE AS-CONSTRUCTED WORKS SUBSTANTIALLY COMPLY WITH THE ORIGINAL DESIGN INTENT. HOWEVER, I DO NOT ACCEPT RESPONSIBILITY FOR THE ACCURACY OR COMPLETENESS OF THE AS-CONSTRUCTED INFORMATION SUPPLIED BY OTHERS CONTAINED IN THESE DRAWINGS."

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**EAST MALL REDESIGN**  
 Existing Site Overview

SCALE:	DATE (YYYY.MM.DD)
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DESIGNED	DWG. NO.
RH	G101
DRAWN	REV.
RH	1
REVIEWED	
TM	



Stadium Road

East Mall

REDESIGNED MEDIAN  
419m TOTAL LENGTH

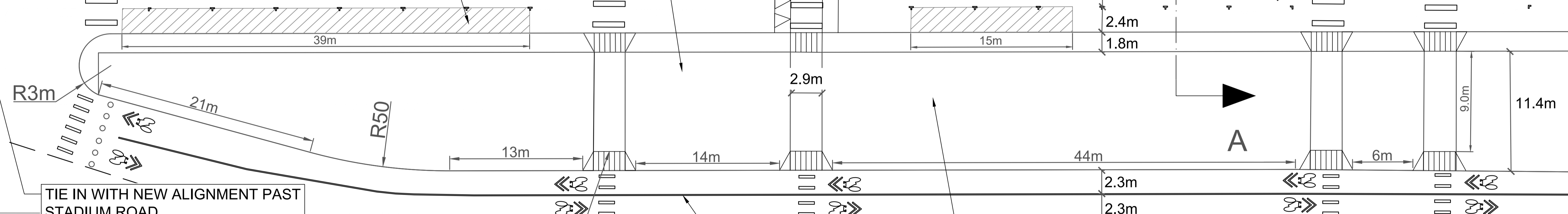
RAISED  
CROSSWALK  
DETAIL

SHOULDER PARKING LANES  
2.4m WIDE AT EVERY 6m

DEDICATED PICK-UP DROP OFF ZONE  
WITH NO PARKING AT ANY TIME

A

A



TIE IN WITH NEW ALIGNMENT PAST  
STADIUM ROAD

BI-DIRECTIONAL CYCLIST  
LANE 4.6m TOTAL WIDTH

MEDIAN  
CURB RAMP

DEDICATED GREEN SPACE

- NOTES:
1. ALL DIMENSIONS ARE IN METRES UNLESS STATED OTHERWISE
  2. FOR ROADWAY CROSS-SECTIONS, REFER TO DRAWINGS R104-105
  3. FOR ROADWAY PROFILES, REFER TO DRAWINGS R106-107
  4. FOR TYPICAL MEDIAN CURB RAMP AND RAISED CROSSWALK DETAILS, REFER TO DRAWING R-108
  5. EXISTING SIDEWALKS DENOTED BY DASHED LINE, TO BE LEFT AS IS UNLESS STATED OTHERWISE

LEGAL DESCRIPTION			
SURVEY BENCHMARK			
REV.	DATE	DESCRIPTION	BY
5			
4			
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2			
1	04/16/2021	Roadway Plan View (Sheet 1 of 3)	KT

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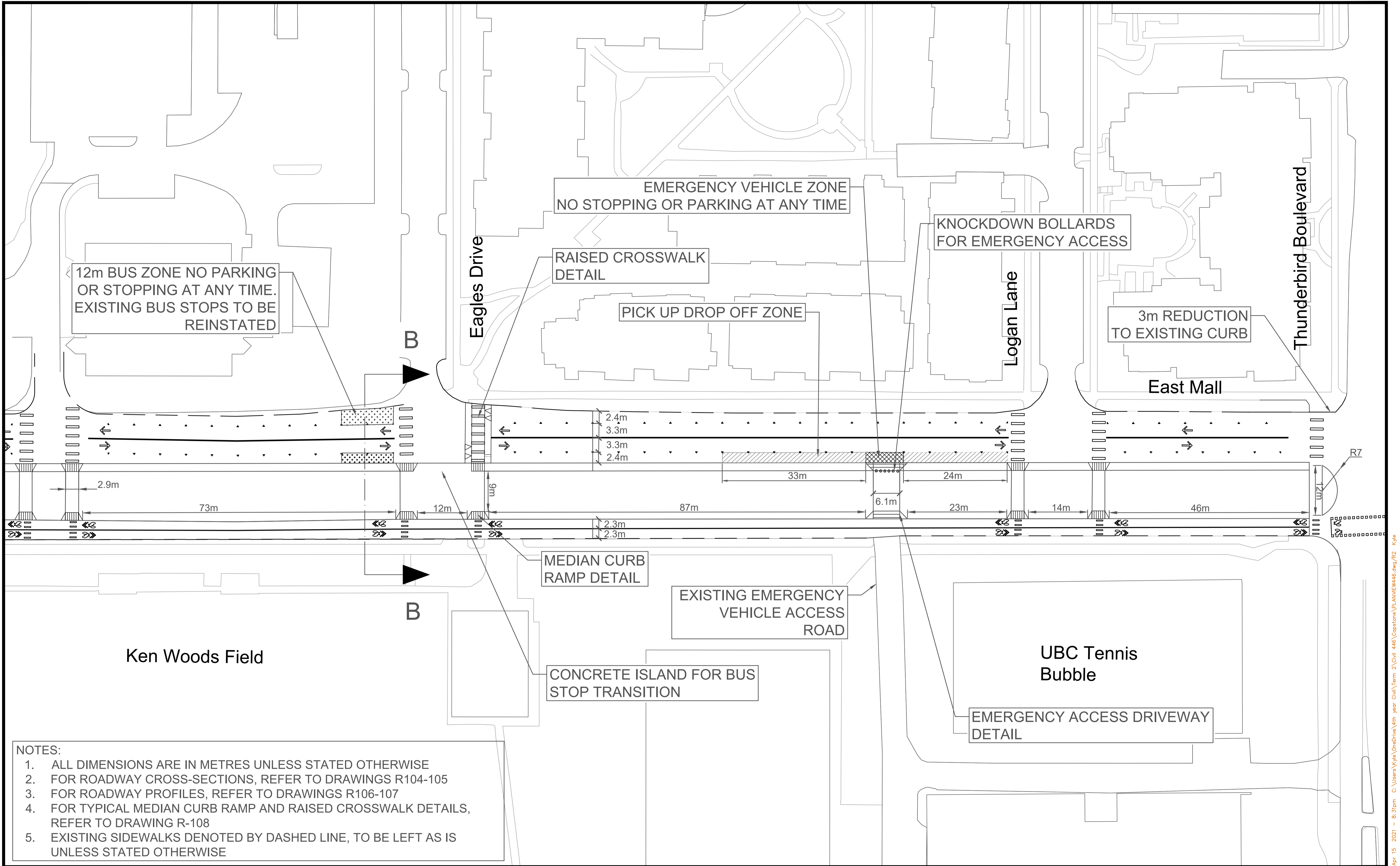


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**EAST MALL REDESIGN**  
Roadway Plan View Drawings (Sheet 1 of 3)

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REVIEWED TM		REV. 1

Ken



12m BUS ZONE NO PARKING OR STOPPING AT ANY TIME. EXISTING BUS STOPS TO BE REINSTATED

EMERGENCY VEHICLE ZONE NO STOPPING OR PARKING AT ANY TIME

RAISED CROSSWALK DETAIL

PICK UP DROP OFF ZONE

KNOCKDOWN BOLLARDS FOR EMERGENCY ACCESS

3m REDUCTION TO EXISTING CURB

MEDIAN CURB RAMP DETAIL

EXISTING EMERGENCY VEHICLE ACCESS ROAD

CONCRETE ISLAND FOR BUS STOP TRANSITION

EMERGENCY ACCESS DRIVEWAY DETAIL

- NOTES:
1. ALL DIMENSIONS ARE IN METRES UNLESS STATED OTHERWISE
  2. FOR ROADWAY CROSS-SECTIONS, REFER TO DRAWINGS R104-105
  3. FOR ROADWAY PROFILES, REFER TO DRAWINGS R106-107
  4. FOR TYPICAL MEDIAN CURB RAMP AND RAISED CROSSWALK DETAILS, REFER TO DRAWING R-108
  5. EXISTING SIDEWALKS DENOTED BY DASHED LINE, TO BE LEFT AS IS UNLESS STATED OTHERWISE

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1	04/16/2021	Roadway Plan View (Sheet 2 of 3)	KT

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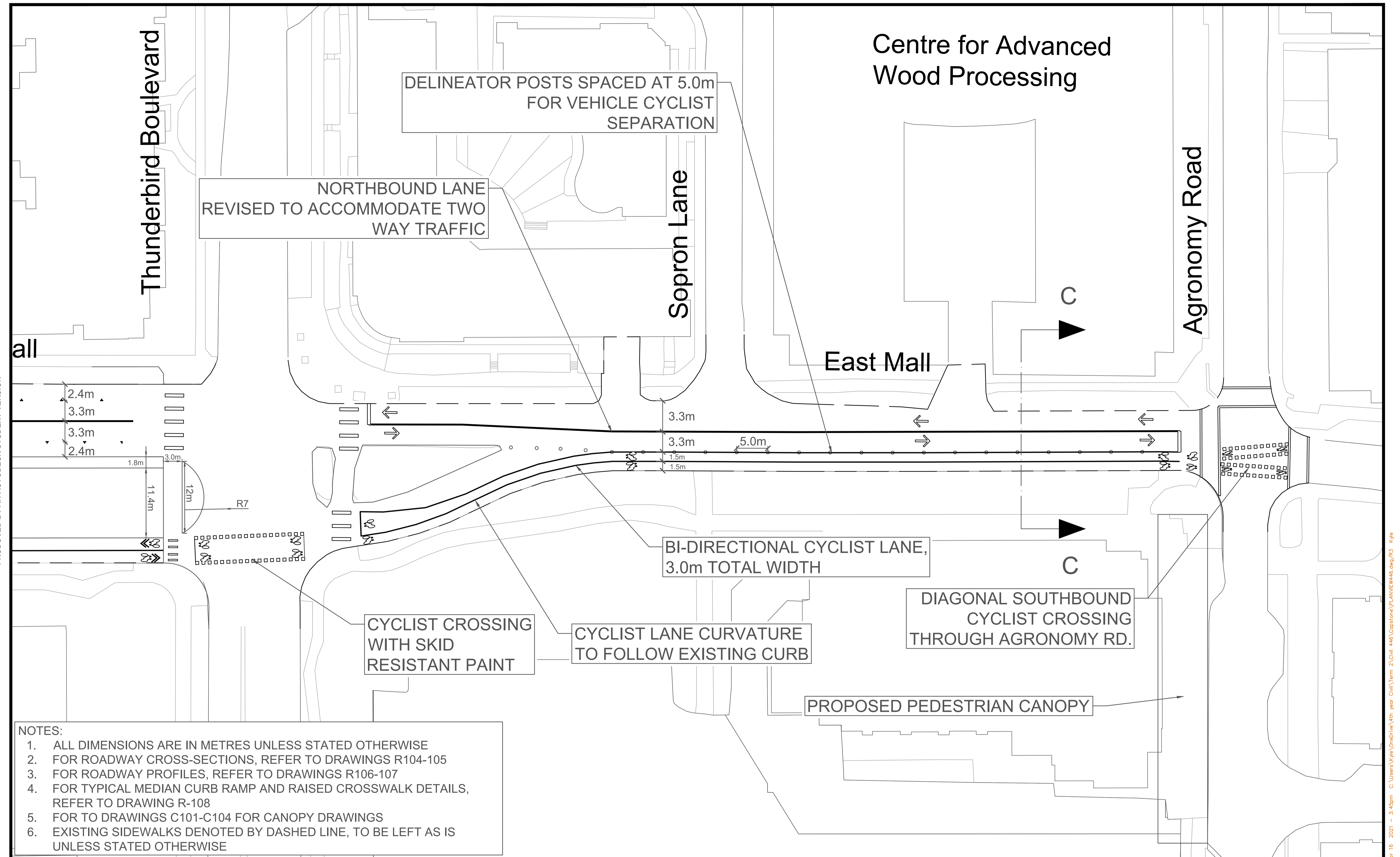


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**EAST MALL REDESIGN**  
 Roadway Plan View (Sheet 2 of 3)

SCALE: 1:400	DATE (YYYY.MM.DD) 04/16/2021
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DRAWN KT	R102
REVIEWED TM	REV. 1





PRODUCED BY AN AUTODESK STUDENT VERSION

PRODUCED BY AN AUTODESK STUDENT VERSION

- NOTES:**
1. ALL DIMENSIONS ARE IN METRES UNLESS STATED OTHERWISE
  2. FOR ROADWAY CROSS-SECTIONS, REFER TO DRAWINGS R104-105
  3. FOR ROADWAY PROFILES, REFER TO DRAWINGS R106-107
  4. FOR TYPICAL MEDIAN CURB RAMP AND RAISED CROSSWALK DETAILS, REFER TO DRAWING R-108
  5. FOR TO DRAWINGS C101-C104 FOR CANOPY DRAWINGS
  6. EXISTING SIDEWALKS DENOTED BY DASHED LINE, TO BE LEFT AS IS UNLESS STATED OTHERWISE

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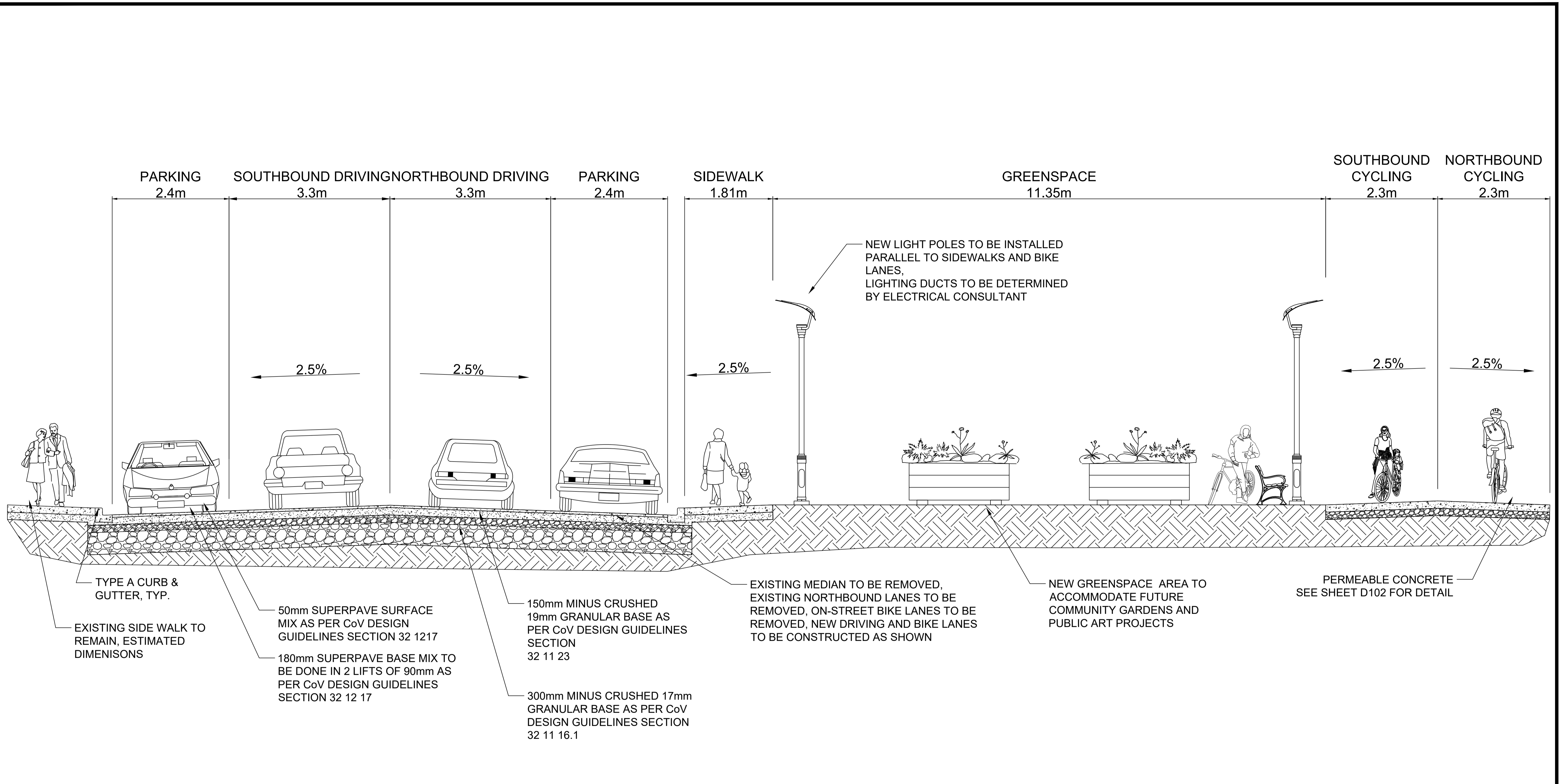


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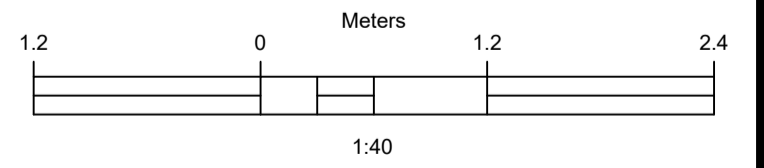
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**TYPICAL  
CROSS-SECTION A**



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2	2021/03/04	Updated Design Cross-Sections	RH
1	2020/12/03	Preliminary Design Cross-Sections	RH

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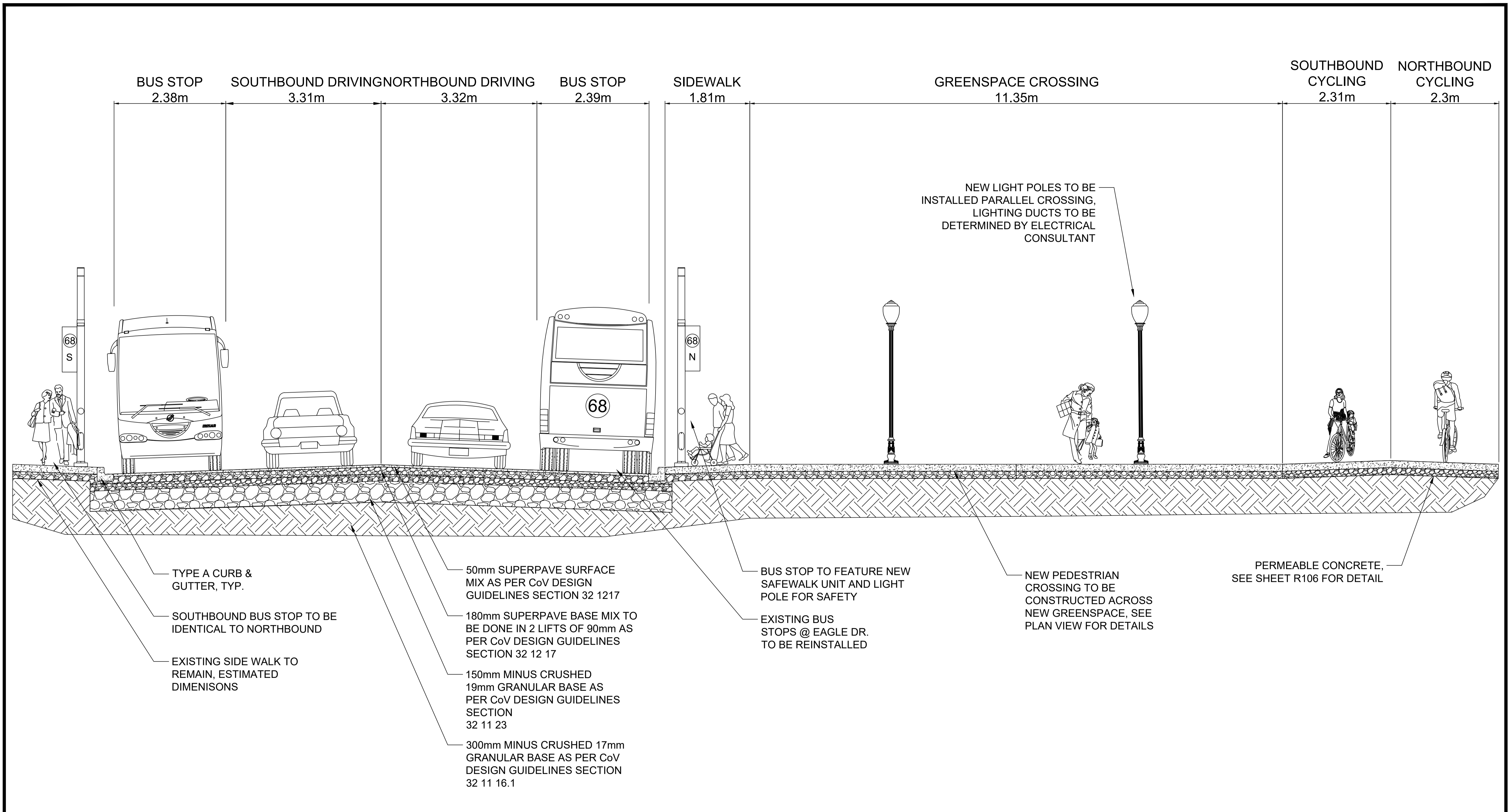
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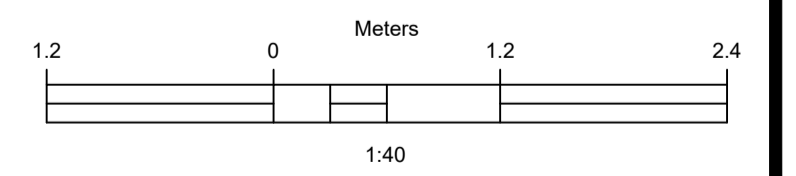
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 Roadway Cross-Sections (Sheet 1 of 3)

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REVIEWED TM	REV. 3

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## BUS STOP AND GREENWAY CROSSING CROSS-SECTION B



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4			
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2	2021/03/04	Updated Design Cross-Sections	RH
1	2020/12/03	Preliminary Design Cross-Sections	RH

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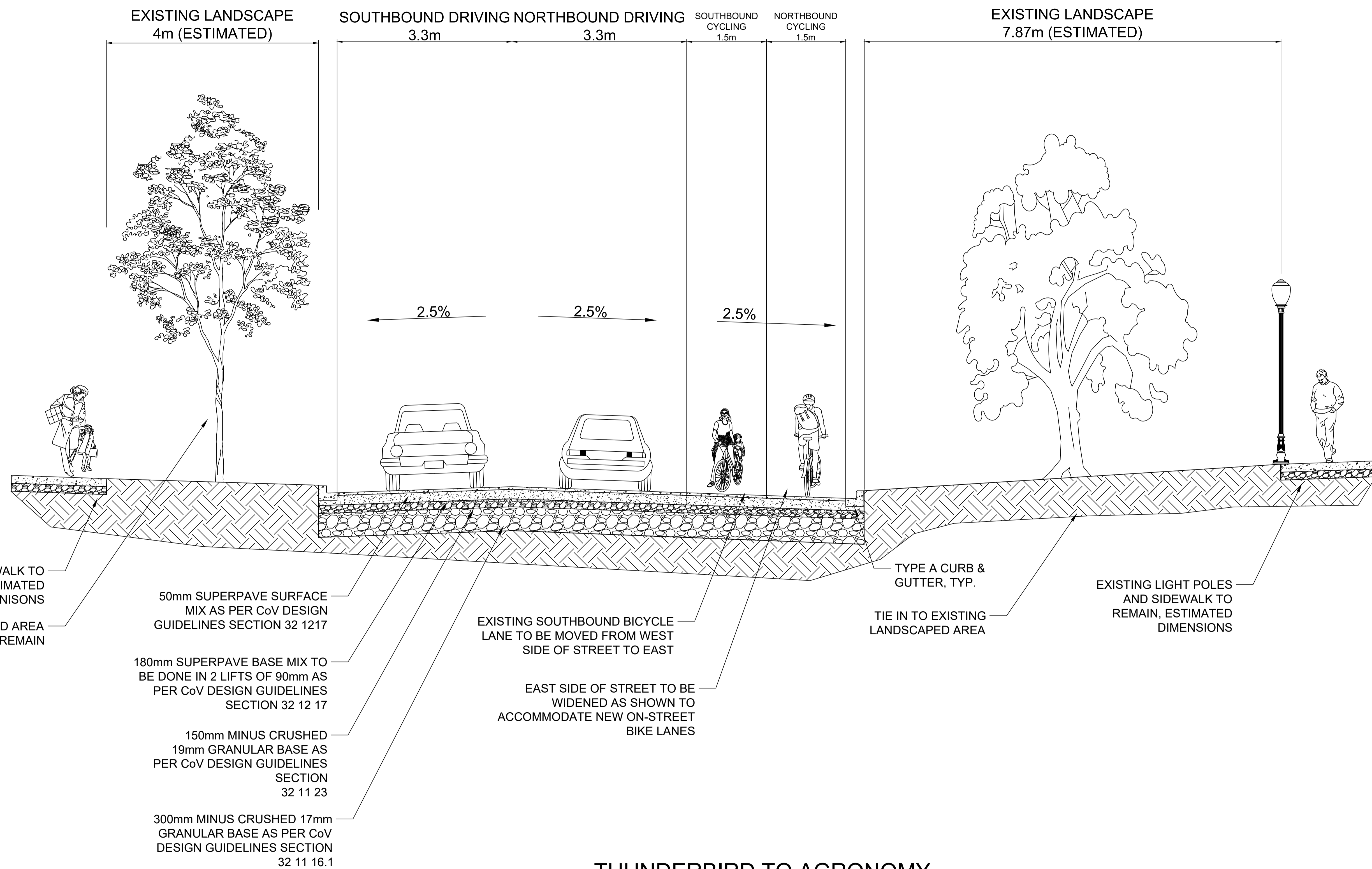


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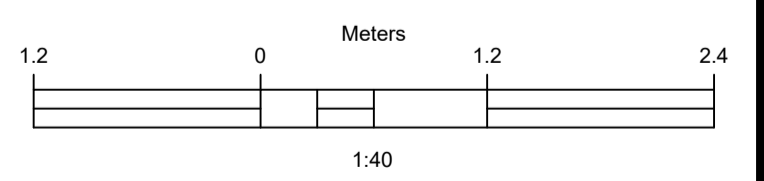
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	DRAWN RH	REV. <b>3</b>
	REVIEWED TM	

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**THUNDERBIRD TO AGRONOMY  
CROSS-SECTION C**



REV.	DATE	DESCRIPTION	BY
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4			
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2	2021/03/04	Updated Design Cross-Sections	RH
1	2020/12/03	Preliminary Design Cross-Sections	RH

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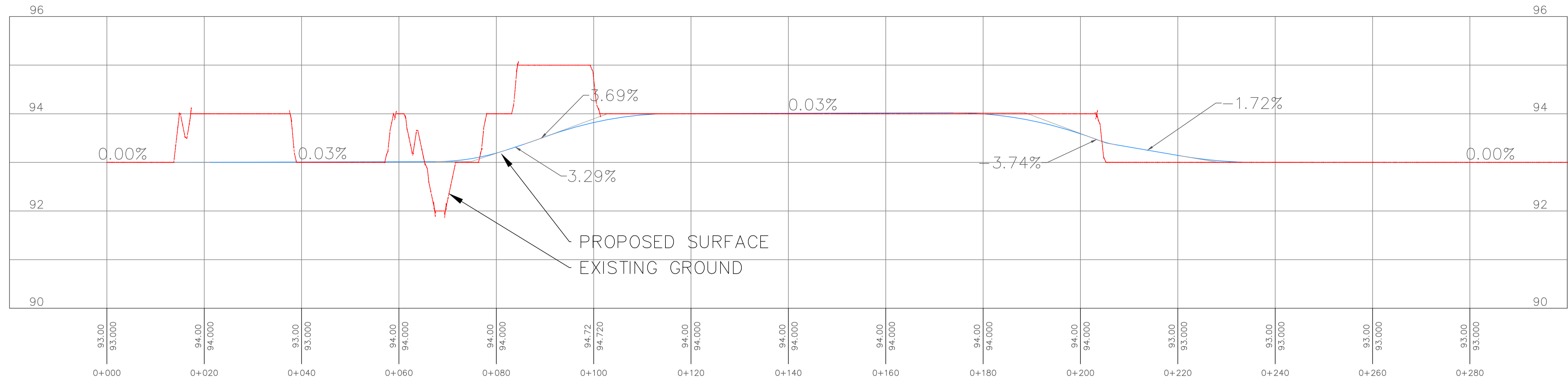


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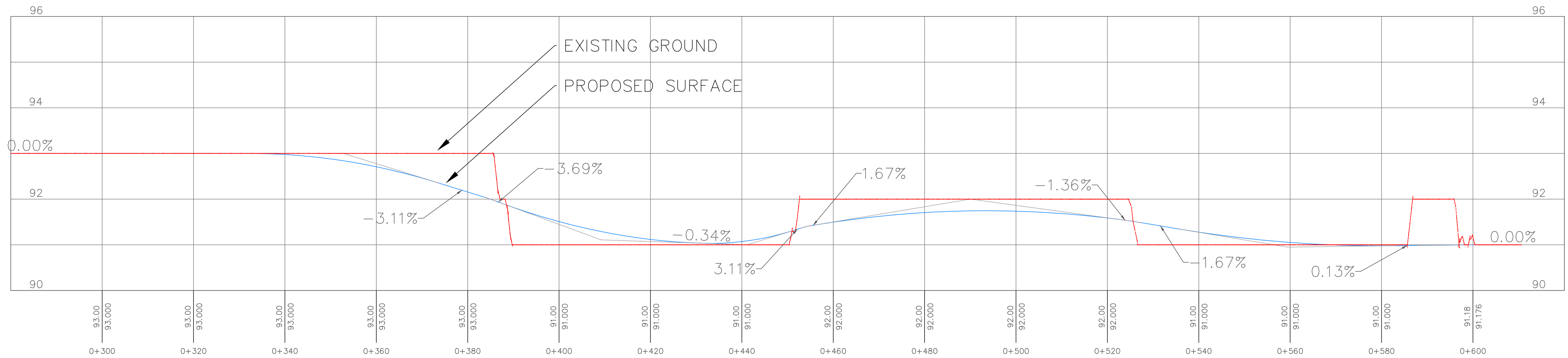
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Roadway Cross-Sections (Sheet 3 of 3)

SCALE:	DATE (YYYY.MM.DD)
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DESIGNED RH	DWG. NO.
DRAWN RH	R106
REVIEWED TM	REV. 3

PROPOSED ALIGNMENT PROFILE  
STA. 0+000m TO STA. 0+300m



PROPOSED ALIGNMENT PROFILE  
STA. 0+300m TO STA. 0+620m



LEGAL DESCRIPTION			
SURVEY BENCHMARK			
REV.	DATE	DESCRIPTION	BY
5			
4			
3			
2			
1	2021/04/16	ROADWAY PROFILE	RH

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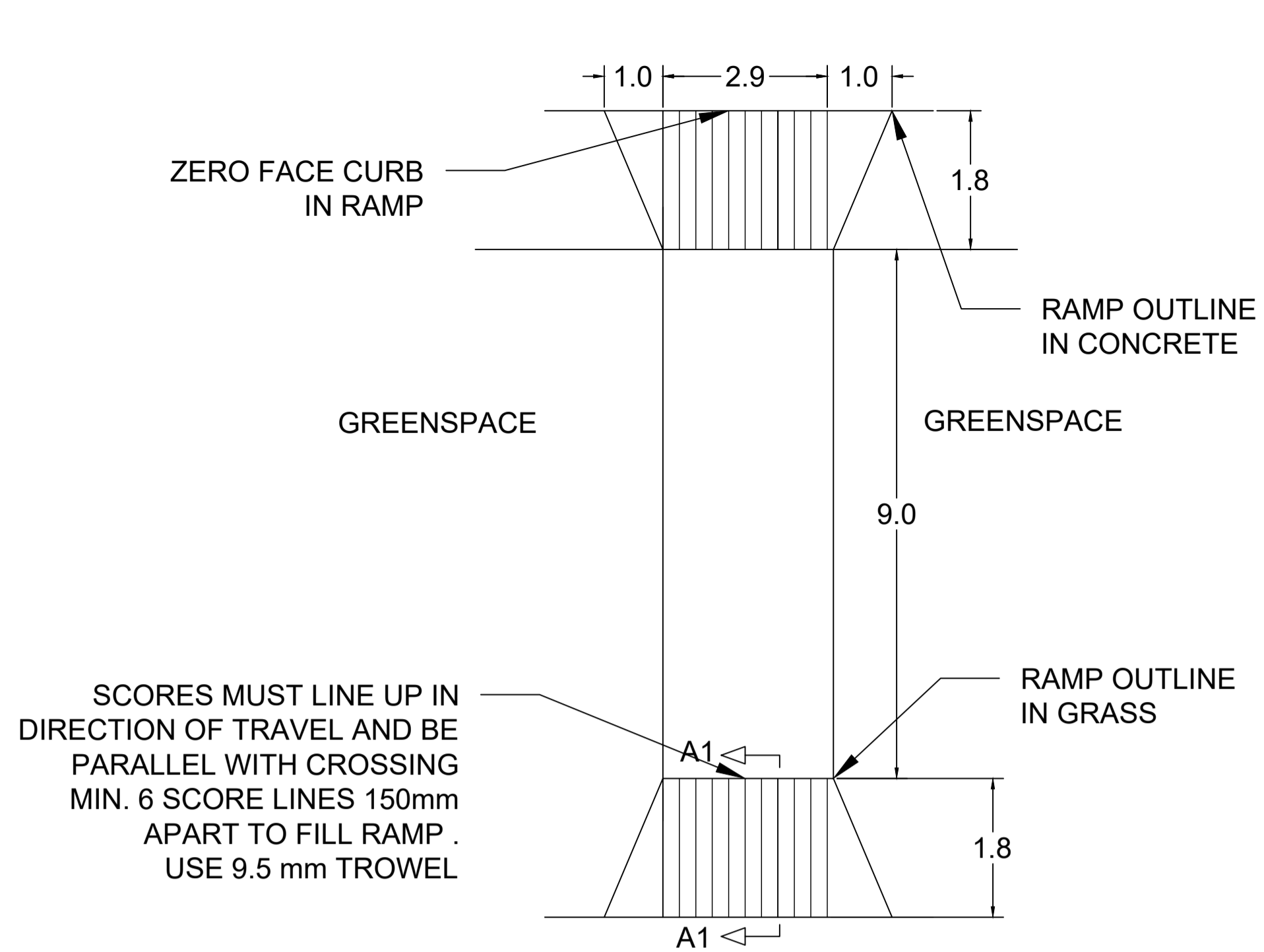
CONSULTANT



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Vancouver, BC V6T 1Z4

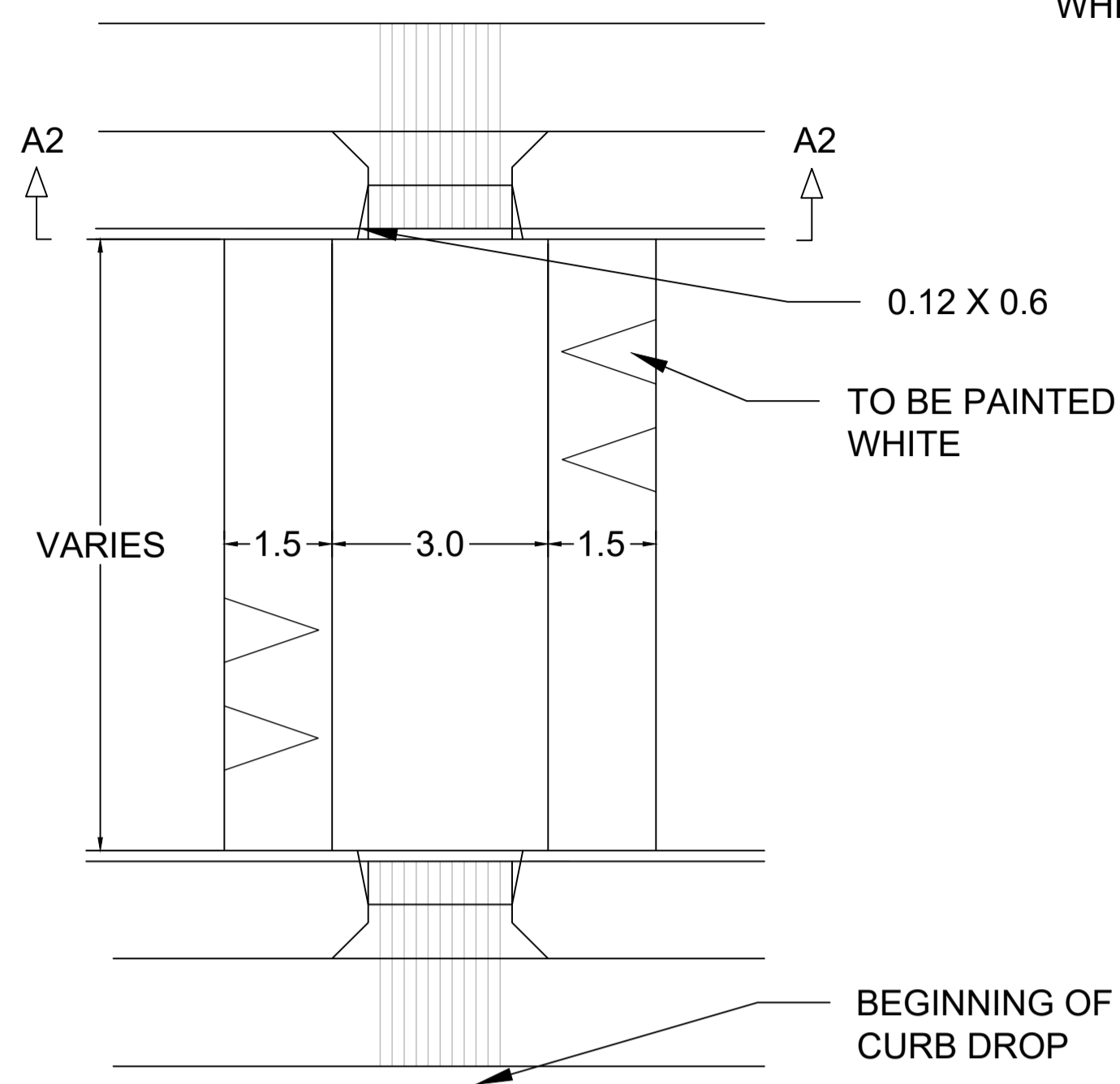
**EAST MALL REDESIGN**  
Roadway Profile

SEAL	SCALE: N.T.S.	DATE (YYYY.MM.DD) 2021/04/16
	DESIGNED TM	DWG. NO. R107
	DRAWN TM	REV. 1
	REVIEWED BM	



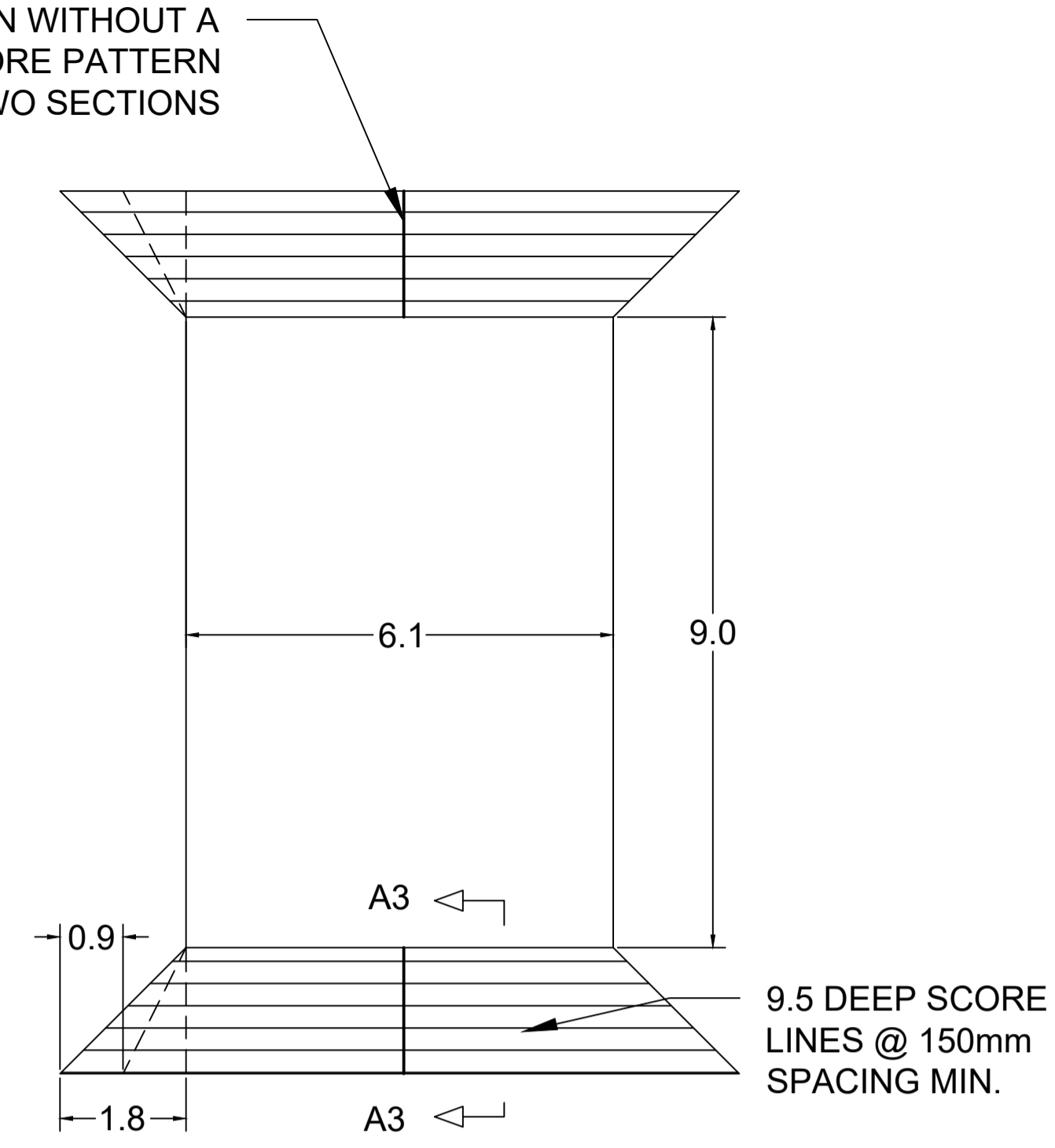
DETAIL 1: MEDIAN CURB RAMPS

SCORES MUST LINE UP IN DIRECTION OF TRAVEL AND BE PARALLEL WITH CROSSING MIN. 6 SCORE LINES 150mm APART TO FILL RAMP. USE 9.5 mm TROWEL

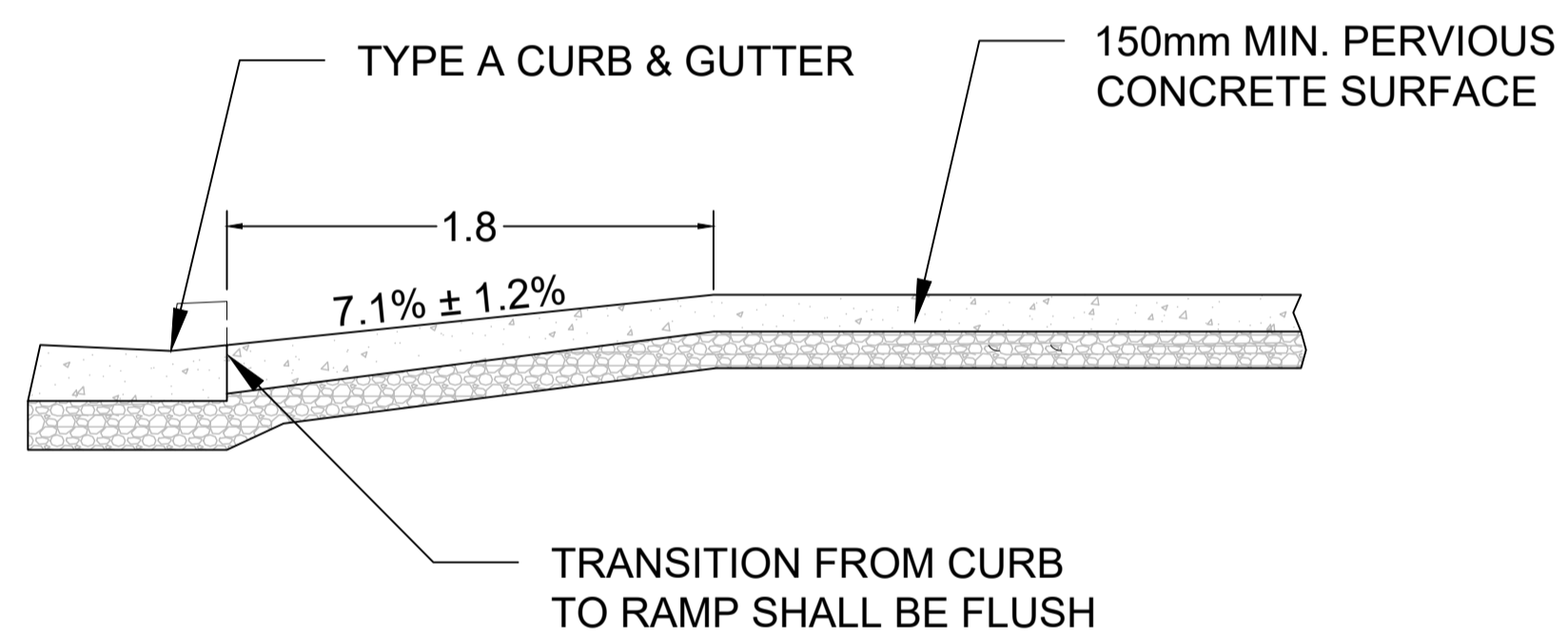


DETAIL 2: RAISED CROSSWALK

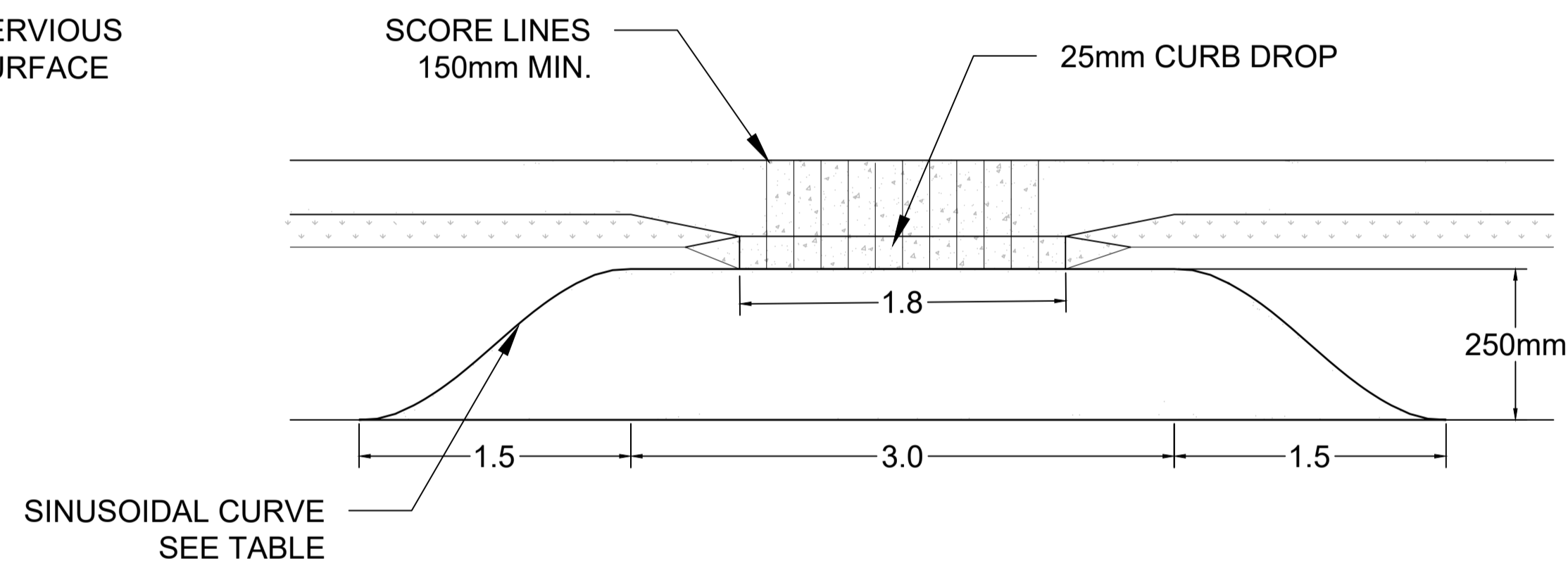
INSTALL CONTROL JOIN WITHOUT A TROWELED EDGE AND ALIGN SCORE PATTERN WHEN CROSSING IS POURED AS TWO SECTIONS



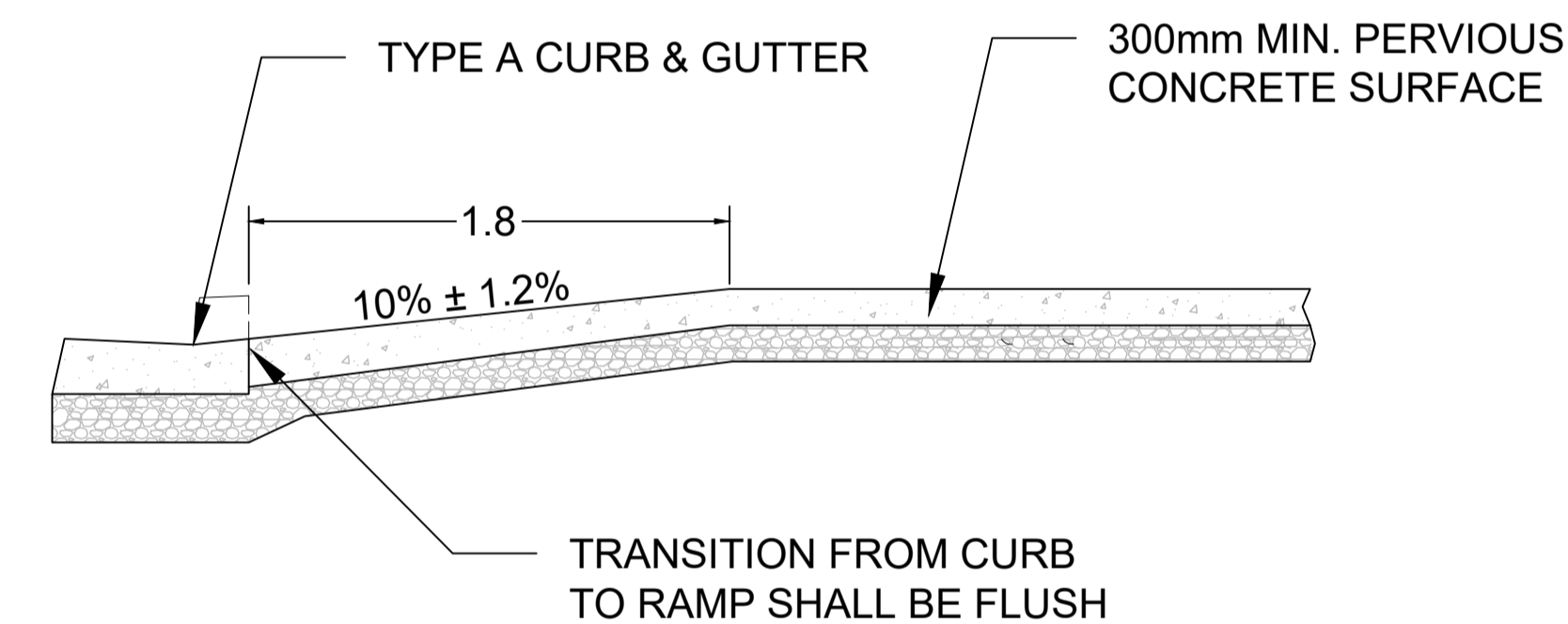
DETAIL C: EMERGENCY ACCESS DRIVEWAY CROSSING



SECTION A1-A1  
MEDIAN CURB RAMP



SECTION A2-A2  
RAISED CROSSWALK



SECTION A3-A3  
EMERGENCY ACCESS DRIVEWAY CROSSING

SINUSOIDAL SPEED DEVELOPMENT HUMP

DISTANCE (m)	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1	1.2	1.3	1.4	1.5
FINISHED HEIGHT (mm)	1	5	12	21	31	43	56	69	82	94	104	113	120	124	125

NOTES:

1. ALL DIMENSIONS ARE IN METERS UNLESS STATED OTHERWISE
2. REFER TO DRAWING R101-103 FOR GENERAL PLAN VIEW
3. REFER TO DRAWING D102 FOR DETAILED SUBGRADE MATERIAL
4. REFER TO CoV CONSTRUCTION SPECIFICATIONS FOR FULL DETAILS
5. CONTRACTOR TO CONFIRM CROSSING LAYOUT IS APPROVED BY CITY INSPECTORS PRIOR TO POURING

REV.	DATE	DESCRIPTION	BY
5			
4			
3			
2			
1	2021/04/16	Roadway Detail	RH

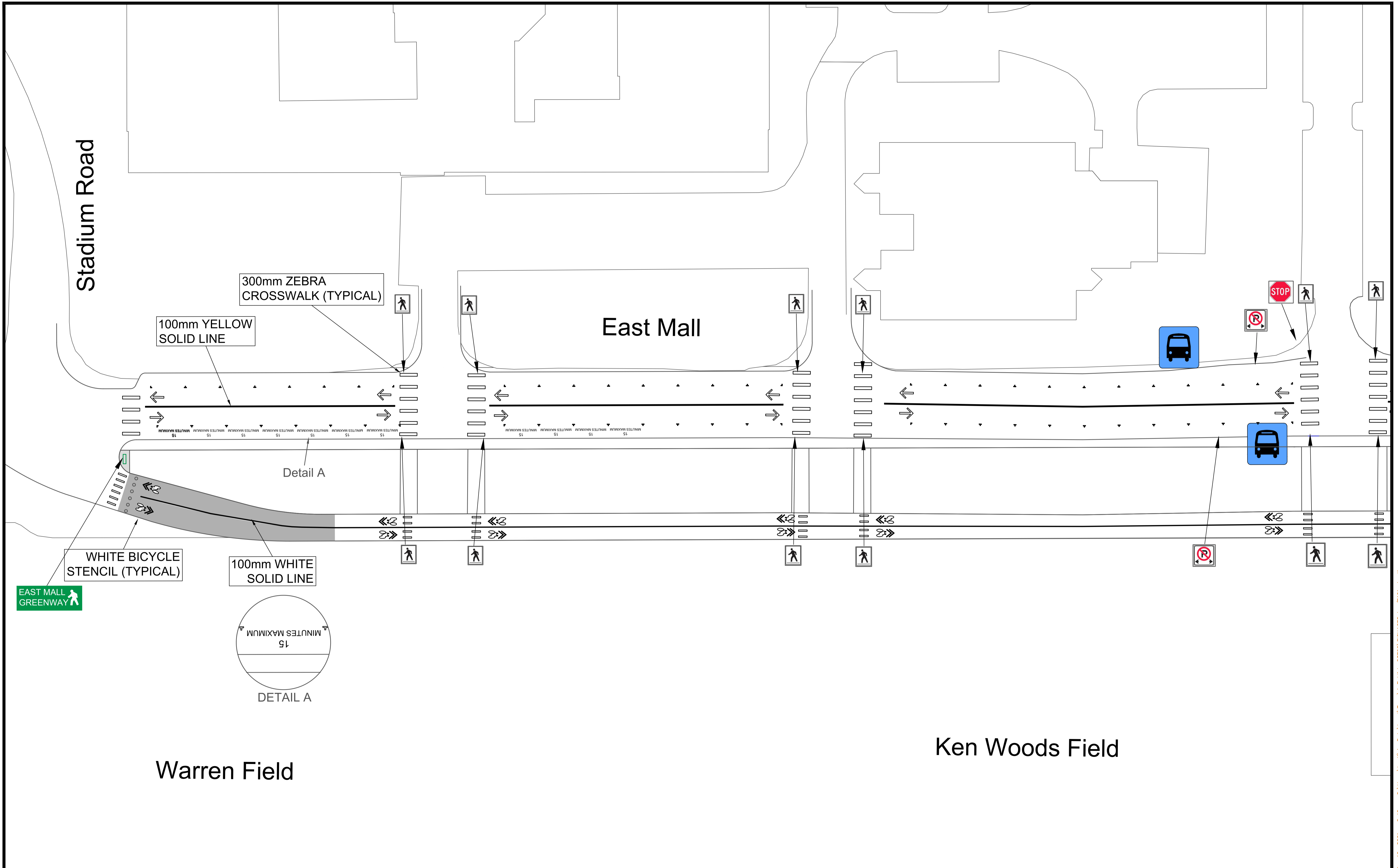
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**EAST MALL REDESIGN**  
 Roadway Details

SCALE: N.T.S.  
 DATE (YYYY.MM.DD)  
 2021/04/16  
 DESIGNED: KT  
 DRAWN: KT  
 REVIEWED: TM  
 DWG. NO.  
**R108**  
 REV. 1



REV	DATE	DESCRIPTION	BY
5			
4			
3			
2			
1	2021/04/16	SIGNAGE PLAN (1 of 2)	BM

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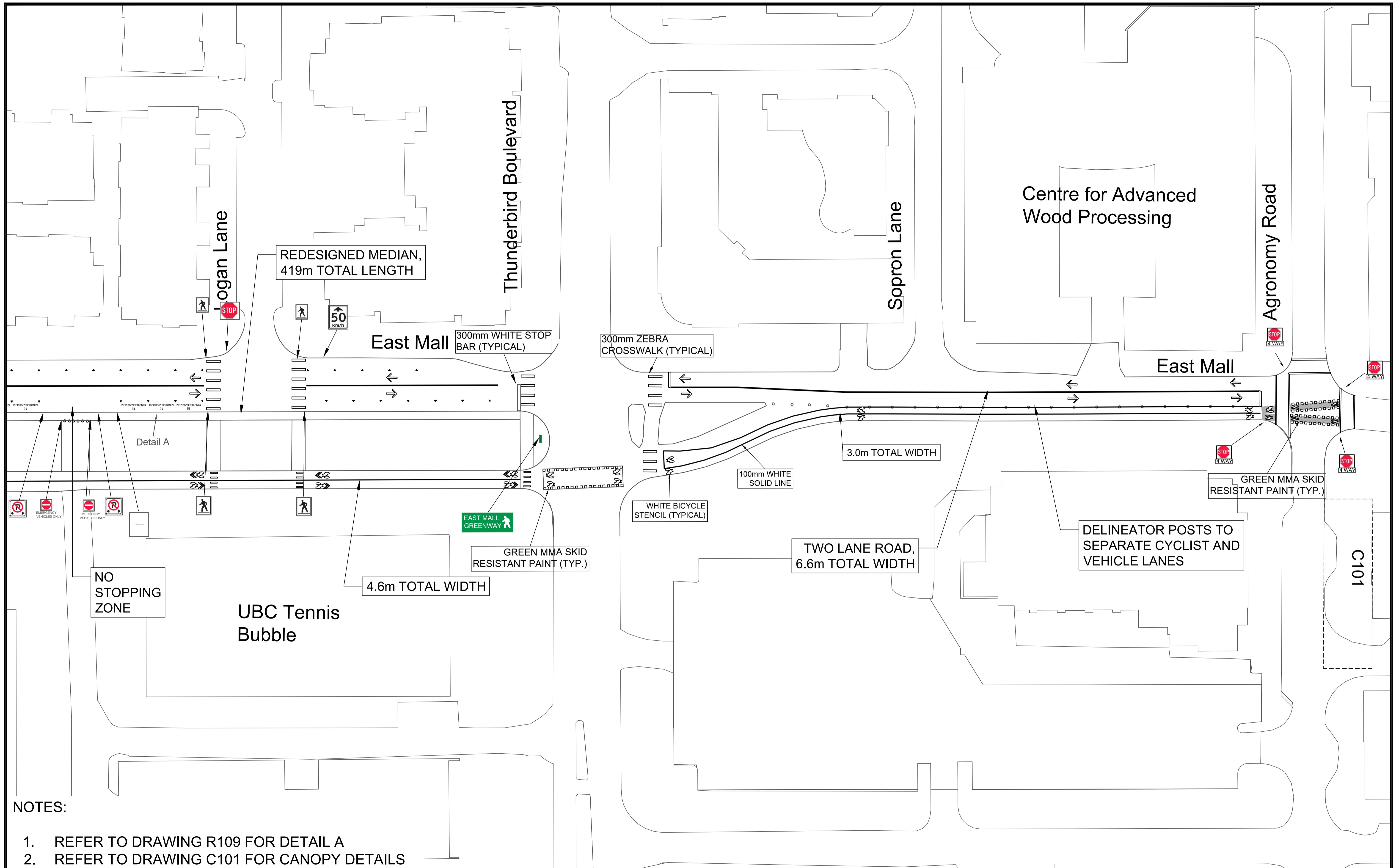
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 Vancouver, BC V6T 1Z4

**EAST MALL REDESIGN**  
 Signage Plan (1 of 2)

SCALE: 1:300	DATE (YYYY.MM.DD) 2021/04/16
DESIGNED: BM	DWG. NO. R109
DRAWN: BM	REV. 1
REVIEWED: KT	



**NOTES:**

1. REFER TO DRAWING R109 FOR DETAIL A
2. REFER TO DRAWING C101 FOR CANOPY DETAILS

REV	DATE	DESCRIPTION	BY
5			
4			
3			
2			
1	2021/04/16	SIGNAGE PLAN (2 of 2)	BM

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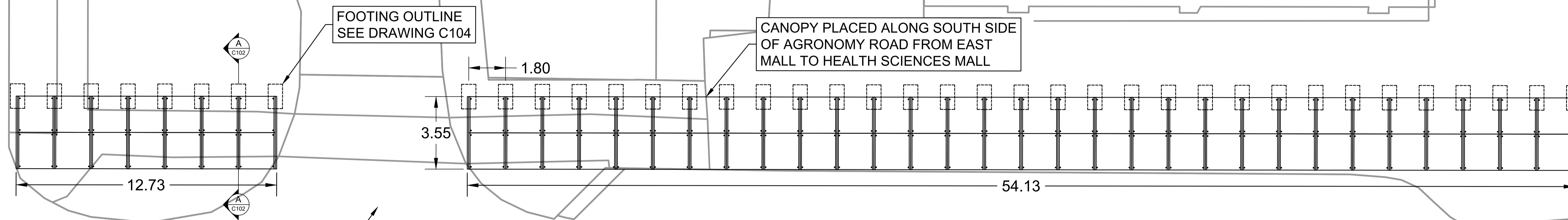
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**EAST MALL REDESIGN**  
 Signage Plan (2 of 2)

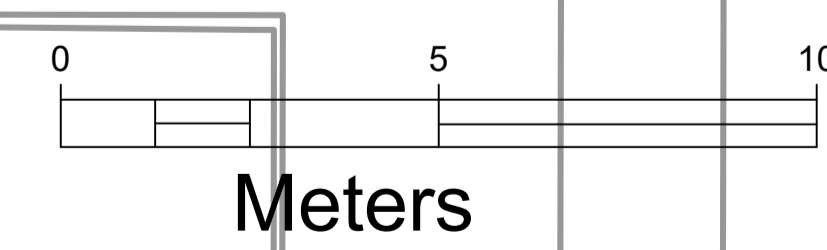
SCALE: 1:300	DATE (YYYY.MM.DD) 2021/04/16
DESIGNED: BM	DWG. NO. R110
DRAWN: BM	REV. 1
REVIEWED: KT	

Apr 16 2021 - 2:40pm C:\Users\boast\AppData\Local\Temp\AcPublish\Temp\AcPublish\_23796\SignageZ.dwg/R102\_boast





# Agronomy Road



REV.	DATE	DESCRIPTION	BY
5			
4			
3			
2			
1	2021/04/16	CANOPY PLAN - FOR CONSTRUCTION	JH

"BY SEALING AND SIGNING THIS DRAWING, I CERTIFY THAT THE INFORMATION CONTAINED IN THESE DRAWINGS ACCURATELY REFLECTS THE ORIGINAL DESIGN, ADDENDA, CHANGE ORDERS AND MATERIAL DESIGN CHANGES MADE DURING CONSTRUCTION AND FIELD REVIEWED BY ME, OR MY REPRESENTATIVE, AND THAT THE AS-CONSTRUCTED WORKS SUBSTANTIALLY COMPLY WITH THE ORIGINAL DESIGN INTENT. HOWEVER, I DO NOT ACCEPT RESPONSIBILITY FOR THE ACCURACY OR COMPLETENESS OF THE AS-CONSTRUCTED INFORMATION SUPPLIED BY OTHERS CONTAINED IN THESE DRAWINGS."

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**EAST MALL REDESIGN**  
 Canopy Plan View

SCALE: 1:100  
 DATE (YYYY.MM.DD) 2021/04/16

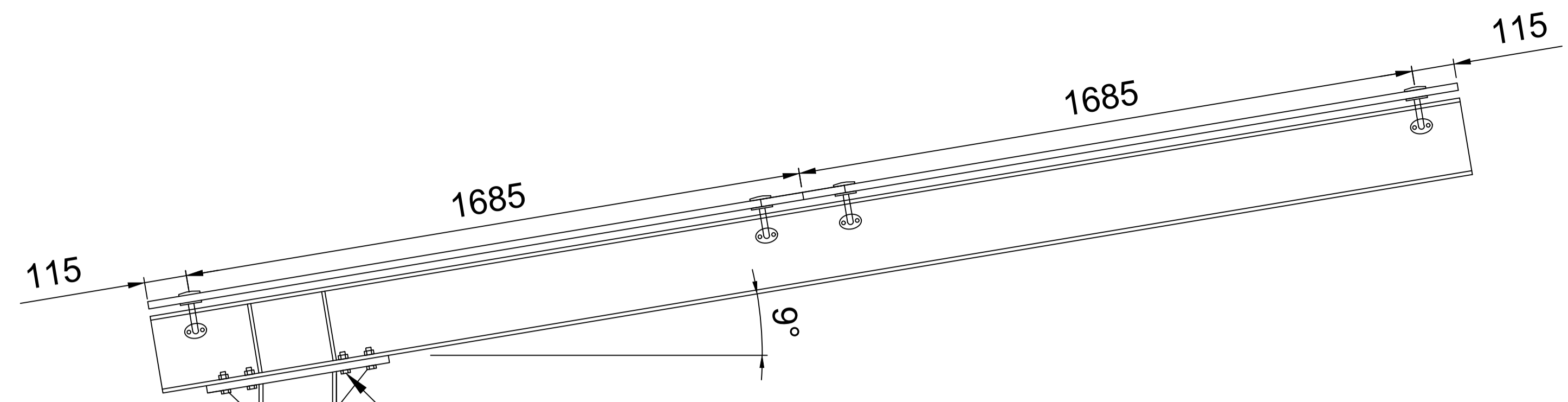
DESIGNED JH  
 DRAWN JH  
 REVIEWED TM

DWG. NO. C101  
 REV. 1

PRODUCED BY AN AUTODESK STUDENT VERSION

PRODUCED BY AN AUTODESK STUDENT VERSION

Apr 16 2021 - 3:47pm C:\Users\8571\Google Drive\UBC-4 Semester 1\CIVL 445 Copstone\Drawings\Detailed Design Drawings\Detailed Copy Drawings.dwg/C101 8571J



SEE DRAWING C103  
FOR CONNECTION DETAIL

1800x1800mm TEMPERED  
GLASS PANEL

GLASS PANEL BREAK  
SEAL WITH RUBBER GASKET

SEE DRAWING C104  
FOR BASE PLATE DETAIL

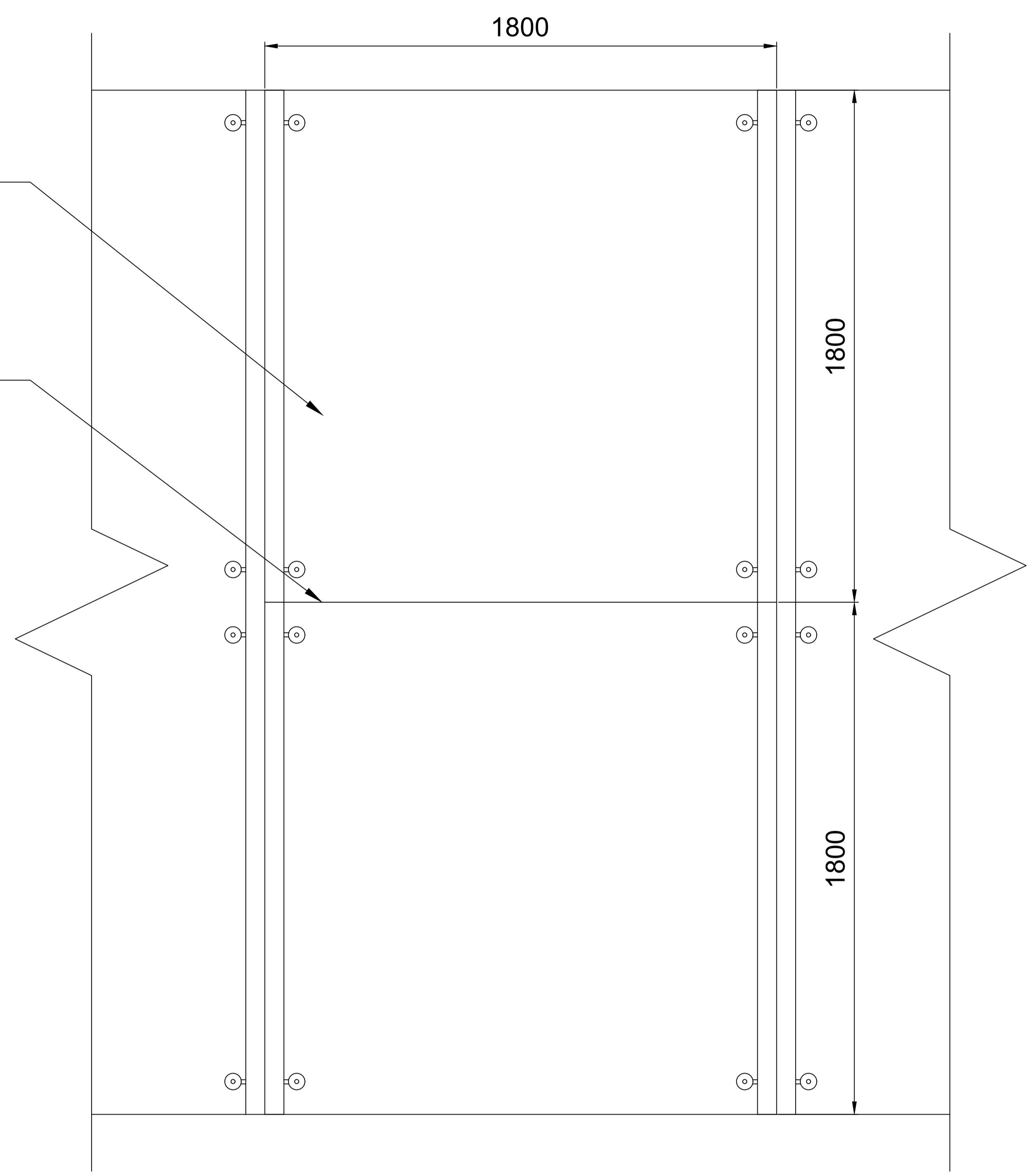
700x700x100mm  
CONCRETE TOPPING  
32MPa CONCRETE

2.8m WIDE SIDEWALK  
32MPa CONCRETE

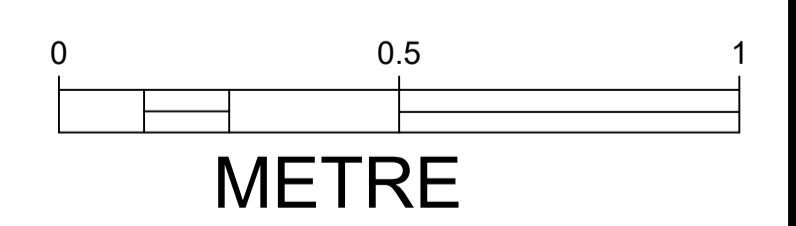
100mm DEPTH MINUS CRUSHED  
GRANULAR BASE 95% MPD

2550

CONCRETE FOUNDATION  
SEE DRAWING C104 FOR DETAILS



**PLAN VIEW TYPICAL  
SECTION**



REV.	DATE	DESCRIPTION	BY
5			
4			
3			
2			
1	2021/04/16	CANOPY TYPICAL CROSS SECTION - FOR CONSTRUCTION	JH

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**EAST MALL REDESIGN**  
CANOPY TYPICAL CROSS-SECTION

SCALE:  
**1:11**

DATE (YYYY.MM.DD)  
**2021/04/16**

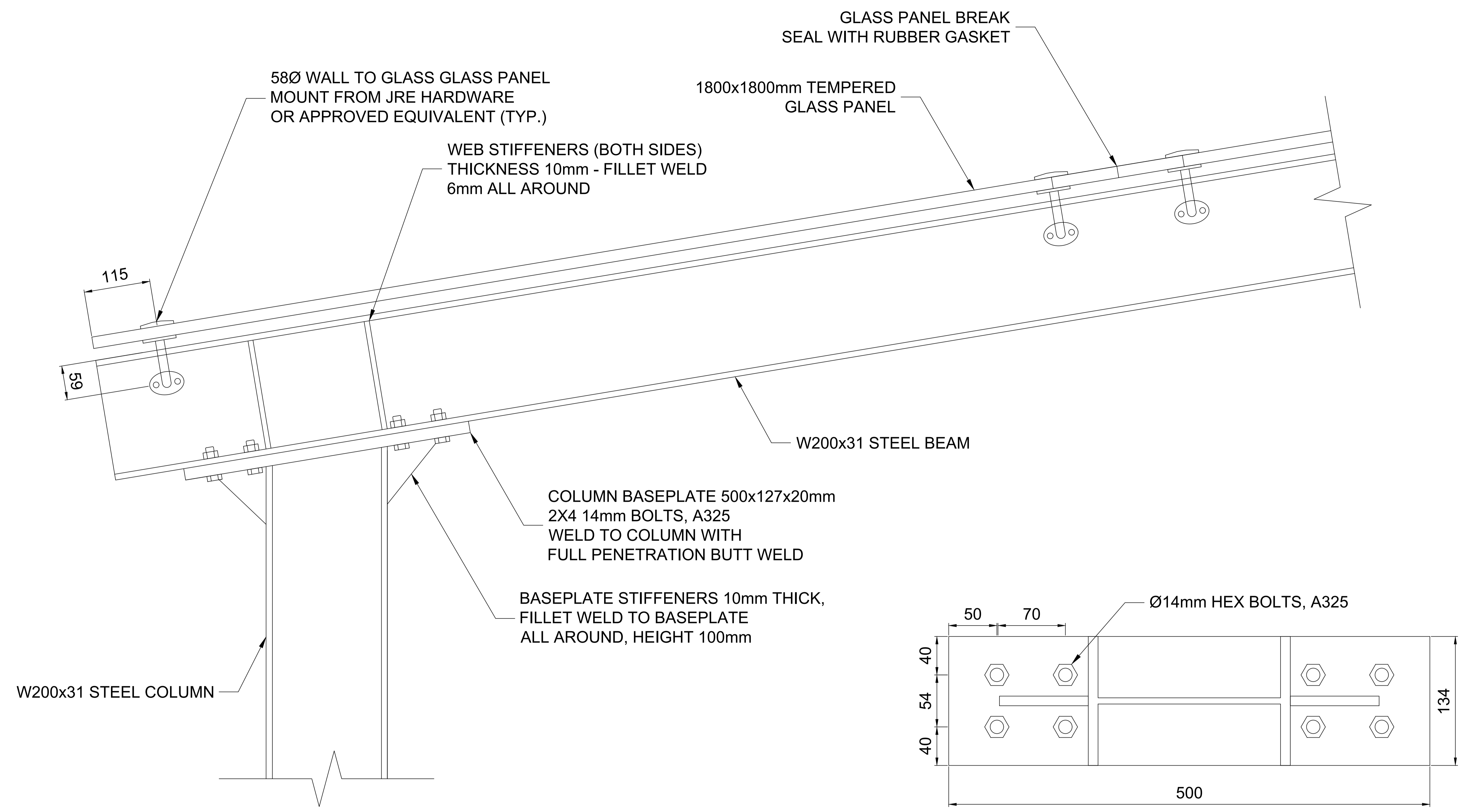
DESIGNED  
JH

DRAWN  
JH

REVIEWED  
DB

DWG. NO.  
**C102**

REV.  
**1**



**COLUMN TO BEAM CONNECTION DETAIL 1:5**

**COLUMN END PLATE DETAIL 1:2**

REV.	DATE	DESCRIPTION	BY
5			
4			
3			
2			
1	2021/04/16	CANOPY COLUMN TO CANTILEVER DETAIL - FOR CONSTRUCTION	JH

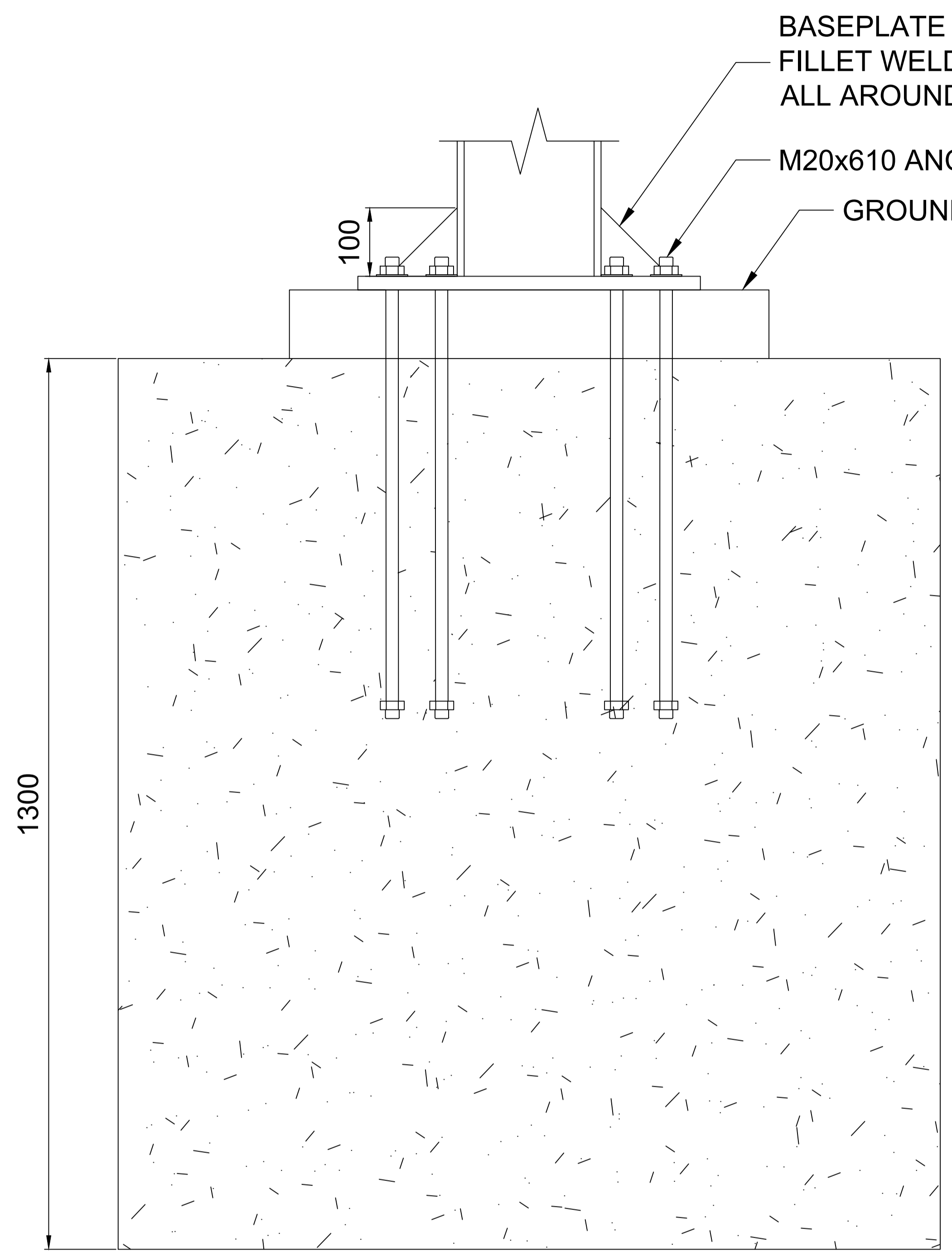
"BY SEALING AND SIGNING THIS DRAWING, I CERTIFY THAT THE INFORMATION CONTAINED IN THESE DRAWINGS ACCURATELY REFLECTS THE ORIGINAL DESIGN, ADDENDA, CHANGE ORDERS AND MATERIAL DESIGN CHANGES MADE DURING CONSTRUCTION AND FIELD REVIEWED BY ME, OR MY REPRESENTATIVE, AND THAT THE AS-CONSTRUCTED WORKS SUBSTANTIALLY COMPLY WITH THE ORIGINAL DESIGN INTENT. HOWEVER, I DO NOT ACCEPT RESPONSIBILITY FOR THE ACCURACY OR COMPLETENESS OF THE AS-CONSTRUCTED INFORMATION SUPPLIED BY OTHERS CONTAINED IN THESE DRAWINGS."

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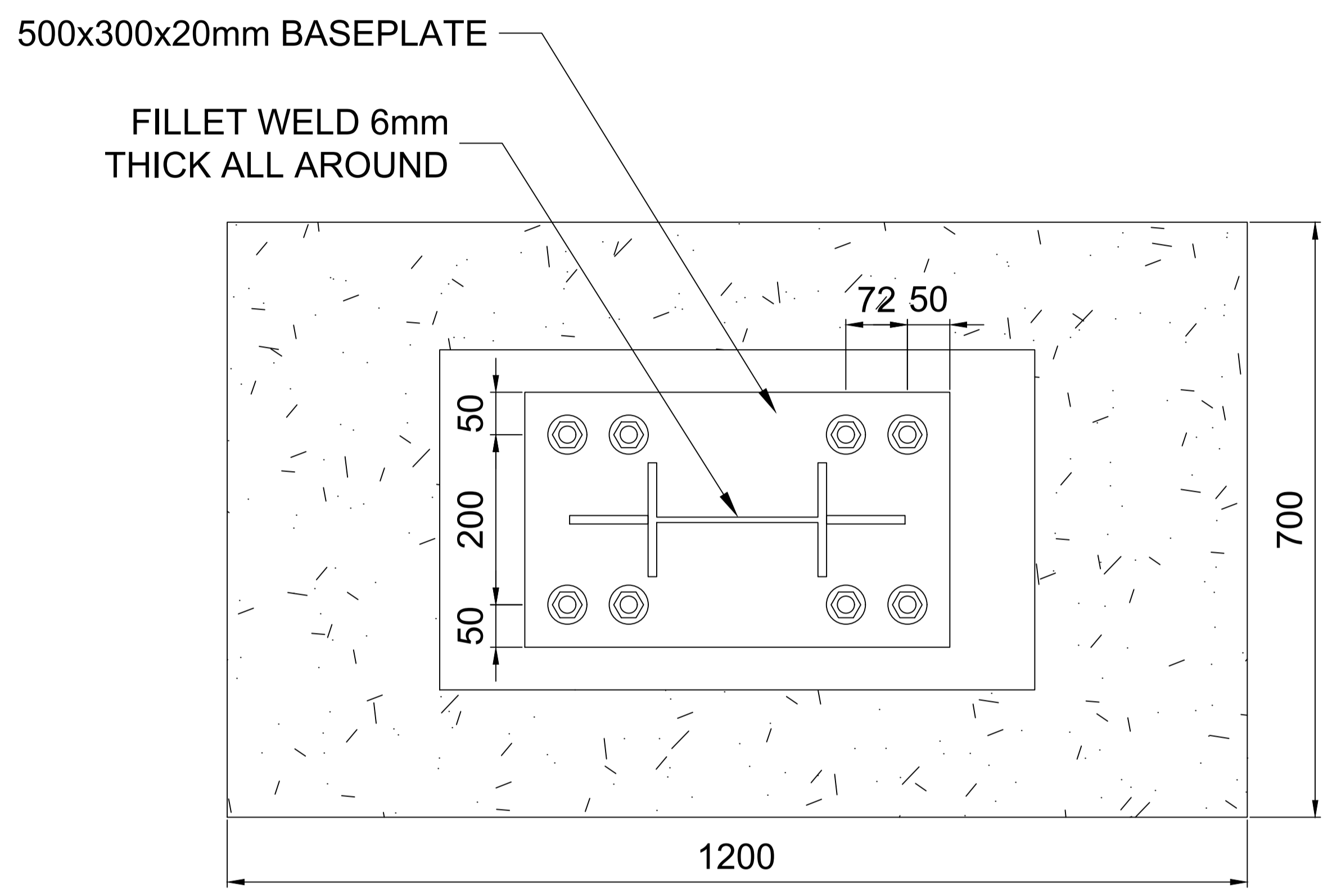


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**EAST MALL REDESIGN**  
 CANOPY CONNECTION DETAILS (Sheet 1 of 2)

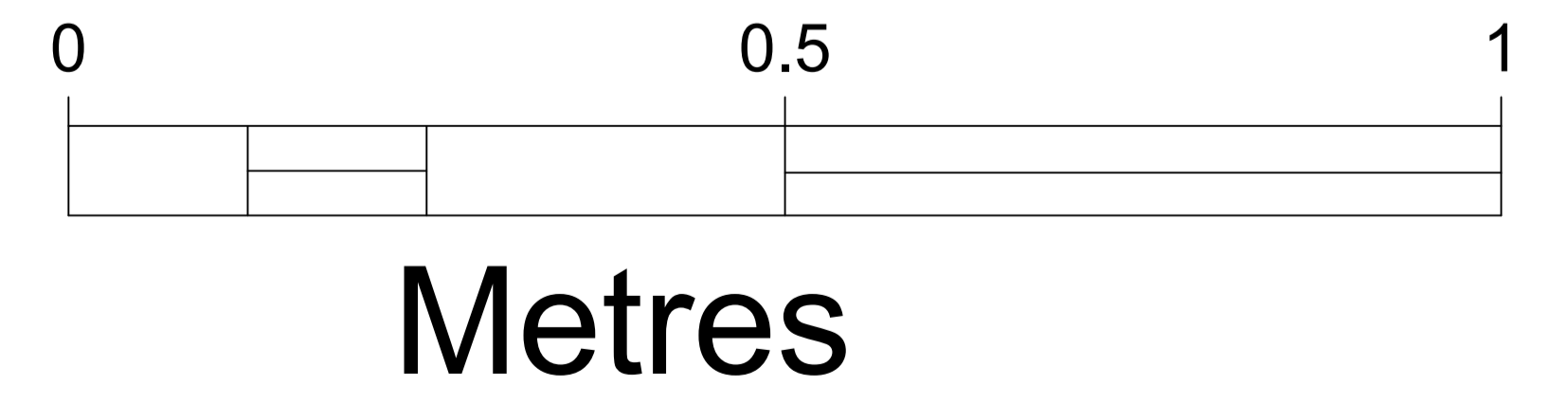
SCALE:	DATE (YYYY.MM.DD)
1:5	2021/04/16
DESIGNED JH	DWG. NO.
DRAWN JH	C103
REVIEWED DB	REV. 1



**COLUMN TO FOOTING CONNECTION DETAIL 1:5**



**COLUMN BASEPLATE DETAIL 1:5**



LEGAL DESCRIPTION			
SURVEY BENCHMARK			
REV.	DATE	DESCRIPTION	BY
5			
4			
3			
2			
1	2021/04/16	CANOPY COLUMN TO FOOTING DETAIL - FOR CONSTRUCTION	JH

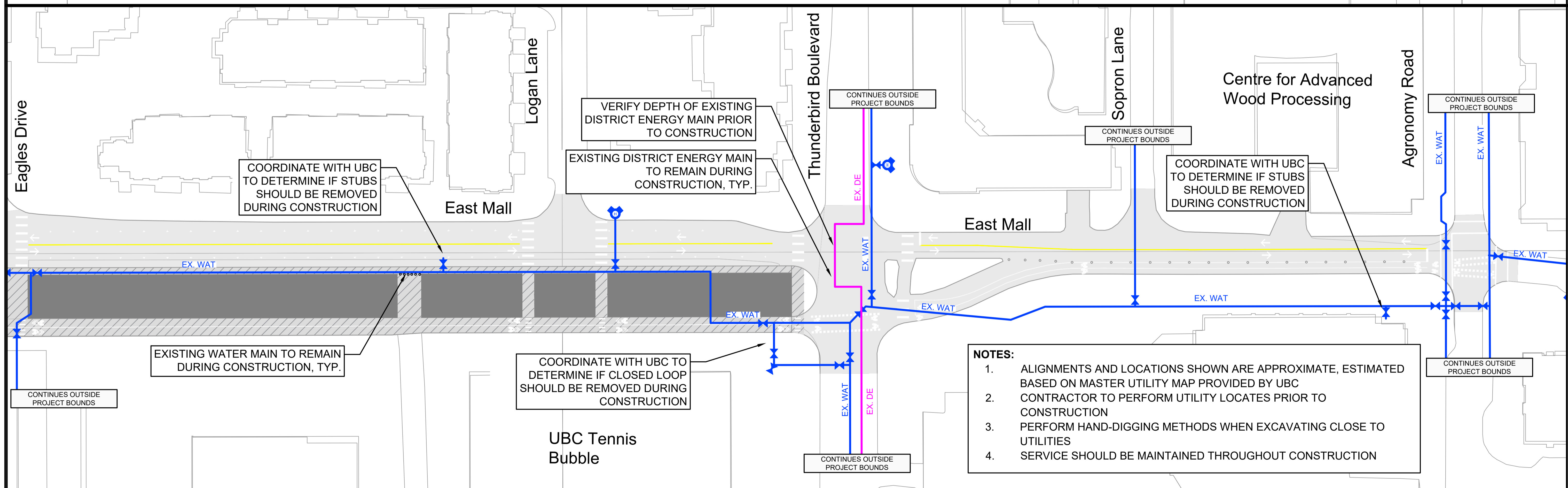
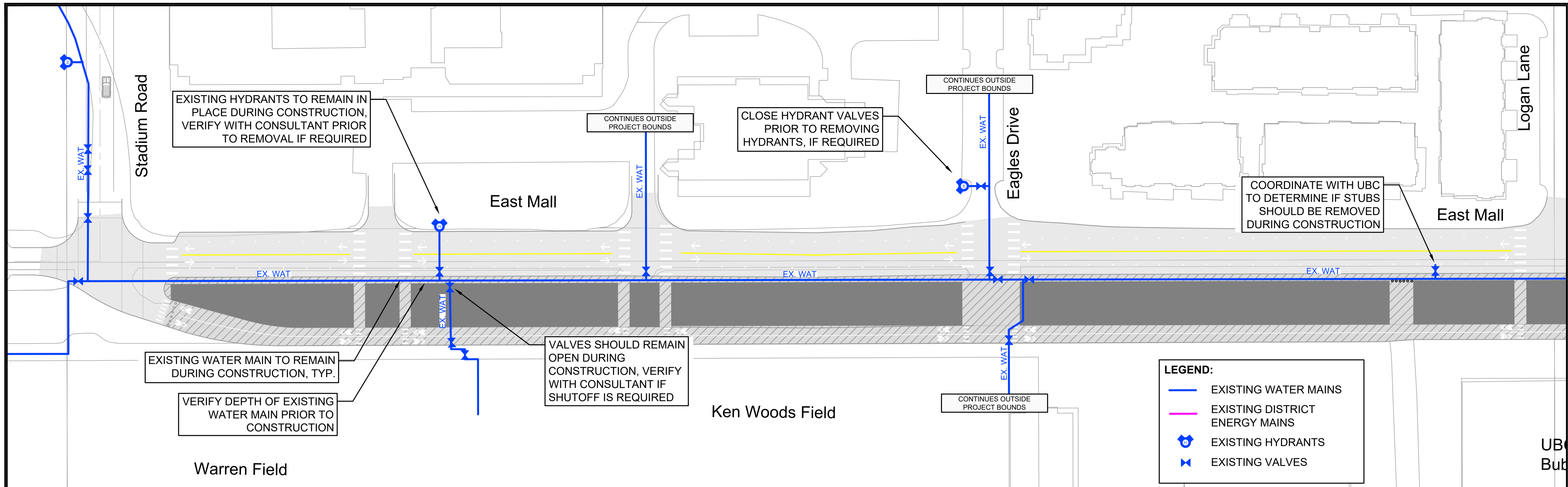
"BY SEALING AND SIGNING THIS DRAWING, I CERTIFY THAT THE INFORMATION CONTAINED IN THESE DRAWINGS ACCURATELY REFLECTS THE ORIGINAL DESIGN, ADDENDA, CHANGE ORDERS AND MATERIAL DESIGN CHANGES MADE DURING CONSTRUCTION AND FIELD REVIEWED BY ME, OR MY REPRESENTATIVE, AND THAT THE AS-CONSTRUCTED WORKS SUBSTANTIALLY COMPLY WITH THE ORIGINAL DESIGN INTENT. HOWEVER, I DO NOT ACCEPT RESPONSIBILITY FOR THE ACCURACY OR COMPLETENESS OF THE AS-CONSTRUCTED INFORMATION SUPPLIED BY OTHERS CONTAINED IN THESE DRAWINGS."

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**EAST MALL REDESIGN**  
 CANOPY CONNECTION DETAILS (Sheet 2 of 2)

SCALE:	DATE (YYYY.MM.DD)
1:40	2021/04/16
DESIGNED JH	DWG. NO.
DRAWN JH	C104
REVIEWED DB	REV. 1



LEGAL DESCRIPTION

SURVEY BENCHMARK

REV.	DATE	DESCRIPTION	BY
5			
4			
3			
2			
1	2021/04/16	UTILITIES PLAN - WATER	RH

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**EAST MALL REDESIGN**

Utilities Plan- Water

SCALE: 1:500

DATE (YYYY.MM.DD) 2021/04/16

DESIGNED RH

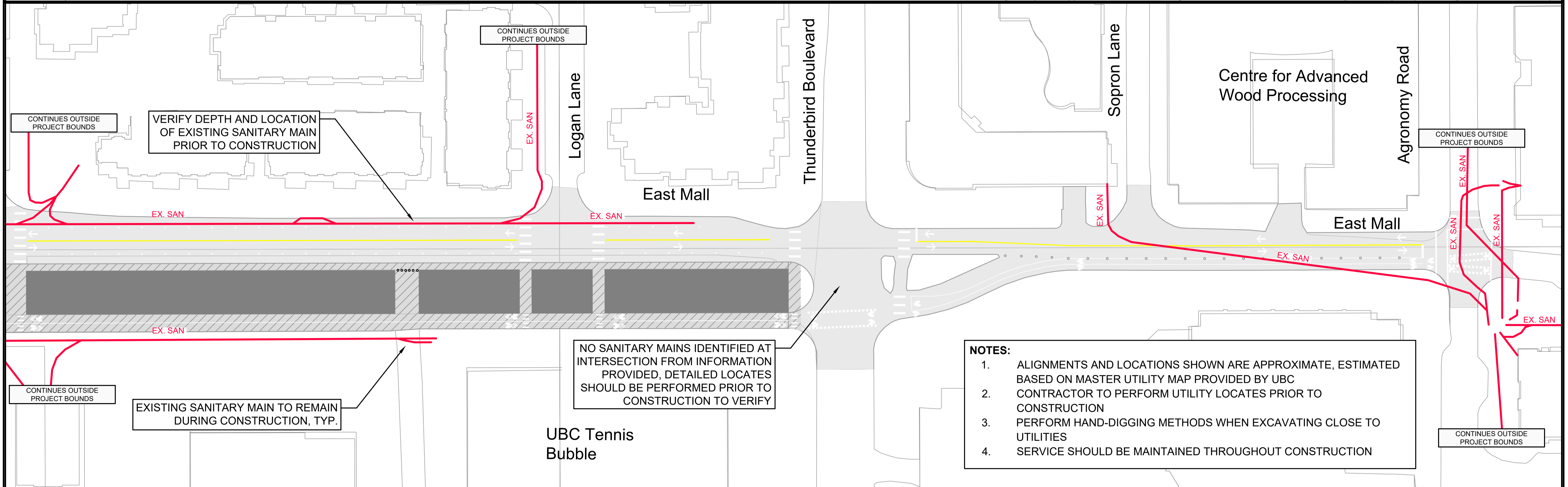
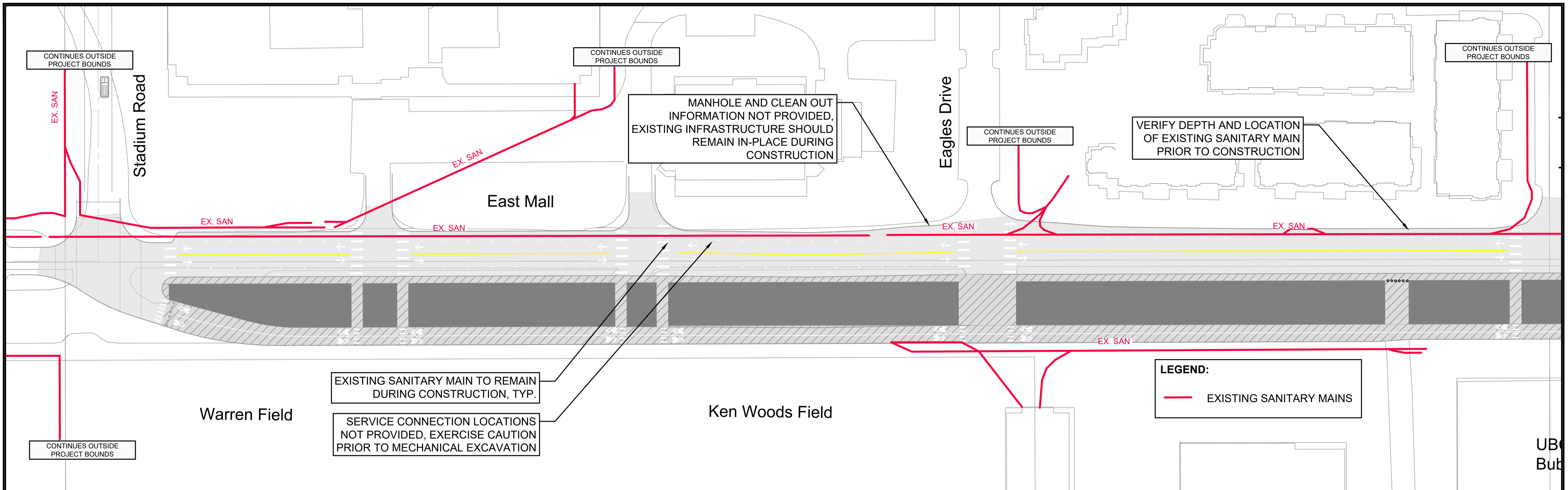
DRAWN RH

REVIEWED TM

DWG. NO. W101

REV. 1

Apr 15 2021 - 11:30am D:\Drive Documents\School Archive\2020\OVL 445\445-Water.dwg/W101.Roy



REV.	DATE	DESCRIPTION	BY
5			
4			
3			
2			
1	2021/04/16	UTILITIES PLAN - SANITARY	RH

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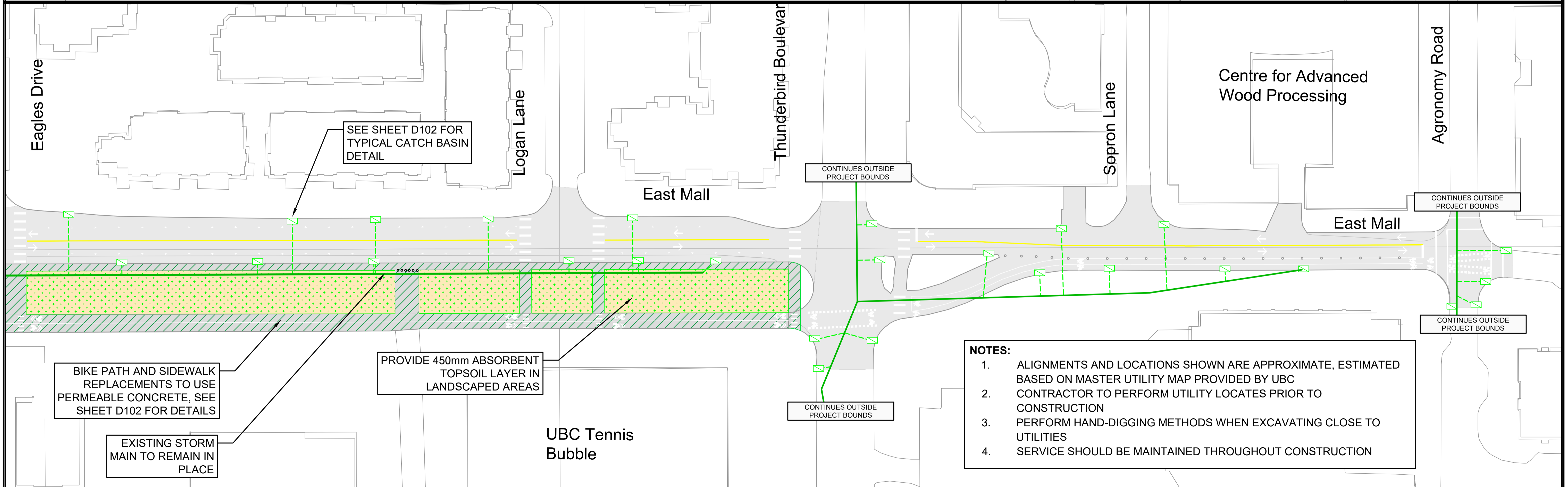
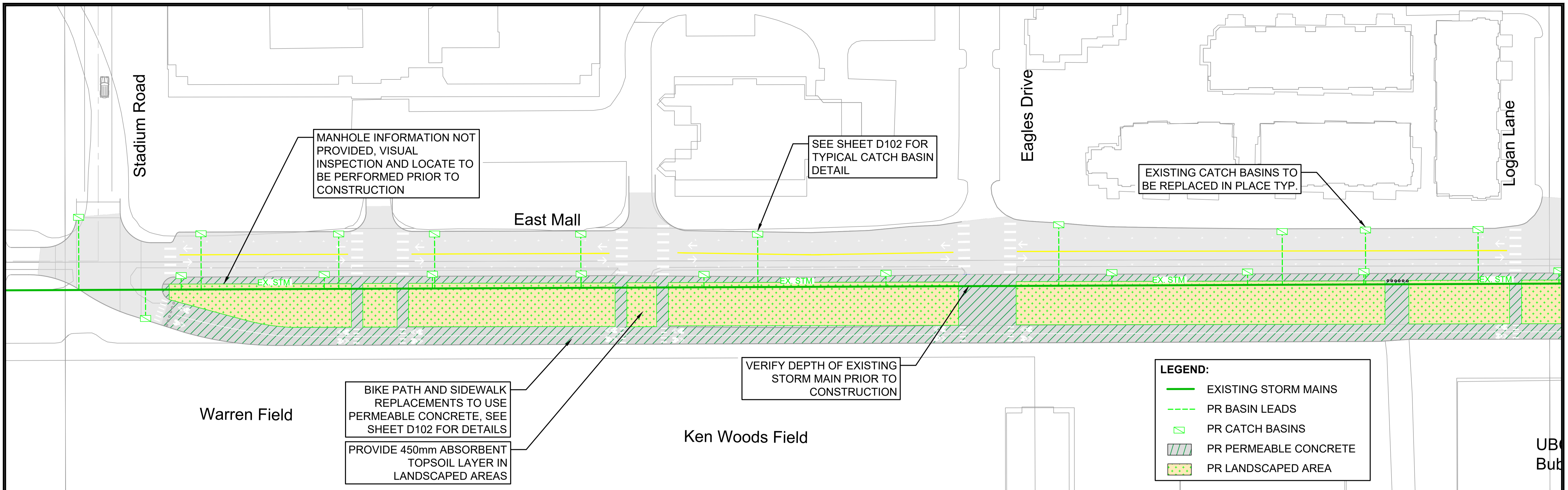
CONSULTANT



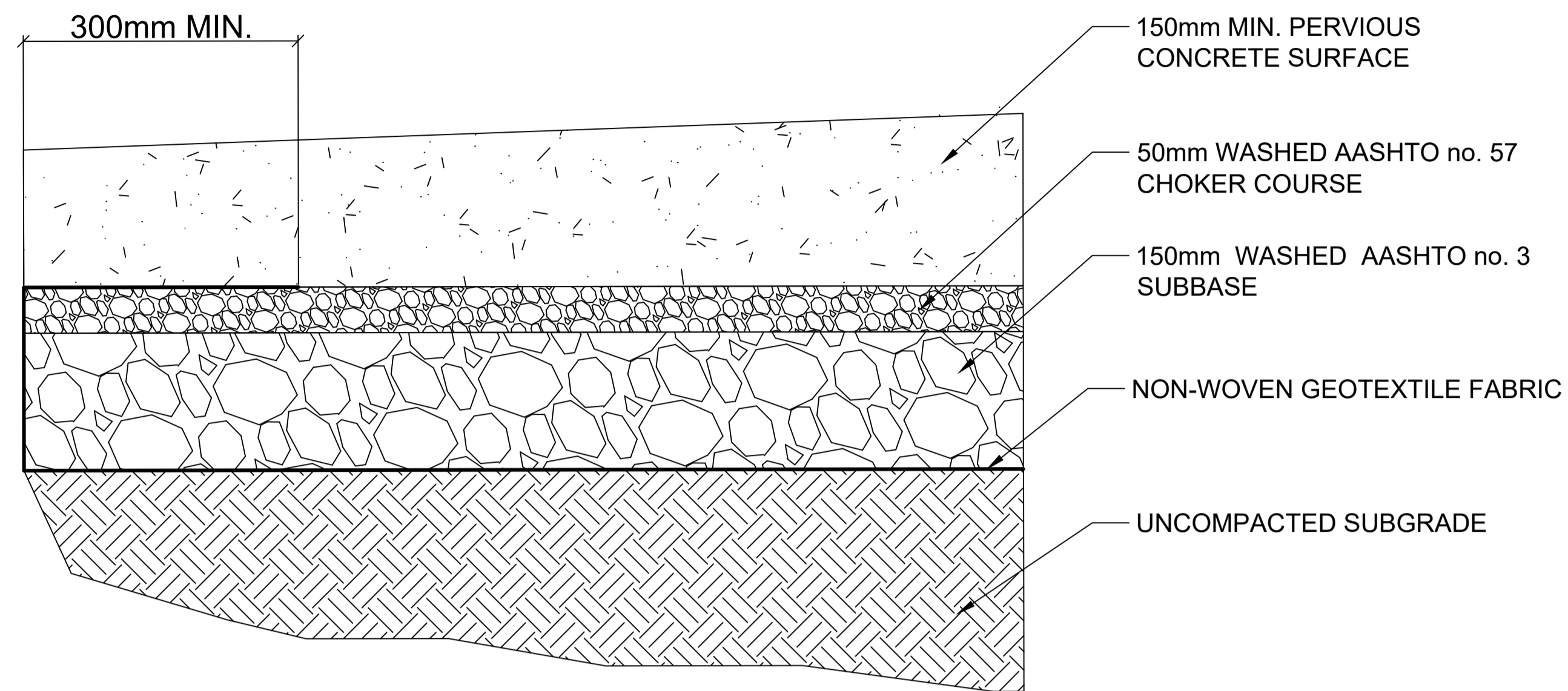
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Vancouver, BC V6T 1Z4

**EAST MALL REDESIGN**  
Utilities Plan - Sanitary

SCALE: <b>1:500</b>	DATE (YYYY.MM.DD) <b>2021/04/16</b>
DESIGNED RH	DWG. NO. <b>S101</b>
DRAWN RH	REV. <b>1</b>
REVIEWED TM	



LEGAL DESCRIPTION		"BY SEALING AND SIGNING THIS DRAWING, I CERTIFY THAT THE INFORMATION CONTAINED IN THESE DRAWINGS ACCURATELY REFLECTS THE ORIGINAL DESIGN. ADDENDA, CHANGE ORDERS AND MATERIAL DESIGN CHANGES MADE DURING CONSTRUCTION AND FIELD REVIEWED BY ME, OR MY REPRESENTATIVE, AND THAT THE AS-CONSTRUCTED WORKS SUBSTANTIALLY COMPLY WITH THE ORIGINAL DESIGN INTENT. HOWEVER, I DO NOT ACCEPT RESPONSIBILITY FOR THE ACCURACY OR COMPLETENESS OF THE AS-CONSTRUCTED INFORMATION SUPPLIED BY OTHERS CONTAINED IN THESE DRAWINGS."	CONSULTANT		CLIENT	<b>The University of British Columbia</b> 6250 Applied Science Ln Vancouver, BC V6T 1Z4	SEAL	SCALE:	DATE (YYYY.MM.DD)
SURVEY BENCHMARK								1:500	2021/04/16
REV.	DATE	DESCRIPTION	BY				DESIGNED	RH	DWG. NO.
5							DRAWN	RH	D101
4							REVIEWED	TM	REV. 2
3									
2	2021/04/16	UTILITIES PLAN - STORMWATER	RH						
1	2021/03/04	STORMWATER DESIGN PLAN	RH						



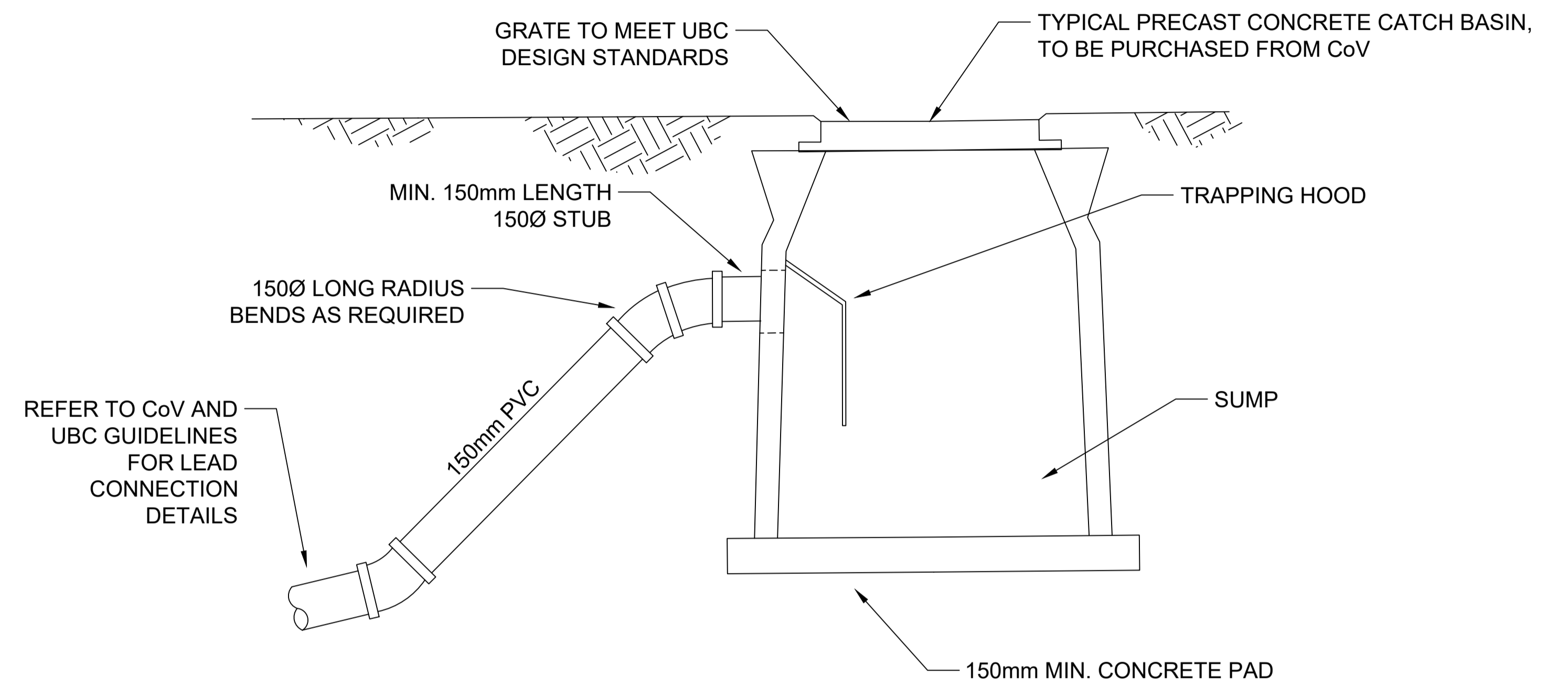
**PERMEABLE PAVEMENT DETAIL**

**NOTES**

1. REFER TO CONSTRUCTION SPECIFICATIONS FOR COMPREHENSIVE INSTALLATION AND TESTING REQUIREMENTS
2. PERMEABLE CONCRETE MIX SHALL BE TESTED DAILY BEFORE FIRST POUR TO VERIFY SLUMP IS WITHIN 15cm TO 18cm AND FRESH UNIT WEIGHT IS WITHIN 80kg/m<sup>3</sup> OF TARGET
3. ENSURE 95% PROCTOR COMPACTION WITHIN SUBBASE AND ADEQUATE MOISTURE PRIOR TO POURING PERMEABLE SURFACE MIX
4. PERMEABLE CONCRETE SURFACE TO BE CONSOLIDATED USING STEEL ROLLER
5. FINISHED SURFACE TO BE MISTED AND COVERED WITH PLASTIC SHEET FOR MINIMUM OF 7 DAYS WITHIN 20 MINUTES OF PLACEMENT

**PERMEABLE CONCRETE SPECIFICATIONS**

1. 18MPa 28-DAY COMPRESSIVE STRENGTH
2. 8600mm/hr INFILTRATION RATE
3. 15cm TO 18cm SLUMP
4. VOID-DENSITY CURVE TO BE PREDETERMINED THROUGH LAB TESTING



**TYPICAL CATCHBASIN DETAIL**

**NOTES**

1. REFER TO CoV STANDARD CONSTRUCTION DOCUMENTS FOR DETAILED INSTALLATION REQUIREMENTS
2. ALTERNATIVE PRECAST CONCRETE CATCHBASIN MEETING MMCD REQUIREMENTS MAY BE USED IF PRE-APPROVED BY DESIGN ENGINEER
3. TRAPPING HOOD CAN BE PURCHASED AND INSTALLED SEPARATELY
4. EXISTING CATCH BASINS FROM ROAD RESTORATION TO BE REUSED WHEREVER POSSIBLE
5. ENSURE GRATE IS ALIGNED WITH FLOW DIRECTION

LEGAL DESCRIPTION			
SURVEY BENCHMARK			
REV.	DATE	DESCRIPTION	BY
5			
4			
3			
2	2021/04/16	Stormwater Design Details - IFC	RH
1	2021/03/04	Stormwater Design Details	RH

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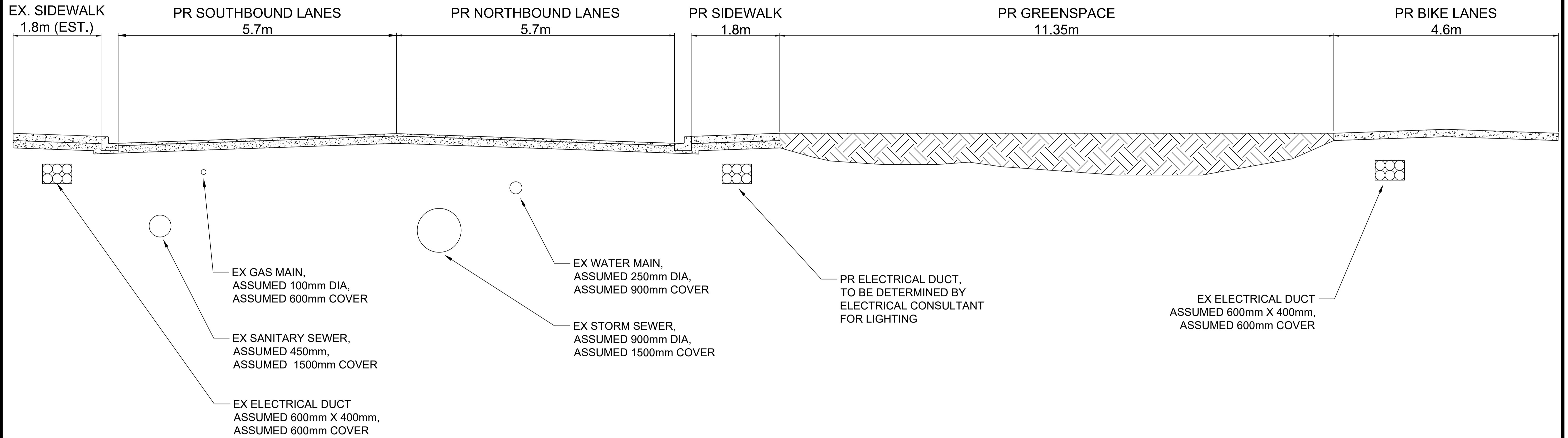
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 Vancouver, BC V6T 1Z4  
**EAST MALL REDESIGN**  
 STORMWATER DESIGN DETAILS

SCALE:	N.T.S.	DATE (YYYY.MM.DD)	2021/04/16
DESIGNED	RH	DWG. NO.	D102
DRAWN	RH	REV.	2
REVIEWED	TM		





**TYPICAL UTILITY CROSS-SECTION  
THUNDERBIRD TO STADIUM**

REV.	DATE	DESCRIPTION	BY
5			
4			
3			
2	2021/04/16	IFC Utility Cross-Section	RH
1	2021/03/04	Initial Utility Cross-Section	RH

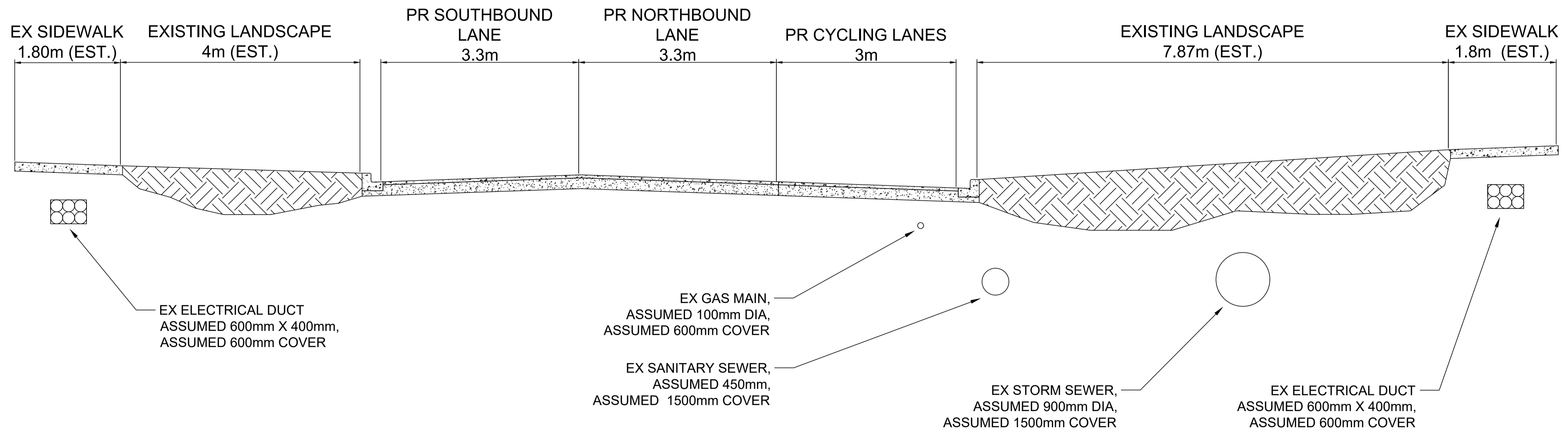
"BY SEALING AND SIGNING THIS DRAWING, I CERTIFY THAT THE INFORMATION CONTAINED IN THESE DRAWINGS ACCURATELY REFLECTS THE ORIGINAL DESIGN, ADDENDA, CHANGE ORDERS AND MATERIAL DESIGN CHANGES MADE DURING CONSTRUCTION AND FIELD REVIEWED BY ME, OR MY REPRESENTATIVE, AND THAT THE AS-CONSTRUCTED WORKS SUBSTANTIALLY COMPLY WITH THE ORIGINAL DESIGN INTENT. HOWEVER, I DO NOT ACCEPT RESPONSIBILITY FOR THE ACCURACY OR COMPLETENESS OF THE AS-CONSTRUCTED INFORMATION SUPPLIED BY OTHERS CONTAINED IN THESE DRAWINGS."

CONSULTANT



CLIENT  
**The University of British Columbia**  
 6250 Applied Science Ln  
 Vancouver, BC V6T 1Z4  
**EAST MALL REDESIGN**  
 Utility Cross-Sections (Sheet 1 of 2)

SCALE:	DATE (YYYY.MM.DD)
1:40	2021/04/16
DESIGNED	DWG. NO.
RH	U101
DRAWN	REV.
RH	2
REVIEWED	
TM	



**TYPICAL UTILITY CROSS-SECTION  
AGRONOMY TO THUNERBIRD**

LEGAL DESCRIPTION			
SURVEY BENCHMARK			
REV.	DATE	DESCRIPTION	BY
5			
4			
3			
2	2021/04/16	IFC Utility Cross-Section	RH
1	2021/03/04	Initial Utility Cross-Section	RH

"BY SEALING AND SIGNING THIS DRAWING, I CERTIFY THAT THE INFORMATION CONTAINED IN THESE DRAWINGS ACCURATELY REFLECTS THE ORIGINAL DESIGN, ADDENDA, CHANGE ORDERS AND MATERIAL DESIGN CHANGES MADE DURING CONSTRUCTION AND FIELD REVIEWED BY ME, OR MY REPRESENTATIVE, AND THAT THE AS-CONSTRUCTED WORKS SUBSTANTIALLY COMPLY WITH THE ORIGINAL DESIGN INTENT. HOWEVER, I DO NOT ACCEPT RESPONSIBILITY FOR THE ACCURACY OR COMPLETENESS OF THE AS-CONSTRUCTED INFORMATION SUPPLIED BY OTHERS CONTAINED IN THESE DRAWINGS."

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**EAST MALL REDESIGN**  
 Utility Cross-Sections (Sheet 2 of 2)

SCALE:	DATE (YYYY.MM.DD)
1:40	2021/04/16
DESIGNED RH	DWG. NO.
DRAWN RH	U102
REVIEWED TM	REV. 2

# APPENDIX B – CONSTRUCTION SPECIFICATIONS

## ROADWAY

### Part 1 General

#### 1. Related Sections

- a. Roadway Drawings
- b. Detailed Design Report

#### 2. References

- a. Transportation Association of Canada Geometric Design Guide for Canadian Roads
- b. British Columbia Active Transportation Guide
- c. City of Vancouver Design Manual

#### 3. Design Criteria

- a. **General.** Review and submit documents required to construct the work for accuracy, completeness, and compliance with the contract for approval by the Owner's Representative (OR). Documents submitted without evidence of Contractor approval may be returned for resubmission. Time for approval starts over when documents are returned for revision or if additional information is requested by the OR. Do not perform work related to submitted documents or drawings before approval of the OR. Obtain written approval before changing or deviating from the approved drawings.
- b. Typical surfacing, as per City of Vancouver Design Guidelines, shall include the following:
  - i. 50mm Superpave surface mix
  - ii. 180mm Superpave base mix implemented in two lifts
  - iii. 150mm minus crushed, 19mm granular base
- c. Typical surfacing for bike lane:
  - i. 50mm porous concrete surface mix
  - ii. 150mm crushed base implemented in two lifts
- d. Maximum grade of 2.5% in travel lanes

#### 4. Execution

- a. Verify that rough-in utilities are in proper location.
- b. Verify that road surfaces are ready to receive work.

#### 5. Materials

- a. **Material sources**
  - i. Material source must be government-approved sources unless otherwise approved
- b. **Handling and Storing Material**
  - i. Handle and store material to preserve its quality and fitness for the work
  - ii. Use only approved portions of the right-of-way for storing material or equipment, do not use private property for storage without written permission
  - iii. Provide security for stored material
- c. Aggregate Gradation shall be determined in accordance with ASTM C117 (Wash Test)
- d. Any Aggregate supplied must not rut when proof rolled with a truck having a 9 tonne single axle dual tire or 17 tonne tandem axle group with dual tires with a tire pressure of 600 kPa.
- e. Water for compaction or dust control shall be incidental to the bid price for the granular material.

#### 6. Acceptance of Work

- a. **Conformity with Contract Requirements**

## ROADWAY

- i. Perform work to the lines, grades, cross-sections, dimensions shown in the contract
- ii. Unless specific contract tolerances are noted, established manufacturing tolerances will be accepted for standard manufactured items
- iii. The owner may inspect, sample, or test work before final acceptance of the project.

## CANTILEVERED WALKWAY COVER

### Part 1 General

#### 1. RELATED SECTIONS

- a. Structural Drawings
- b. Detailed Design Report

#### 2. REFERENCES

- a. National Building Code of Canada 2015
- b. British Columbia Building Code 2018
- c. American Society for Testing and Materials International (ASTM)
- d. Canadian Standards Association (CSA International)

#### 3. DESIGN CRITERIA

- a. Beam and column depths are shown on the drawings. Adjust beam and column material thicknesses and spacings, as required by the design criteria. Use greater or lesser beam and column depths only if approved by the Consultant.
- b. For beam and columns, conform to the minimum design thicknesses, 95% of the design thickness as limited by CSA-S136
- c. Maximum flexural deflections under specified live shall conform to the following:
  - i. Beam and column,  $L/120$ .
- d. Wall Assembly:
  - i. Refer to Structural Drawings for deflection requirements for, wind loads, tolerances, drift requirements and other design parameters.
  - ii. Design to provide for movement of components without damage, failure of joint seals, undue stress on fasteners, or other detrimental effects when subject to seasonal or cyclic day/night temperature ranges.
  - iii. Design to accommodate construction tolerances, deflection of building structural members, and clearances of intended openings.

#### 4. QUALITY ASSURANCE

- a. Professional Engineer Qualifications: A professional engineer who is legally qualified to practice in jurisdiction where Project is located and who is experienced in providing engineering services of kind indicated. Engineering services are defined as those performed for installations of sun controls that are similar to those indicated for this Project in material, design, and intent.
  - i. Welding Standards: As follows:
    1. Structural Welding Code—Steel
  - ii. Certify that each welder has satisfactorily passed AWS qualification tests for welding processes involved and, if pertinent, has undergone recertification. SMACNA Standard: Comply with SMACNA's "Architectural Sheet Metal Manual" recommendations for fabrication, construction details, and installation procedures.

### Part 2 Products

#### 1. FRAMING MATERIALS

- a. Framing Materials: Cold-rolled steel, with metallic coating, minimum coating thickness Z180 (G60). Minimum 18 gauge.

#### 2. ACCESSORIES

## CANTILEVERED WALKWAY COVER

- a. Stiffener Plates: Formed sheet steel, thickness determined by performance requirements specified.

### 3. FASTENERS

- a. Bolts, Nuts and Washers: ASTM A307 or ASTM A325, hot dip galvanized to minimum requirements of CSSBI.
- b. Anchorage Devices: Drilled expansion bolts, screws with sleeves.

### 4. FABRICATION

- a. Fabricate assemblies of formed sections of sizes and profiles required.
- b. Provide cut-outs centered in webs of members to accommodate services and through-the-knockout style bridging.
- c. Fit, reinforce, and brace framing members to suit design requirements.
- d. Fit and assemble in largest practical sections for delivery to site, ready for installation.
- e. Do welding to CSA S136, as applicable.

## Part 3 Installation and Execution

### 1. PREPARATION

- a. Coordinate Installation Drawings, diagrams, templates, instructions, and directions for anchorages that are to be embedded in concrete or masonry construction. Coordinate delivery of such items to Project site.

### 2. ERECTION

- a. Canopies are to be installed according to approved shop drawings and plans.
- b. The entire structure shall be installed straight, true, and plumb according to standard construction procedures.
- c. Canopies shall be installed minimal slope to allow water flow from top of canopy to draining columns and eliminate ponding.
- d. All joints, corners, and connections shall be tight and clean.
- e. All exposed fasteners are to be painted to match the canopy color.
- f. Decking is to be aligned and secured to aluminum frame structure.

### 3. COLUMN FOUNDATION

- a. Styrofoam blockouts shall be provided by the canopy manufacturer and installed by the General Contractor into the concrete foundation.
- b. General Contractor shall pour the required concrete foundation size around the Styrofoam blockouts provided by the manufacturer.
- c. Canopy installer is to remove the Styrofoam after the foundation has cured, set column in cavity, and fill with minimum 2000 psi grout to level of finished concrete slab.

### 4. CLEANING

- a. All canopy surfaces exposed are to be cleaned after installation is complete.
- b. Surplus materials and debris shall be removed from the jobsite after installation is complete.

**END OF SECTION**

**Part 1 General**

**1. RELATED SECTIONS**

- a. Utilities Drawings
- b. Detailed Design Report

**2. REFERENCES**

- a. City of Vancouver Engineering Design Manual
- b. City of Surrey Design Criteria Manual
- c. UBC Integrated Stormwater Management Plan
- d. American Society for Testing and Materials International (ASTM)
- e. American Concrete Institute (ACI)
- f. American Water Works Associations (AWWA)
- g. Master Municipal Construction Documents (MMCD)

**Part 2 Products**

**1. STORMWATER AND GRAVITY FED SANITARY MAINS AND CONNECTIONS**

- a. PVC, class SDR for pipes under 150mm and SDR 35 for pipes in diameter up to 600mm
- b. Concrete (reinforced C76 required for all pipes 600mm in diameter and larger)
- c. Water

**2. WATERMAINS AND CONNECTIONS**

- a. Class 50 ductile iron pipe in accordance with AWWA, cement mortar lined to AWWA C104 and coated with 1mm thick asphalt coating or approved equivalent
- b. Type K copper pipes with brazed joints up to 75mm for connections up to 75mm
- c. Single rubber gasket Tyton joints in accordance with AWWA C111 for push-on bell and spigot type joints or approved equivalent
- d. Flat faced flanged joints in accordance with AWWA C110
- e. Fittings to be ductile iron in accordance with AWWA C110 along with pressure rating of 2415 kPa
- f. Minimum design pressure for piping is 1210 kPa

**3. SANITARY FORCEMAINS**

- a. PVC, Class C900 for mains under 300mm diameter and C905 for any larger mains

**4. ACCESSORIES**

- a. Ductile iron gate valves in accordance with AWWA C509 with flanged or hub ends
- b. Nelson-type circular valve boxes manufactured by Terminal City of Dobney foundry
- c. 150mm diameter Terminal City type C-71-P hydrants, tested to 2070 kPa hydrostatic pressure in accordance with AWWA C502
- d. Concrete catch basins to be purchased from City of Vancouver, including trapping hoods and typical sump

**5. PIPE BEDDING AND SURROUND MATERIALS**

- a. 19mm minus, MMS type 1, cleaned, granular pipe bedding with minimum bottom thickness of 100mm, 300mm top thickness, 225mm minimum side thickness
- b. Use native backfill wherever possible under paved areas
- c. Imported bedding must be approved by UBC Energy & Water Services prior to use



**Part 3 Execution**

**1. GENERAL**

- b. Existing utility mains should be left in place during construction unless explicit direction is provided by the Consultant or UBC Water & Energy Services
- c. Existing ground-level infrastructure including fire hydrants, manholes, cleanouts, and inspection chambers should be left in place during construction unless explicit direction is provided by the Consultant or UBC Water & Energy Services
- d. Relocated catch basins should be reused wherever possible as long as visual inspection suggests adequate quality. If any leakage is observed from catch basin, existing catch basin should be discarded, and new basin used as specified

**2. PREPARATION AND TRENCHING**

- a. Site preparation to follow details outlined in MMCD Section 02666
- b. Trenching to follow details outlined in City of Vancouver Construction Specifications Section 31 23 01

**3. INSTALLATION**

- a. Maintain 3m horizontal clearance between parallel sanitary sewer or storm sewer mains and water mains. If existing clearance is less, or if approved by UBC Water & Energy Services, installation should follow details in MMCD Design Guideline Manual Section 1.4 and Vancouver Coastal Health's Water Supply System Construction Permit Guidelines and Application. Water main joints should be wrapped in shrink plastic or petroleum tape in accordance with AWWA C217, C214, and C209
- b. Maintain 750mm clearance between water mains and other utility services, and 3m clearance to building foundations
- c. Prior to covering, pipe and bedding should be inspected by UBC Energy & Water Services. Contractor shall provide written notification to both the Utilities Engineer and Head Plumber with a minimum of 24 hours' notice
- d. Contractor shall be responsible for maintaining detailed records of pipe sizes and inverts to be provided to UBC's Records Manager, Infrastructure Development, and Mechanical Utilities Engineer in accordance with Section 01 78 39 of UBC's Project Record Documents Technical Guidelines
- e. Upon completion of pipe laying, pipes should be surrounded and covered with specified backfill. Joints and fittings should be exposed until field testing is complete
- f. Backfill and pipe surround should be compacted to at least 95% Modified Proctor Density

**4. FLUSHING AND TESTING**

- a. Cleaning, flushing, and pressure testing to be conducted by Contractor
- b. Engineer should be notified within 24 hours of and present for proposed test
- c. Contractor shall apply for UBC Hydrant Use Permit prior to using water supplied from UBC fire hydrants for cleaning and flushing
- d. Pressure and leakage testing for PVC piping to AWWA M23 standards, HDPE piping to AWWA M55 standards, with no leakage allowed and pressures not exceeding CSA B137.3

**END OF SECTION**

# PERMEABLE CONCRETE

## Part 1 General

### 1. RELATED SECTIONS

- a. Permeable Concrete Detail Drawing
- b. Detailed Design Report

### 2. REFERENCES

- a. City of Vancouver Engineering Design Manual
- b. UBC Integrated Stormwater Management Plan
- c. American Society for Testing and Materials International (ASTM)
- d. American Concrete Institute (ACI)
- e. American Association of State Highway and Transportation Officials
- f. National Ready Mixed Concrete Association
- g. UNHSC Design Specifications for Porous Asphalt Pavement and Infiltration Beds
- h. Flood Testing Labs

## Part 2 Products

### 1. Specifications

- a. Final concrete mix must adhere to the following property requirements as determined through lab testing in accordance with ACI standards:

Property	Specification
28-Day Compressive Strength	20 MPa
Infiltration Rate	8600 mm/hr
Void Space	15%
Unit Weight	1500 kg/m <sup>3</sup> to 2000 kg/m <sup>3</sup>
Slump	15cm to 18cm

- b. Contractor to develop target void-density curve for final mix design for use during field testing

### 2. Materials

- a. Contractor to develop mix design meeting specifications outlined above and seek approval from Engineer prior to construction
- b. Calcium chloride is not permitted in any form in mix
- c. Material Source must be government-approved unless specified with grading and density following those outlined in Drawing D102
- d. Filter geotextiles shall meet requirements outlined in AASHTO M288 for Class 2

## Part 3 Execution

### 5. PRE-INSTALLATION

- a. A minimum of two panel tests to be conducted on site on native material in accordance with ACI 522.1-13. Panels must have minimum area of 225 sq. ft, with width and thickness outlined in construction drawings.
- b. Dimensions and density of hardened cores must be recorded to establish acceptable reference points for quality assurance purposes

### 6. SUBBASE AND SUBGRADE PREPARATION

## PERMEABLE CONCRETE

- a. Do not compact subgrade beyond 90% of theoretical density to maintain void spaces
- b. Subgrade should be cleaned prior to installation
- c. Moisten subgrade and ensure no free-standing water is visible prior to placement

### **7. INSTALLATION**

- a. Mix must be completely discharged within one hour of initial mixing and visually inspected for consistency and even aggregate coating
- b. Placement shall be done in a continuous pour into conventional formwork with mechanical screeds used and strike offs done 20 mm above formwork
- c. Consolidate concrete using steel roller within 15 minutes of placement
- d. Control joints shall be placed every 6m in with a depth of  $\frac{1}{4}$  of the slab thickness
- e. Moisten concrete surface with water then cover with plastic sheeting within 20 minutes of initial placement
- f. Plastic cover should be held down and remain in place for a minimum of 7 days or until core tests are completed.
- g. Formwork shall be left in place for a minimum of 28 days unless otherwise directed

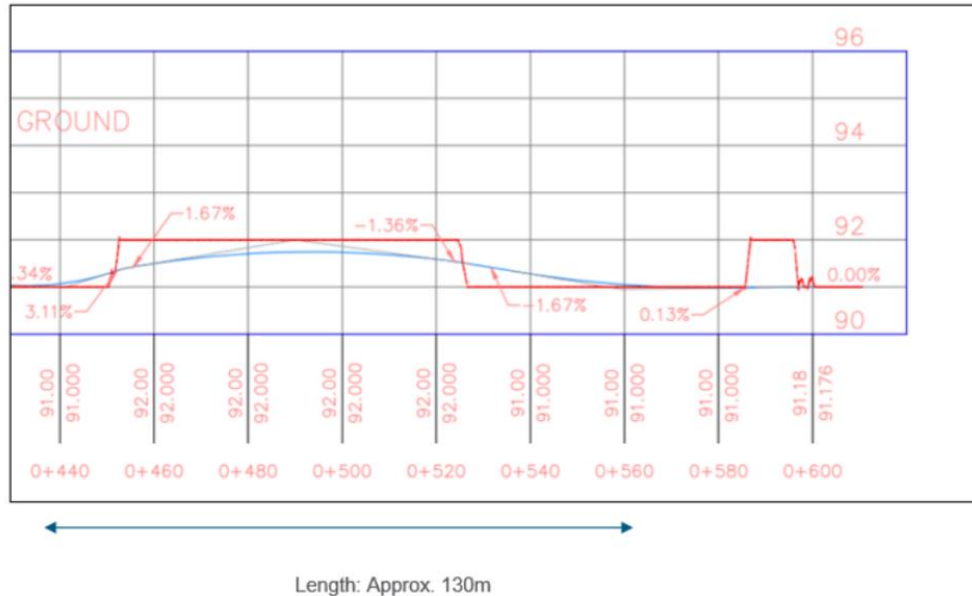
### **8. INSPECTION AND TESTING**

- a. Three core samples will be tested for every 75 m<sup>3</sup> poured on-site. The average density of these cores must be within 5% of the density determined from the test panel cores, thickness within 19mm, and average length within -10mm and 38mm of design values in accordance with ASTM C1754
- b. Infiltration testing will be conducted in accordance with ASTM C1701

**END OF SECTION**

# APPENDIX C – SAMPLE TRANSPORTATION CALCULATIONS

## Road Crest Curve Calculations



Example curve: Crest curve at Station  $\equiv 0 + 500$

Elevation of highest point =  $\sim 91.75m$

Length of crest curve =  $\sim 130m$

Calculations shown below.

### CREST CURVE CALCULATION

$$S \text{ (Sight Distance)} = (50/3.6)*2.5 + ((50/3.6)^2 / (2*0.3*9.81)) = 67.49511 \text{ m}$$

Assume  $S < L$

$$L \text{ (Length of Vertical Curve)} = (AS^2) / (100 * (\sqrt{2*H1} + \sqrt{2*H2})^2) = 33.80774 \text{ m}$$

$S > L$

$$L \text{ (Length of Vertical Curve)} = 2S - (200 * (\sqrt{H1} + \sqrt{H2})^2) / A = 129.0009 \text{ m}$$

>> **Use 130 m**

$$\text{Station VPC} = \text{Station VPI} - L/2 = 0 + 500 - 65 = 0 + 435$$

$$\text{Station VPT} = \text{Station VPI} + L/2 = 0 + 500 + 65 = 0 + 565$$

$$\text{Elevation VPC} = \text{Elevation VPI} - G(L/2) = 91.75 - 0.0167*65 = 91.1645 \text{ m}$$

$$\text{Elevation VPC} = \text{Elevation VPI} - G(L/2) = 91.75 - 0.0136*65 = 91.366 \text{ m}$$

$$\text{Location of High Point} = (g1*L) / (g2 - g1) = (1.67*130) / (3) = 72.36667 \text{ m}$$

>> **Use 75 m**

$$0 + 435 + 75 = 0 + 510$$

$$\text{Elevation of High Point} = 90.66 + 0.0167*75 + ((-0.03*75^2) / (2*130)) + 91.76796 \text{ m}$$

# APPENDIX D – STRUCTURAL CALCULATIONS

## A DIMENSIONS

Length of Roof	3.6 m
Col to Col	1.8 m
Cover Length	3.16 m
Column Height	3.07 m
Length of Section	2.6 m
Reference height	3.5519 m
Maximum height	3.8414 m
Cantilever Trib A	3.24 m <sup>2</sup> half of roof

## B SNOW

I <sub>s</sub>	1 Normal Importance
S <sub>s</sub>	1.8 Vancouver City Hall
C <sub>b</sub>	0.8
>I <sub>c</sub>	2.353846154 70 C <sub>b</sub> = 0.8
>>w	1.8
C <sub>w</sub>	1
C <sub>s</sub>	1
C <sub>a</sub>	1
S <sub>r</sub>	0.2
S	1.64 kPa
Load on Cantilever Column	1.476 kN/m 5.3136 kN

$$S = I_s [S_s (C_b C_w C_s C_a) + S_r]$$

## C WIND

I <sub>w</sub>	1
q	0.45
C <sub>e</sub>	0.7
>(h/10) <sup>0.2</sup>	0.9
>0.7*(h/12) <sup>0.3</sup>	0.7
C <sub>t</sub>	1
C <sub>g</sub>	2
C <sub>p</sub>	-0.5
>H/D	1.067055556
C <sub>ei</sub>	0.7
C <sub>gi</sub>	1.999962112
>V <sub>o</sub>	19.6560216 m <sup>3</sup>
>A	37.32156 m <sup>2</sup>
C <sub>pi</sub>	-0.7
W <sub>ext</sub>	-0.315 kPa
W <sub>int</sub>	-0.88198329 kPa
W <sub>sum</sub>	-1.196983292 kPa

$$p_i = I_w q C_{ei} C_t C_{gi} C_{pi}$$

Load on Cantilever Column	-1.077285 kN/m -3.8782259 kN
---------------------------	---------------------------------

## D DEAD

Cantilever Section	W200x31	Column Section	W200x31	W200x31
A	4000 mm <sup>2</sup>	A	4000 mm <sup>2</sup>	
r <sub>x</sub>	88.6 mm	r <sub>x</sub>	88.6 mm	
r <sub>y</sub>	32 mm	r <sub>y</sub>	32 mm	
Cross Section		Densities		Loads
Steel Column	0.01228 m <sup>3</sup>	8050 kg/m <sup>3</sup>		0.9697577 kN
Cantilever	0.004 m <sup>2</sup>	8050 kg/m <sup>3</sup>		0.315882 kN/m
Glass Panels	0.02 m	2500 kg/m <sup>3</sup>		0.4905 kN/m <sup>2</sup>
>Glass Length	3.2 m			
>Glass Thickness	0.02 m			
Load on Cantilever Column				0.757332 kN/m 4.1810318 kN

## E Load Combinations

Summary of Loads	Cantilever	Column	Servicability	Cantilver	Column
Snow	1.48 kN/m	5.31 kN	1.0*D+1.0*S+1.0*W	3.31	13.37
Wind	1.08 kN/m	3.88 kN			
Dead	0.76 kN/m	4.18 kN			
1 1.4D	1.06 kN/m	5.85 kN			
2 1.25D+1.0S or 0.4W	2.42 kN/m	10.54 kN			
3 1.25D+1.5S+0.4W	3.59 kN/m	14.75 kN			
4 1.25D+1.4W+0.5S	3.19 kN/m	13.31 kN	1.25D	0.946665	
5 1.0D		4.18 kN	1.5S	2.214	
			0.4W	-0.430913985	
M <sub>f</sub>	17.93 kNm	11.64			
V <sub>f</sub>	11.35 kN	N/A			

## F FLEXURE

CANTILEVER		W200x31		COLUMN		W200x31	
E	200000 MPa			E	200000 MPa		
G	76923.07692 MPa			G	76923.07692 MPa		
J	119000 mm <sup>4</sup>			J	119000 mm <sup>4</sup>		
I <sub>y</sub>	4100000 mm <sup>4</sup>			I <sub>y</sub>	4100000 mm <sup>4</sup>		
bel	134 mm			bel	134 mm		
t	10.2 mm			t	10.2 mm		
C <sub>w</sub>	40900000000 mm <sup>6</sup>			C <sub>w</sub>	40900000000 mm <sup>6</sup>		
z <sub>x</sub>	335000 mm <sup>3</sup>			z <sub>x</sub>	335000 mm <sup>3</sup>		
s <sub>x</sub>	299000 mm <sup>3</sup>			s <sub>x</sub>	299000 mm <sup>3</sup>		
Phi	0.9			Phi	0.9		
bel/t	6.57	<	7.750576015 Class 1	bel/t	6.57	<	7.750576015 Class 1
		<	9.086882225 Class 2			<	9.086882225 Class 2
		<	12.82853961 Class 3			<	12.82853961 Class 3
delta_max	54.5921141 mm			delta_max	54.5921141 mm		
My	94.185 kNm			My	94.185 kNm		
0.67*My	63.10395 kNm			0.67*My	63.10395 kNm		
Mu	286.7470112	>	63.10	Mu	286.7470112	>	63.10
>>w2	2.425913739 kNm			>>w2	2.425913739 kNm		
>>M1	0.79	10.08677 kNm		>>M1	0.79	10.08677 kNm	
>>M2	1.58	4.483008889 kNm		>>M2	1.58	4.483008889 kNm	
>>M3	2.37	1.120752222 kNm		>>M3	2.37	1.120752222 kNm	
>>Mmax	0	17.93203556 kNm		>>Mmax	0	17.93203556 kNm	
Mr = Mu<0.67Mp	258.0723101 kNm			Mr = Mu<0.67Mp	258.0723101 kNm		
Mr = Mu>0.67Mp	88.51621342 kNm	>	Mf	Mr = Mu>0.67Mp	88.51621342 kNm	>	Mf

## G MOMENT END PLATE CONNECTION DESIGN

### PRYING ACTION

#### Equilibrium

Mf	17.93 kNm				
Lever Arm 1	0.2 m				
Lever Arm 2	0.1288 m				
F	109.0756421 kN				
Tf1	70.89916735 kN	65% of Load			
Tf2	38.17647472 kN	35% of Load			
Nom. Area Bolt	155 mm <sup>2</sup>				
Stress in Bolt 1	457.4139829 MPa	<	Fub =	825	
Stress in Bolt 2	246.2998369 MPa	<	Fub =	825	
14mm A325 Bolts					
Fub	825 MPa				
Tr (Bolt)	76.725 kN				

### END PLATE YIELDING

Mf	17.93 kNm				
End Plate Length	0.5 mm				
Lever Arm	0.125 mm				
Equivalent Force	143.4562844 kN				
End Plate Thickness	10 mm				
End Plate Width	127 mm				
End Plate Area	1270 mm <sup>2</sup>				
F	112.9577043 MPa	<	f <sub>y</sub> =	400.05	
Tr (End Plate)	400.05 MPa				

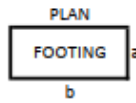
## WELD STRENGTH

Mf	17.93 kNm		
Lever Arm	0.06 m		
Tf	298.8672593 kN	<	Vr = 337.16777
Vr	337.1677659 kN		
>Phi_w	0.67		
>Aw	1077.468 mm <sup>2</sup>		
>>Weld Leg	6 mm		
>>Weld Length	254 mm		
>Xu	490 MPa		
>Theta	90 deg		
Mw	1		

## H FOOTING DESIGN

### OVERTURNING MOMENT DESIGN

f'c	25 MPa		
q <sub>Allowable</sub>	150 kPa	Dense Sand	
Total P	34.34 kN		
A <sub>req</sub>	0.228933333 m <sup>2</sup>		
b <sub>req</sub>	0.478469783 m		
use A	0.8 m <sup>2</sup>		
use a	0.666666667		
use b	1.2 m		
Fb	11050 kN		
>A1	0.09 m <sup>2</sup>		
>A2	0.8 m <sup>2</sup>		
Vc	1064.7 kN		
Depth of Footing	1.3		
Volume of Footing	1.04		
Weight of Footing	6.993913333 kN		
Overturing Mom.	17.93 kNm	<	Mr = 18.845032
Overturing Resis.	18.84503181 kNm		



### MOMENT BASEPLATE CONNECTION DESIGN

Mf	17.93 kNm		
Lever Arm 1	0.2 m		
Lever Arm 2	0.1288 m		
F per bolt	109.0756421 kN	2 Bolts	
Tf1	70.89916735 kN	65% of Load	
Tf2	38.17647472 kN	35% of Load	
Nom. Area Bolt	315 mm <sup>2</sup>		
Stress in Bolt 1	225.0767217 MPa	<	Fub = 825
Stress in Bolt 2	121.1951579 MPa	<	Fub = 825
Anchor Bolt Size	20 mm		
Fub	825 MPa		
Tr (Bolt)	155.925 kN		
Development Ld	576 mm		

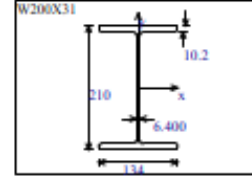
>use 610mm (24") anchor bolts

## Code Details




Project: Detailed Canopy Design  
 Structure:  
 Filename: Detailed Canopy Design.TEL  
 Engineer: Johnson Hu

Page: 1  
 Date: 2021-04-15

**Member: 1** S-FRAME Section is W200X31  
 Member is part of group: SECTION 1  
 Note: Neglecting: axial < 1.0 kN, shear < 1.0 kN, moment < 1.0 kNm  
 Note: Member in braced frame(s).



→ **Load Case 1 (Bending + Compression)**

Section classification ( $f_y=350$ MPa):	Section Class = 1
Governing geometrical slenderness ratio $k_x=1.00; k_y=1.00; k_x L/r_x=36.2;$	$\frac{k_x L/r_x}{200} = \frac{100}{200} = 0.500$
Axial Load - (kN)	
Factored Compressive Resistance Check $n=1.34; \lambda_y=1.33$	$\frac{C_f}{C_{fy}} = \frac{C_f}{\phi A F_y (1 + \lambda_y^{2n})^{-1/n}} = \frac{C_f}{\phi A (148 \text{ MPa})} = \frac{1}{534} = 0.003$
Strong Axis Shear - (kN)	
Strong axis shear strength check $A_w = 1344 \text{ mm}^2$	$\frac{V_{fy}}{\phi A_w F_y} = \frac{V_{fy}}{\phi A_w 0.66 F_y} = \frac{10}{279} = 0.036$
Strong Axis Moment - (kN-m)	
Bending Stability Check $L_u=3.20 \text{ m}; \omega_2=2.426$	$\frac{M_{fy}}{M_{rx}} = \frac{16}{106} = 0.153$
Axial Compression and Bending cross-sectional Strength Check $\omega_{1x}=1.00; U_{1x}=1.00$	$\frac{C_f}{\phi A F_y} + \frac{0.85 U_{1x} M_{fy}}{\phi Z_x F_y} = 0.131$
Axial Compression and Bending overall member Strength Check $\omega_{1x}=1.00; U_{1x}=1.00$	$\frac{C_f}{C_{rx}} + \frac{0.85 U_{1x} M_{fy}}{\phi Z_x F_y} = 0.132$
Axial Compression and Bending lateral torsional buckling strength check $\omega_{1x}=1.00; U_{1x}=1.00$	$\frac{C_f}{C_{ry}} + \frac{0.85 U_{1x} M_{fy}}{M_{rx}} = 0.133$

[Clause 11](#)

[Clause 10.4.2.1](#)

[Clause 13.3.1.1](#)

[Clause 13.4.1.1\(a\)\(i\)](#)

[Clause 13.6.1\(a\)](#)

[Clause 13.8.2\(a\)](#)

[Clause 13.8.2\(b\)](#)

[Clause 13.8.2\(c\)](#)

Design Code: CAN/CSA S16-19  
 Steel Table : Canadian (CISC)  
 Analysis Program: S-FRAME (Linear static analysis)  
**ACADEMIC VERSION NOT FOR COMMERCIAL USE**



**S-STEEL**  
 Version 2020.2.10

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## Code Details

Project: DetailedCanopyDesign  
 Structure:  
 Filename: Detailed Canopy Design.TEL  
 Engineer: Johnson Hu

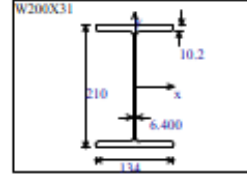
Page: 1  
 Date:2021-04-15

**Member: 2** S-FRAME Section is W200X31

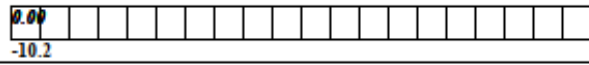
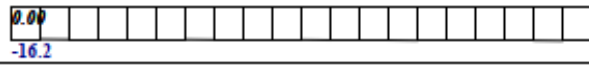
Member is part of group: SECTION 1

Note: Neglecting: axial<1.0 kN, shear<1.0 kN, moment<1.0 kNm

Note: Member in braced frame(s). Angle Gamma is 90.0 degrees



⇒ **Load Case 1 (Bending + Compression)**

Section classification ( $f_y=350$ MPa):	Section Class = 1
Governing geometrical slenderness ratio $k_x=1.00; k_y=1.00; k_x L/r_x=35.9;$	$\frac{k_x L/r_x}{200} = \frac{99}{200} = 0.497$
Axial Load - (kN)	
	3.18 (m)
Factored Compressive Resistance Check $n=1.34; \lambda\gamma=1.32$	$\frac{C_f}{C_{ry}} = \frac{C_f}{\phi A F_y (1+\lambda^{2n})^{-1/n}} = \frac{C_f}{\phi A (150 \text{ MPa})} = \frac{10}{539} = 0.019$
Strong Axis Moment - (kN-m)	
	3.18 (m)
Bending Stability Check $L_u=3.18$ m; $\omega_2=1.020;$	$\frac{M_{fx}}{M_{rx}} = \frac{17}{88} = 0.192$
Axial Compression and Bending cross-sectional Strength Check $\omega_{1x}=0.98; U_{1x}=1.00;$	$\frac{C_f}{\phi A F_y} + \frac{0.85 U_{1x} M_{fx}}{\phi Z_x F_y} = 0.144$
Axial Compression and Bending overall member Strength Check $\omega_{1x}=0.98; U_{1x}=0.98;$	$\frac{C_f}{C_{rx}} + \frac{0.85 U_{1x} M_{fx}}{\phi Z_x F_y} = 0.143$
Axial Compression and Bending lateral torsional buckling strength check $\omega_{1x}=0.98; U_{1x}=1.00;$	$\frac{C_f}{C_{ry}} + \frac{0.85 U_{1x} M_{fx}}{M_{rx}} = 0.182$

[Clause 11](#)

[Clause 10.4.2.1](#)

[Clause 13.3.1.1](#)

[Clause 13.6.1\(a\)](#)

[Clause 13.8.2\(a\)](#)

[Clause 13.8.2\(b\)](#)

[Clause 13.8.2\(c\)](#)

Design Code: CAN/CSA S16-19

Steel Table : Canadian (CISC)

Analysis Program: S-FRAME (Linear static analysis)

**ACADEMIC VERSION NOT FOR COMMERCIAL USE**



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Version 2020.2.10

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# APPENDIX E – STORMWATER CALCULATIONS

## Permeable Concrete Storage Depth Calculations

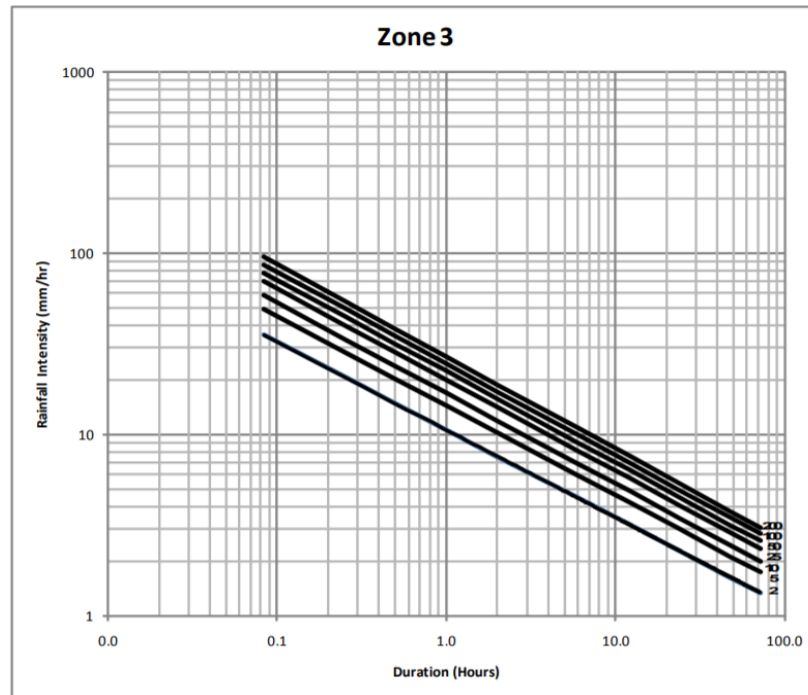


Figure 27: IDF Curve for UBC

10 – year, 24 – hour Storm Intensity = 2.8mm/hr

$$\text{Total Precipitation} = i * d = 2.8 * 24 = 67.2\text{mm}$$

$$\text{Storage in Concrete Layer} = \text{Min. Depth} * \text{Void Space} = 150\text{mm} * 15\% = 22.5\text{mm}$$

$$\begin{aligned} \text{Min. Depth of Reservoir Base} &= \frac{\text{Total Precipitation} - \text{Storage in Concrete Layer}}{\text{Void Space}} = \frac{67.2\text{mm} - 22.5\text{mm}}{35\%} \\ &= 128\text{mm}, \quad \text{Round up to 200mm for contingency} \end{aligned}$$

50mm minimum depth for choker course, so 200mm – 50mm = 150mm depth for reservoir course

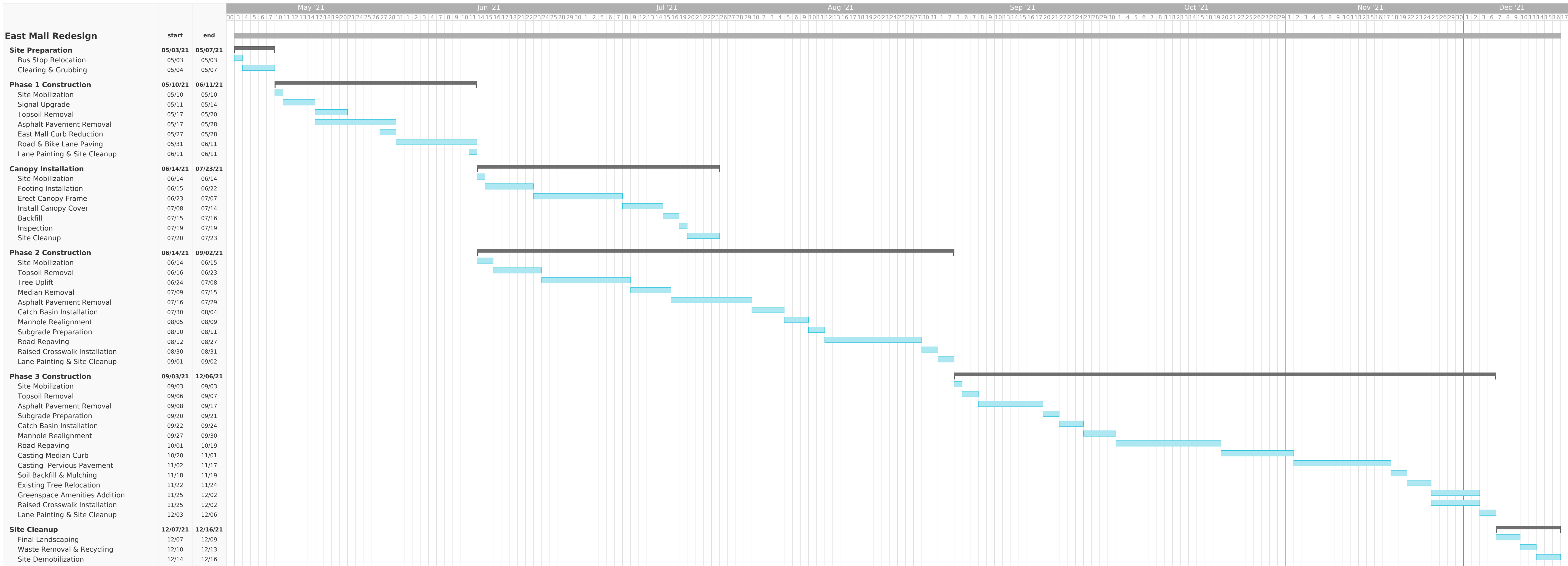
Layer	Void Space (%)	Depth (mm)	Storage (mm)
<b>Permeable Concrete</b>	15	150	22.5
<b>Reservoir</b>	35	200	70
<b>Total</b>		350	92.5
<b>Precipitation</b>			67.2

# APPENDIX F – CLASS A COST ESTIMATE

Description	Quantity	Unit	Pricing		
			Cost per Unit	Sub Cost	Total Cost
<b>DESIGN</b>					<b>\$179,600</b>
<b>Development</b>					\$179,600
Conceptual Design	1	LS	\$39,600	\$39,600	
Preliminary Design	1	LS	\$45,000	\$45,000	
Detailed Design	1	LS	\$80,000	\$80,000	
Drawings	1	LS	\$15,000	\$15,000	
<b>CONSTRUCTION</b>					<b>\$3,826,224</b>
<b>General Permitting</b>					\$28,100
Development Permit	1	LS	\$10,000	\$10,000	
Building Permit	1	LS	\$5,000	\$5,000	
Streets & Landscape Permit	1	LS	\$2,500	\$2,500	
Utilities Permit	1	LS	\$10,600	\$10,600	
<b>On-Site Personnel</b>					\$324,000
Senior Field Engineer	1200	hrs	\$135	\$162,000	
Senior Technician	1200	hrs	\$135	\$162,000	
<b>Construction</b>					\$450,000
Implement Traffic Management Plan	1	LS.	\$150,000	\$150,000	
Equipment Rentals	1	LS.	\$250,000	\$250,000	
Erosion & Sediment Control	1	LS.	\$50,000	\$50,000	
<b>Site Preparation</b>					\$690,730
Site Mobilization	1	LS	\$25,000	\$25,000	
Clearing and Grubbing	2,840	m <sup>2</sup>	\$10	\$28,400	
Top Soil Removal	2,840	m <sup>3</sup>	\$12	\$34,080	
Removal of Concrete Median - Saw Cut	2,840	m <sup>3</sup>	\$75	\$213,000	
Asphalt Pavement Removal - Saw Cut	11,150	m <sup>2</sup>	\$5	\$55,750	
Existing Subgrade Removal	11,150	m <sup>2</sup>	\$30	\$334,500	
Subgrade Preparation	11,150	m <sup>2</sup>	\$5	\$55,750	
<b>Road Repavement</b>					\$797,875
50mm Superpave Mix	85,000	ft <sup>2</sup>	\$3	\$255,000	
180 mm Superpave Mix	85,000	ft <sup>2</sup>	\$5	\$425,000	
150mm Minus Crushed 19mm Granular Base	1,500	ton	\$30	\$45,000	
300mm Minus Crushed 17 mm Granular Base	1,500	ton	\$30	\$45,000	
Site Grading	11,150	m <sup>2</sup>	\$3	\$27,875	
<b>Median Insallation</b>					\$131,725
152 mm Concrete Curb	860	m	\$50	\$43,000	
Curb Ramp	84	ft	\$250	\$21,000	
Soil Backfill	4,515	m <sup>2</sup>	\$15	\$67,725	
<b>Bike Lane &amp; Sidewalks</b>					\$118,025
150mm Pervious Concrete Mix	3,499	m <sup>2</sup>	\$25.00	\$87,475	
50mm Washed AASHTO no.57 Choker Course	500	ton	\$25.00	\$12,500	
150mm Washed AASHTO no.3 Subbase	500	ton	\$25.00	\$12,500	
Non-woven Geotextile Fabric	37,000.000	ft <sup>2</sup>	\$0.15	\$5,550	
<b>Stormwater Facilities</b>					\$100,000
Catch Basins	40	ea.	\$2,500	\$100,000	
<b>Greenspace</b>					\$646,650
450mm Absorbent Topsoil Layer	2,030	m <sup>3</sup>	\$30	\$60,900	
Mulch	20,000	ft <sup>3</sup>	\$3	\$60,000	
Existing Tree Transplant	1	LS.	\$300,000	\$300,000	
Community Garden	1	LS.	\$150,000	\$150,000	
Saucer Magnolia	1	ea.	\$8,000	\$8,000	
Weeping Cherry	1	ea.	\$9,250	\$9,250	
Eastern Redbud	1	ea.	\$7,500	\$7,500	
Red Oak	1	ea.	\$9,000	\$9,000	
Grass Sod	20,000	ft <sup>2</sup>	\$0.85	\$17,000	
Light Fixtures	1	LS.	\$25,000	\$25,000	
32" Flex Bollard - Emergency Access	5	ea.	\$500	\$2,500	

<b>Permanent Traffic Controls</b>						\$177,035
New Signage Implementation	1	LS.	\$150,000	\$150,000		
Raised Crosswalks	2	ea.	\$7,000	\$14,000		
Signal Upgrades	1	LS.	\$4,000	\$4,000		
Skid resistant conflict paint (Bike Crossing/Lane)	1,345	ft <sup>2</sup>	\$6	\$8,070		
Elephants Feet (Bike Crossing)	74	m	\$0	\$15		
48" In-Ground Post	25	ea.	\$38	\$950		
<b>Structural</b>						\$188,084
W200x31 Beam	124.00	m	\$106	\$13,144		
W200x31 Column	140.00	m	\$106	\$14,840		
500x300x20mm Column Base Plate	39	ea.	\$100	\$3,900		
14mm Hex Bolts	312	ea.	\$5	\$1,560		
20mm Anchor Bolts	312	ea.	\$5	\$1,560		
500x134x20mm Column End Plate	39	ea.	\$750	\$29,250		
Concrete Fill	45	m <sup>3</sup>	\$300	\$13,500		
Zingalu Coating	1	LS	\$750	\$750		
20mm Tempered Glass Panel	226	m <sup>2</sup>	\$250	\$56,500		
Glass Mounts	234	ea.	\$120	\$28,080		
Installation and Welding	1	LS.	\$25,000	\$25,000		
<b>End of Construction</b>						\$174,000
Site Cleanup	1	LS	\$20,000	\$20,000		
General Landscaping	1	LS	\$50,000	\$50,000		
Lane & Parking Painting	800	m	\$5	\$4,000		
Waste Removal & Recycling	1	LS	\$100,000	\$100,000		
<b>OPERATION &amp; MAINTENANCE</b>						\$23,500
<b>Maintenance</b>						\$23,500
Greenspace Upkeep	1	yrs	\$12,000	\$12,000		
Signal Operation & Maintenance	1	yrs	\$4,000	\$4,000		
Corridor Operation & Maintenance	1	yrs	\$7,500	\$7,500		
Canopy Maintenance	1	yrs	\$2,000	\$2,000		
Stormwater Facilities Maintenance	1	yrs	\$1,000	\$1,000		
<b>CONTINGENCY (15%)</b>						\$604,399
					<b>Pre-tax cost</b>	<b>\$4,610,222</b>
					<b>PST (7%)</b>	<b>\$322,716</b>
					<b>GST (5%)</b>	<b>\$230,511</b>
					<b>Post-tax cost</b>	<b>\$5,163,449</b>

# APPENDIX G – CONSTRUCTION SCHEDULE



# APPENDIX H – RISK REGISTER

Risk	Project Phase	Likelihood	Impact	Mitigation Strategy
Significant design changes	Design	Low	High	Ensure clarity when communicating with contractors and that all specifications and requirements are understood
Inaccurate cost estimate	Design	Low	High	Continually refine costs estimates and minimize major design changes throughout the project
Delays in obtaining permits	Design	Low	Moderate	Ensure all necessary documents and fees are included in application process
Schedule delays	Design	Moderate	Moderate	Have clear schedule specifications and confirm design with contractors before the start of major work
On-site incidents	Construction	Moderate	Moderate	Ensure equipment is only operated by qualified personnel. Implement adequate signage and minimize contact with pedestrians
Interrupting Buried Utilities	Construction	Low	High	Conduct One-Calls prior to digging and contractor to confirm utility depths. Hand-digging will be used when in proximity to utilities
Traffic Delays	Construction	Moderate	Moderate	Ensure Traffic Management Plan is understood and relayed to all contractors. Equipment transport will be done outside of peak hours
Damage during tree transplant	Construction	Moderate	Low	Ensure all tree work is done in accordance to UBC Tree Protection Guidelines
Contaminated or unsuitable soil	Construction	Moderate	Moderate	Contractor to conduct adequate geotechnical studies. Contaminated soils will be removed and disposed of and replaced with new soil
Concrete Plastic Shrinkage	Construction	Moderate	Low	Ensure concrete curing specifications are conveyed to relevant contractors
COVID 19 - Restrictions	Construction	Moderate	High	Contractors and on-site workers to follow all B.C. and WorkSafeBC COVID-19 protocols relevant to on-site work
Extreme weather	Construction	Low	High	Ensure on-site work and equipment are adequately stored when inclement weather is predicted
Site Vandalism	Construction	Low	Moderate	Ensure all on-site work and equipment are adequately stored and protected after hours
Noise Complaints	Construction	Moderate	Low	Ensure noise sensitive work is done outside of the morning and evening periods



# APPENDIX I – SYNCHRO ANALYSIS

## Thunderbird Boulevard at East Mall – 2020 AM

Lanes, Volumes, Timings  
3: Int 2020-12-01

Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↔		↔	↔	↔	↔	↔	↔	↔	↔	↔	↔
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (m)	0.0	0.0	0.0	50.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Storage Lanes	0	0	0	1	0	0	0	0	0	0	0	0
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0
Leading Detector (m)	15.0	15.0	15.0	15.0	15.0	15.0	15.0	15.0	15.0	15.0	15.0	15.0
Trailing Detector (m)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Turning Speed (k/h)	25	25	15	25	15	25	15	25	15	25	15	25
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Ped Bike Factor	0.95	0.85	0.99	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97
Frt	0.970	0.982	0.946	0.946	0.946	0.946	0.946	0.946	0.946	0.946	0.946	0.946
Fit Protected	0.997	0.950	0.997	0.997	0.997	0.997	0.997	0.997	0.997	0.997	0.997	0.997
Satd. Flow (prot)	0	1713	0	1770	1811	0	0	1716	0	0	1774	0
Fit Permitted	0.982	0.643	0.982	0.982	0.982	0.982	0.982	0.982	0.982	0.982	0.982	0.982
Satd. Flow (perm)	0	1682	0	1022	1811	0	0	1680	0	0	1498	0
Right Turn on Red	Yes		Yes		Yes		Yes		Yes		Yes	
Satd. Flow (RTOR)	30	14	72	19	32	296	187	28	68	11	54	54
Headway Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Link Speed (k/h)	50	50	50	50	50	50	50	50	50	50	50	50
Link Distance (m)	108.8	143.4	126.2	127.5	9.2	9.2	9.2	9.2	9.2	9.2	9.2	9.2
Travel Time (s)	7.8	10.3	9.1	9.2	9.2	9.2	9.2	9.2	9.2	9.2	9.2	9.2
Volume (vph)	5	87	36	59	94	19	32	296	187	28	68	11
Confl. Peds. (#/hr)	53	170	170	53	54	25	25	25	25	25	25	25
Peak Hour Factor	0.42	0.62	0.82	0.87	0.53	0.79	0.89	0.89	0.77	0.78	0.85	0.55
Adj. Flow (vph)	12	140	44	68	177	24	36	333	243	36	80	20
Lane Group Flow (vph)	0	196	0	68	201	0	0	612	0	0	136	0
Turn Type	Perm	4	Perm	8	Perm	2	Perm	6	Perm	6	Perm	6
Protected Phases	4	4	8	8	2	2	2	2	6	6	6	6
Detector Phases	4	4	8	8	2	2	2	2	6	6	6	6
Minimum Initial (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0
Minimum Split (s)	29.0	29.0	29.0	29.0	23.0	23.0	23.0	23.0	23.0	23.0	23.0	23.0
Total Split (s)	29.0	29.0	0.0	29.0	29.0	0.0	31.0	31.0	0.0	31.0	31.0	0.0
Total Split (%)	48.3%	48.3%	0.0%	48.3%	48.3%	0.0%	51.7%	51.7%	0.0%	51.7%	51.7%	0.0%
Maximum Green (s)	25.0	25.0	25.0	25.0	27.0	27.0	27.0	27.0	27.0	27.0	27.0	27.0
Yellow Time (s)	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5
All-Red Time (s)	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
Lead/Lag												
Lead-Lag Optimize?												
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0
Recall Mode	None	None	None	None	Max	Max	Max	Max	Max	Max	Max	Max
Walk Time (s)	14.0	14.0	14.0	14.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0
Flash Dont Walk (s)	11.0	11.0	11.0	11.0	11.0	11.0	11.0	11.0	11.0	11.0	11.0	11.0
Pedestrian Calls (#/hr)	30	30	30	30	10	10	10	10	10	10	10	10
Act Effct Green (s)	12.1	12.2	12.2	12.2	33.0	33.0	33.0	33.0	33.0	33.0	33.0	33.0
Actuated g/C Ratio	0.23	0.23	0.23	0.23	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65
v/c Ratio	0.48	0.29	0.47	0.55	0.55	0.55	0.55	0.55	0.55	0.55	0.55	0.55
Control Delay	16.0	16.5	16.9	10.0	6.1	6.1	6.1	6.1	6.1	6.1	6.1	6.1
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Baseline  
University of British Columbia

Synchro 6 Report  
Page 1

Lanes, Volumes, Timings  
3: Int 2020-12-01

Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Total Delay	16.0	16.5	16.9	10.0	6.1	6.1	6.1	6.1	6.1	6.1	6.1	6.1
LOS	B	B	B	B	A	A	A	A	A	A	A	A
Approach Delay	16.0	16.8	10.0	6.1	6.1	6.1	6.1	6.1	6.1	6.1	6.1	6.1
Approach LOS	B	B	B	A	A	A	A	A	A	A	A	A

**Intersection Summary**

Area Type: Other  
 Cycle Length: 60  
 Actuated Cycle Length: 50.7  
 Natural Cycle: 60  
 Control Type: Semi Act-Uncoord  
 Maximum v/c Ratio: 0.55  
 Intersection Signal Delay: 12.1  
 Intersection LOS: B  
 Intersection Capacity Utilization 68.7%  
 ICU Level of Service C  
 Analysis Period (min) 15

Splits and Phases: 3: Int

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Synchro 6 Report  
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